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AERODYNAMIC DATA ON LARGE SEMISPAN TILTING WING WITH 0.4-DIAMETER CHORD, SINGLE-SLOTTED FLAP, AND SINGLE PROPELLER 0.22 CHORD BELOW WING

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#### SUMMARY

An investigation has been made in the Langley full-scale tunnel to determine the longitudinal aerodynamic characteristics of a large-scale semispan V/STOL tilt-wing configuration with a single propeller which was tested for both up-at-the-tip and down-at-the-tip modes of rotation. The wing had a ratio of chord to propeller diameter of 0.4, a 40-percent-chord single-slotted flap, an aspect ratio of 6.14 (3.07 for the semispan), a taper ratio of 1.0, and an NACA 4420 airfoil section.

The data have not been analyzed in detail but have been examined to observe the predominant trends. The direction of propeller rotation was found to have a very significant effect on the lift and descent capability (as determined from drag-lift ratios attainable without stalling of any part of the wing within the propeller slipstream) and that upat-the-tip rotation gave the more favorable results. The use of a trailing-edge flap was also very effective in increasing the descent capability. The use of flow-control devices (slats and fences) was very effective in increasing the descent capability and lift for down-at-the-tip propeller rotation where the characteristics without such devices were poor but was much less effective for up-at-the-tip propeller rotation where reasonably favorable results were achieved without these devices. For the most favorable combination of the configuration variables, descent angles of nearly 27° were achieved over the entire test range of power conditions.

#### INTRODUCTION

Most of the aerodynamic research that has been done on tilt-wing propeller-driven V/STOL configurations in the past has been of an exploratory character and has been done with small-scale models. The interest in this type of airplane has now become so substantial, however, that there is need for large-scale systematic aerodynamic design data for this concept. A program has therefore been initiated at the Langley Research Center to provide such information by means of tests of a large-scale semispan tilt-wing propeller-driven model. The results of tests for the wing-alone configuration with a

chord-diameter ratio of 0.6 have been presented in references 1 to 3. The results of tests for the configuration with a chord-diameter ratio of 0.5 have been presented in references 4 to 8. These tests covered variations in the model such as height of propeller, presence of fuselage, and use of a single- or double-slotted flap. The present tests were made to obtain aerodynamic data for a model with a single propeller on a semispan wing, a half-fuselage, a chord-diameter ratio of 0.4, a single-slotted flap, a leading-edge slat, and fences. The investigation covered a range of angle of attack from 5° to 80° and a range of thrust coefficient, based on slipstream dynamic pressure, from 0.30 to 0.90. Tests with both directions of propeller rotation were included in the investigation. The results of this investigation are presented herein without analysis in order to expedite their dissemination to industry and the military services.

# SYMBOLS

The positive sense of forces, moments, and angles is shown in figure 1. The pitching-moment coefficients are presented with reference to the wing quarter-chord line. The coefficients are based on the dynamic pressure in the propeller slipstream. Conventional lift, drag, and pitching-moment coefficients based on the free-stream dynamic pressure can be obtained by dividing the slipstream coefficients by  $1 - C_{T,s}$ ; for example,  $C_L = C_{L,s}/(1 - C_{T,s})$ . The thrust coefficient  $C_T'$  may be obtained from the equation  $C_T' = \left[C_{T,s}(A/S)\right]/(1 - C_{T,s})$ .

Measurements for this investigation were made in the U.S. Customary System of Units and equivalent values are indicated herein in the International System of Units (SI). Factors relating the two systems of units used in this paper can be found in the appendix.

The coefficients and symbols used in this paper are defined as follows:

- A total propeller disk area, ft<sup>2</sup> (meters<sup>2</sup>)
- b propeller blade chord, ft (meters); also, wing span, excluding tip fairing, ft (meters)
- $C_{\mathrm{D,s}}$  drag coefficient based on slipstream,  $\frac{\mathrm{D}}{\mathrm{q_s S}}$
- $C_L$  lift coefficient based on free airstream,  $\frac{L}{qS}$
- $C_{L,s}$  lift coefficient based on slipstream,  $\frac{L}{q_s S}$
- $C_{m,s}$  pitching-moment coefficient based on slipstream,  $\frac{M_Y}{q_sSc}$

 $c_{T,s}$  thrust coefficient based on slipstream,  $\frac{T}{q_s \frac{\pi D^2}{4}}$ 

 $C_{T}^{\prime}$  thrust coefficient based on free airstream,  $\frac{T}{qS}$ 

c wing chord, ft (meters)

c<sub>f</sub> flap chord, ft (meters)

D propeller diameter, ft (meters); also, total model drag, lbf (newtons)

h thickness of propeller blade, ft (meters)

L total model lift, lbf (newtons)

 $M_{Y}$  pitching moment, lbf-ft (newton-meters)

q free-stream dynamic pressure,  $\frac{\rho V^2}{2}$ ,  $\frac{lbf}{ft^2}$   $\frac{newtons}{meter^2}$ 

qs slipstream dynamic pressure,  $q + \frac{T}{\frac{\pi D^2}{4}}, \frac{lbf}{ft^2}$   $\left(\frac{newtons}{meter^2}\right)$ 

R radius of propeller blade, 2.83 ft (0.86 meter)

r radius to element on propeller blade, ft (meters)

S area of semispan wing, 15.68 ft<sup>2</sup> (1.46 meters<sup>2</sup>)

T propeller thrust, lbf (newtons)

V free-stream velocity,  $\frac{ft}{sec}$   $\left(\frac{meters}{second}\right)$ 

x distance along wing chord line, ft (meters)

 $y_l$  lower-surface ordinate, ft (meters)

 $\mathbf{y}_{\mathbf{u}}$  upper-surface ordinate, ft (meters)

z vertical distance, ft (meters)

 $\alpha$  angle of attack, degrees

 $\delta_{\mathbf{f}}$  flap deflection, degrees

 $\rho$  mass density of air,  $\frac{\text{slugs}}{\text{ft}^3}$   $\left(\frac{\text{kilograms}}{\text{meter}^3}\right)$ 

# MODEL

The model used in this investigation was a semispan model which would represent the left panel of the full-span wing and the left half of the fuselage. Sketches of the model are presented in figure 2. A three-view drawing of the fuselage-wing combination is shown in figure 2(a), and the principal dimensions of the wing are given in figure 2(b). Details of the wing slat, flap, and fences are given in figures 3(a) and 3(b). The propeller-blade characteristics are shown in figure 4, and a photograph of the model is presented in figure 5.

The wing was constructed to allow numerous modifications to be made in the test configuration, such as a change of wing planform, change of airfoil, the addition of flow-control devices, deflection of the trailing-edge flap, and change of the direction of rotation of the propeller. The basic structure of the wing consisted of a heavy box-beam spar to which a power train was attached to drive the propellers through spanwise shafting and around which various airfoil contours could be fitted. The propeller location was such that the propeller tip extended out to the wing tip. In the present investigation both directions of propeller rotation were tested. The propeller thrust was measured by a strain-gage balance which was a part of the propeller shaft. The output was fed through sliprings to an indicating instrument. The required values of thrust for each value of  $C_{T,s}$  were set by the operator by changing the speed of the propeller drive motor. The blade angle at the 0.75R station of the propeller was held constant at 17° throughout the investigation. The propeller was located 0.22c below the wing chord plane and 0.84c ahead of the wing quarter-chord line as shown in figure 2(b). The thrust line was parallel to the wing chord plane.

The airfoil used on the wing was the NACA 4420 section with a 2.26-ft (0.69-m) chord. This chord length gave a ratio of wing chord to propeller diameter of 0.4. The reference area of the wing based on a semispan of 6.92 ft (2.11m) was 15.68 ft $^2$  (1.46 m $^2$ ) and did not include the area of the tip fairing.

The model had a 0.40c single-slotted trailing-edge flap. The flap ordinates and the positions of the nose for the various deflections are given in figure 3(a). The flap is illustrated in figure 3(a) for the  $40^{\circ}$  deflection.

The leading-edge slat shown in figure 3(a) was investigated in combination with the flap on this model. With down-at-the-tip rotation only, the inboard section of slat was used (0.21b/2 to 0.51b/2); with up-at-the-tip rotation, the inboard and outboard sections (0.69b/2 to 0.95b/2) were used both separately and together.

Fences with a height of 0.20c and extending from 0.14c on the lower surface around the leading edge including the slat to about 0.75c on the upper surface were installed at two spanwise locations on the wing (see fig. 3(b)) in an attempt to confine the center section stall inboard of the propeller slipstream. When tests were made with fences on, both fences were installed.

# TESTS AND RESULTS

The tests were made for a range of single-slotted flap deflections with and without the leading-edge slat and fences. The specific configurations tested and a list of tables and figures in which data for each may be found are given in the following table:

Direction of	Configuration	Flap deflection,		odynamic ita
rotation	-	$^{\delta}_{\mathbf{f}},$ deg	Table	Figure
Down at tip	Basic leading edge	0	1	6
		20	2	7
		40	3	8
		60	4	9
	Basic leading edge and	0	5	10
	fences on	20	6	11
		40	7	12
		60	8	13
	Inboard slat on	20	9	14
		40	10	15
		60	11	16
	Inboard slat on and fences on	20	12	17
		40	13	18
		60	14	19
Up at tip	Basic leading edge	0	15	20
		20	16	21
		40	17	22
		60	18	23
	Basic leading edge and	0	19	24
	fences on	20	20	25
		40	21	26
: 		60	22	27
	Inboard slat on	20	23	28
		40	24	29
		60	25	30
	Inboard slat on and fences on	20	26	31
		40	27	32
		60	28	33
	Full-span slat on and fences on	20	29	34
		40	30	35
		60	31	36

The tests were made over a range of thrust coefficients from 0.30 to 0.90. For any given test the thrust coefficient was held constant over the angle-of-attack range by adjusting the propeller speed to give the required thrust at each angle of attack. The angle-of-attack range was from  $5^{\rm O}$  to that required to stall the wing or to develop a draglift ratio of about 0.3, whichever was lower. The test Reynolds number, based on the wing chord length and the velocity of the propeller slipstream, was about  $1.9 \times 10^6$ .

No tunnel-wall corrections have been applied to the data since surveys and analysis had indicated that there would be no significant correction, as explained in reference 1.

#### DISCUSSION

The data presented have not been analyzed in detail but have been examined to observe general trends. One general observation was that the force-test data could not be used as an indication of the occurrence or extent of wing stalling. The tuft-test results show that the onset of stalling over significant areas of that part of the wing within the propeller slipstream frequently occurs considerably below or above the angle of attack for maximum lift coefficient. The data were examined, in particular, to determine the effect of the various test variables on descent capability, the descent capability being determined from the D/L values attainable prior to indication by the tufts of stalling of any part of the wing within the propeller slipstream.

# Effect of Direction of Propeller Rotation

The force- and tuft-test data show that the up-at-the-tip direction of rotation consistently gave higher maximum lift and higher descent capability. In general, the tuft pictures show that rough flow and stalling occurred at an angle of attack as much as  $25^{\circ}$  to  $30^{\circ}$  lower with down-at-the-tip rotation than with up-at-the-tip rotation for the higher thrust coefficients ( $C_{T,s} = 0.90$  and 0.80). Down-at-the-tip propeller rotation consistently causes stalling (of the part of the wing in the slipstream) to start inboard of the nacelle, that is, behind the up-going blades. When stall occurred on the wing for the up-at-the-tip mode of rotation, it occurred only outboard of the nacelle.

# Effect of Leading-Edge Slat

Comparison of figures 6 to 9 with 14 to 16 for down-at-the-tip rotation and figures 20 to 23 with 28 to 30 for up-at-the-tip rotation gives the effect of the inboard leading-edge slat. With down-at-the-tip rotation, the inboard slat was particularly effective for the lower thrust coefficients ( $C_{T,s}=0.30$  and 0.60) in alleviating the sharp break in the lift curves at stall. The lift-coefficient curves for the configuration with slats were broader at the tops than those for the configuration without slats, and a nearly constant value of  $C_{L,s}$  was obtained over a much higher angle-of-attack range. With

up-at-the-tip rotation, where there was no problem with inboard stall, the slat had an adverse effect for some conditions on the aerodynamic characteristics of the wing.

The effect of the full-span slat was only determined for up-at-the-tip rotation (figs. 34 to 36). By comparison with the inboard-slat results (figs. 31 to 33), the tuft tests show that the use of a full-span slat caused a notable increase in descent capability for the  $20^{\rm O}$  flap deflection and a general improvement in wing stall for both  $\delta_{\rm f}=40^{\rm O}$  and  $60^{\rm O}$ .

# Effect of Fences

The effect of fences can be ascertained for both directions of propeller rotation for the model with the basic leading edge and with the inboard leading-edge slat installed. Compare figures 6 to 19 for down-at-the-tip rotation and figures 20 to 33 for up-at-the-tip rotation. The results show that the fences were most effective for the down-at-the-tip mode of propeller rotation. In this case the wing had a tendency to stall inboard of the nacelle because of the rotation of the propeller slipstream, and the fences were effective in preventing the center-section stall from spreading and prematurely triggering the stalling of the section of the wing in the propeller slipstream inboard of the nacelle. For this mode of propeller rotation, the fences gave significantly more descent capability over the range of flap deflection, particularly for the higher thrust coefficients.

# Effect of Flap Deflection

A progressive increase in maximum lift coefficient and descent capability occurred as the flap deflection was increased. The greatest increment occurred with the deflection from  $0^{\rm O}$  to  $20^{\rm O}$  for either mode of propeller rotation; but it must be pointed out that for down-at-the-tip rotation, the model with  $\delta_{\rm f}=0^{\rm O}$  had a negative descent capability (-D/L). (See fig. 6.) With  $20^{\rm O}$  of flap deflection (fig. 7), a change in the positive direction occurred but still not enough to produce any noticeable descent capability. With upat-the-tip rotation, increasing the flap deflection from  $0^{\rm O}$  to  $20^{\rm O}$  increased the descent angle from about  $-14^{\rm O}$  to about  $10^{\rm O}$  for thrust coefficients of 0.30 and 0.60. (See figs. 20 and 21.) With this direction of rotation, full-span slat, and fences, a descent angle of nearly  $27^{\rm O}$  was obtained with  $60^{\rm O}$  of flap deflection (fig. 36).

#### CONCLUSIONS

An experimental investigation has been made to determine the longitudinal aero-dynamic characteristics of a large-scale semispan V/STOL tilt-wing configuration with a single propeller which was tested for both modes of rotation. The following conclusions were drawn from the results of the investigation:

- 1. The direction of propeller rotation had a significant effect on the lift and descent capability attainable for most of the configurations tested, the up-at-the-tip mode of propeller rotation giving the more favorable results.
- 2. Leading-edge stall-control devices were very effective in improving the descent capability for the down-at-the-tip mode of propeller rotation. With fences and leading-edge slats, almost as favorable results could be achieved with this mode of propeller rotation as with up-at-the-tip rotation.
- 3. The use of flaps was very effective in increasing the lift and the descent capability for either mode of rotation. With  $40^{\circ}$  or  $60^{\circ}$  flap deflection and with the most favorable combination of flow-control devices tested, descent angles of nearly  $27^{\circ}$  were achieved for the entire test range of power conditions.

Langley Research Center,

National Aeronautics and Space Administration, Langley Station, Hampton, Va., September 26, 1968, 721-01-00-11-23.

# APPENDIX

# CONVERSION FACTORS - U.S. CUSTOMARY UNITS TO SI UNITS

The International System of Units (SI) was adopted by the Eleventh General Conference on Weights and Measures, Paris, October 1960. (See ref. 9.) The following conversion factors are included in this report for convenience:

Physical quantity	U.S. Customary Unit	Conversion factor (*)	SI Unit
Area	ft <sup>2</sup>	0.0929	meters <sup>2</sup> (m <sup>2</sup> )
Density	slugs/ft <sup>3</sup>	515.38	kilograms/meter <sup>3</sup> (kg/m <sup>3</sup> )
Force	lbf	4.448	newtons (N)
Length	jin.	0.0254	meters (m)
Hengin	ft	0.3048	meters (m)
Moment	lbf-ft	1.356	newton-meters (N-m)
Pressure	$1$ bf/ft $^2$	47.88	newtons/meter <sup>2</sup> $(N/m^2)$
Velocity	ft/sec	0.3048	meters/second (m/sec)

<sup>\*</sup>Multiply value given in U.S. Customary Unit by conversion factor to obtain equivalent value in SI Unit.

### REFERENCES

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- 2. Fink, Marvin P.; Mitchell, Robert G.; and White, Lucy C.: Aerodynamic Data on Large Semispan Tilting Wing With 0.6-Diameter Chord, Single-Slotted Flap, and Single Propeller Rotating Down at Tip. NASA TN D-2412, 1964.
- 3. Fink, Marvin P.; Mitchell, Robert G.; and White, Lucy C.: Aerodynamic Data on Large Semispan Tilting Wing With 0.6-Diameter Chord, Single Slotted Flap, and Single Propeller Rotating Up at Tip. NASA TN D-1586, 1964.
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- 8. Fink, Marvin P.: Aerodynamic Data on Large Semispan Tilting Wing With 0.5-Diameter Chord, Single-Slotted Flap, and Single Propeller 0.08 Chord Below Wing. NASA TN D-4030, 1967.
- 9. Mechtly, E. A.: The International System of Units Physical Constants and Conversion Factors. NASA SP-7012, 1964.

Table 1.- Aerodynamic data for down-at-tip rotation,  $\text{basic Leading edge, and} \quad \delta_{\mathbf{f}} = 0^O$ 

$  \alpha$	$C_{L,s}$	$c_{\mathrm{D,s}}$	$C_{\mathrm{m,s}}$	$C_{ m L,s}$	${\tt C_{D,s}}$	C <sub>m,s</sub>
deg		$C_{T,s} = 0.90$			$C_{T,S} = 0.80$	)
5	0.307	-1.415	0.419	0.371	-1.234	0.373
10	.498	-1.355	.435	.587	-1.203	.401
15	.659	-1.304	.455	.771	-1.152	.430
20	.831	-1.230	.476	.960	-1.068	.456
25	.986	-1.140	.484	1.114	954	.461
30	1.118	-1.036	.497	1.256	822	.471
35	1.238	915	.505	1.385	690	.484
40	1.345	774	.512	1.487	523	.490
45	1.439	630	.522	1.543	369	.486
50	1.476	483	.512	1.553	198	.473
55	1.513	339	.513	1.570	046	.486
60	1.523	196	.513	1.571	.103	.498
65	1.565	037	.534	1.544	.217	.506
70	1.557	.092	.530	1.519	.343	.534
75	1.559	.229	.558	1.485	.477	.547
80	1.531	.375	.560			
		$C_{T,S} = 0.60$	•		$C_{T,s} = 0.30$	· ·
5	0.383	-0.914	0.286	0.470	-0.435	0.135
10	.646	870	.315	.735	394	.175
15	.865	810	.358	.981	328	.229
20	1.101	717	.376	1.147	220	.217
25	1.283	588	.386	1.191	091	.186
30	1.409	424	.362	1.278	.055	.190
35	1.364	276	.347			
40	1.462	098	.370			

Table 2.- Aerodynamic data for down-at-tip rotation,  $\label{eq:basic} \text{Basic Leading edge, and} \quad \delta_f = 20^O$ 

$\alpha$ ,	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
deg		$C_{T,S} = 0.90$	0		$C_{T,s} = 0.8$	30
5	0.632	-1.325	0.277	0.729	-1.148	0.230
10	,832	-1.263	.304	.970	-1,085	.258
15	1.002	-1.197	.332	1.183	991	.268
20	1.174	-1.086	.332	1.396	865	.280
25	1.328	963	.337	1.569	713	.286
30	1.450	818	.340	1.666	550	.282
35	1.560	672	.354	1.759	380	.282
40	1,643	515	.357	1.831	189	.301
45	1,681	~.366	.358	1.822	028	.267
50	1,692	207	.348	1.710	.088	.273
55	1.685	~.055	.346	1.674	.201	.300
60	1,678	.080	.376	1.615	.310	.325
65	1.655	.203	.385	1.584	.408	.362
70	1.628	.330	.418	1.536	.520	.405
75	1.582	.433	.442	}	}	
80	1.545	.553	.465			
		$C_{T,s} = 0.60$	)		$C_{T,s} = 0.3$	30
5	0.901	-0.822	0.119	1.060	-0.343	-0.041
10	1.187	744	.159	1.399	~.240	021
15	1.474	649	.163	1,736	134	006
20	1.745	493	.174	2,055	.028	.003
25	1.938	319	.180	1,759	.175	057
30	1.987	~.122	.172	1.644	.312	043
35	1.945	.043	.155		]	
40	1.823	.213	.158			:
45	1.801	.346	.175			

Table 3.- Aerodynamic data for down-at-tip rotation,  $\text{Basic Leading edge, and} \quad \delta_{\mathbf{f}} = 40^{O}$ 

$\alpha$ ,	$c_{L,s}$	C <sub>D,s</sub>	$C_{m,s}$	$c_{\mathrm{L,s}}$	$c_{ m D,s}$	C <sub>m,s</sub>
deg	_,~	$C_{T,s} = 0.90$		,-	$C_{T,S} = 0.8$	!
5	0.896	-1.225	0.209	1.038	-1.048	0.139
10	1.078	-1.151	.211	1.260	950	.160
15	1.244	-1.047	.230	1.504	842	.177
20	1.398	924	.250	1.700	690	.171
25	1.548	785	.253	1.883	508	.173
30	1.650	614	.247	1.913	319	.182
35	1.734	452	.251	1.974	139	.198
40	1.772	290	.265	1.968	.049	.201
45	1.756	160	.279	1.831	.159	.197
50	1.767	.001	.287	1.713	.225	.230
55	1.743	.138	.290	1.647	.328	.278
60	1.695	.252	.312	1.611	.451	.296
65	1.640	.363	.336	1.551	.525	.348
70	1.598	.446	.380	1.499	.603	.384
75	1.555	.533	.411			
80	1.513	.667	.434			
		$C_{T,s} = 0.60$	)		$C_{T,s} = 0.3$	0
5	1.199	-0.672	0.037	1.509	-0.200	0.050
10	1.495	569	.045	1.782	078	135
15	1.789	440	.054	2.110	.064	129
20	2.083	253	.043	2.456	.249	135
25	2.194	065	.057	1.952	.376	139
30	2.176	.131	.075	1.763	.504	121
35	1.783	.202	.055		}	
40	1.850	.399	.098			
45	1,790	.519	.121			

table 4.- Aerodynamic data for down-at-tip rotation,  $\text{Basic Leading edge, and} \quad \delta_{\mathbf{f}} = 60^{O}$ 

$\alpha$ ,	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{L,s}$	$C_{D,s}$	C <sub>m,s</sub>
deg		$C_{T,S} = 0.90$			$C_{T,s} = 0.80$	
5	0.997	-1.114	0.165	1.168	-0.939	0.116
10	1.174	-1.024	.176	1.374	821	.120
15	1.331	915	.190	1.585	693	.133
20	1.478	780	.192	1.785	517	.117
25	1.609	631	.198	1.941	326	.123
30	1.697	468	.204	1.959	166	.141
35	1.767	281	.202	1.978	.022	.158
40	1.806	111	.215	1.952	.195	.180
45	1.798	.031	.238	1.753	.279	.180
50	1.750	.159	.253	1.618	.295	.213
55	1.713	.310	.255	1.568	.403	.258
60	1.657	.421	.270	1.526	.508	.289
65	1.597	.509	.291	1.455	.558	.340
70	1.529	.516	.354			
75	1.478	.656	.367			
80	1.438	.840	.364			
		$C_{T,S} = 0.60$			$C_{T,s} = 0.30$	
5	1.360	-0.587	0.005	1.623	-0.086	-0.175
10	1.633	462	.008	1.931	.050	163
15	1.969	296	001	2.261	.193	160
20	2.229	097	.009	2.546	.389	~.156
25	2.231	.082	.027	1.891	.457	129
30	2.193	.269	.040	1.789	.565	122
35	1.906	.375	.043			1
40	1.830	.488	.088			1
45	1.741	.580	.133			

TABLE 5.- AERODYNAMIC DATA FOR DOWN-AT-TIP ROTATION, BASIC LEADING EDGE, FENCES ON, AND  $\,\,\delta_{\mbox{\scriptsize f}}=0^{\mbox{\scriptsize O}}$ 

$\alpha$ ,	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
deg		$C_{T,S} = 0.90$			$C_{T,S} = 0.8$	0
5	0.318	-1.389	0.422	0.365	-1.233	0.384
10	.510	-1.352	.442	.575	-1.187	.407
15	.690	-1.300	.462	.767	-1.137	.435
20	.858	-1.235	.481	.958	-1.050	.452
25	1.012	-1.137	.486	1.134	947	.471
30	1.158	-1.031	.502	1.293	815	.477
35	1.277	903	.504	1.424	675	.483
40	1.393	756	.504	1.546	513	.492
45	1.488	609	.525	1.538	353	.473
50	1.575	449	.520	1.552	203	.471
55	1.627	280	.529	1.569	050	.474
60	1.645	126	.538	1.586	.101	.499
65	1.631	.007	.545	1.588	.254	.523
70	1.622	.147	.562	1.559	.388	.538
75	1.601	.282	.573	1.507	.473	.564
80	1.577	.405	.589			
		$C_{T,s} = 0.60$			$C_{T,s} = 0.3$	30
5	0.396	-0.908	0.294	0.466	-0.436	0.125
10	.645	865	.310	.734	386	.176
15	.869	805	.349	.951	318	.202
20	1.065	695	.336	1.153	195	.201
25	1.231	564	.351	1.297	055	.204
30	1.340	421	.353	1.359	.089	.190
35	1.385	272	.348	1.415	.229	.198
40	1.457	116	.354			

Table 6.- Aerodynamic data for down-at-tip rotation,  $BASIC\ LEADING\ EDGE,\ FENCES\ ON,\ AND\quad \delta_f=20^O$ 

$lpha,  ext{deg}$	$c_{\mathrm{L,s}}$	$C_{\mathrm{D,s}}$	Cm,s	$_{ m C_{L,s}}$	$C_{\mathrm{D,s}}$	$c_{\mathrm{m,s}}$
deg		$C_{T,s} = 0.90$			$C_{T,s} = 0.80$	
5	0.628	-1.329	0.282	0.763	-1.189	0.251
10	.850	-1.262	.309	1.004	-1.125	.269
15	1.032	-1.203	.336	1.228	-1.005	.274
20	1.217	-1.095	.338	1.460	890	.290
25	1.378	966	.353	1.617	716	.298
30	1.510	818	.351	1.745	537	.297
35	1.617	661	.346	1.865	358	.306
40	1.729	474	.347	1.954	157	.309
45	2.018	277	.361	1.988	.033	.304
50	1.879	095	.365	1.683	.038	.314
55	1.800	.022	.368	1.674	.152	.335
60	1.700	.087	.380	1.668	.303	.364
65	1.744	.310	.398	1.673	.488	.396
70	1.719	.417	.424	1.619	.598	.443
75	1.682	.573	.462	1.537	.643	.472
80	1.645	.683	.503			
		$C_{T,s} = 0.60$			$C_{T,s} \approx 0.30$	
5	0.916	-0.833	0.136	1.060	-0.359	-0.024
10	1.217	753	.168	1.427	261	004
15	1.497	654	.180	1.754	138	.006
20	1.762	486	.186	2.084	.029	.006
25	1.968	291	.180	1.809	.204	069
30	2.081	104	.186	1.793	.372	059
35	1.774	.036	.147		-	
40	1.802	.212	.150			
45	1.715	.312	.191			

Table 7.- Aerodynamic data for down-at-tip rotation,  $\text{Basic Leading edge, fences on, and} \quad \delta_{\mathbf{f}} = 40^O$ 

lpha,	$c_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
deg		$C_{T,s} = 0.90$	•		$C_{\mathrm{T,s}} = 0.80$	
5	0.882	-1.250	0.206	1.038	-1.077	0.153
10	1.089	-1.171	.218	1.264	969	.163
15	1.262	-1.068	.229	1.476	842	.178
20	1.425	938	.238	1.678	682	.161
25	1.573	782	.251	1.834	495	.173
30	1.685	623	.242	1.928	297	.175
35	1.778	443	.253	1.975	082	.179
40	1.874	233	.254	2.095	.118	.181
45	1.931	037	.247	2.073	.299	.192
50	2,108	.123	.252	1.682	.189	.226
55	1.893	.287	.283	1.655	.326	.254
60	1.853	.441	.313	1.667	.482	.301
65	1.658	.369	.322	1.643	.623	.331
70	1.622	.480	.360	1.561	.681	.385
75	1.655	.738	.378			
80	1.584	.828	.416			
		$C_{T,S} = 0.60$			$C_{T,s} = 0.30$	
5	1.215	-0.692	0.038	1.440	-0.204	-0.150
10	1.508	574	.034	1.778	086	136
15	1.798	446	.040	2.119	.059	116
20	2.040	252	.033	2.446	.263	136
25	2.198	037	.031	1.970	.404	176
30	2.279	.167	.041	1.913	.556	172
35	2.297	.381	.044			
40	1.823	.380	.062			
45	1.657	.431	.112			
50	1.749	.652	.122	]	]	

table 8.- Aerodynamic data for down-at-tip rotation,  $\text{Basic Leading edge, fences on, and} \quad \delta_{\mathbf{f}} = 60^{O}$ 

α,	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	$C_{m,s}$
deg		$C_{T,s} = 0.90$			$C_{T,s} = 0.80$	
5	0.998	-1.146	0.180	1.145	-0.947	0.119
10	1.162	-1.029	.183	1.366	827	.136
15	1.335	921	.199	1.572	695	.130
20	1.473	776	.204	1.786	521	.122
25	1.591	626	.204	1.916	319	.138
30	1.700	445	.196	1.987	127	.149
35	1.793	266	.201	2.031	.084	.147
40	1.856	051	.208	2.071	.286	.156
45	1.891	.127	.214	1.994	.433	.175
50	1.864	.285	.221	1.593	.294	.228
55	1.831	.458	.236	1.550	.403	.262
60	1.768	.560	.258	1.605	.618	.286
65	1.689	.671	.281	1.538	.694	.338
70	1.592	.709	.316	1.438	.692	.376
75	1.536	.817	.340			
80	1.456	.898	.354			<u></u>
		$C_{T,s} = 0.60$			$C_{T,s} = 0.30$	
5	1.339	-0.587	-0.015	1.601	-0.077	-0.190
10	1.634	456	.001	1.936	.044	161
15	1.904	319	003	2.266	.202	166
20	2.170	089	010	2.514	.433	153
25	2.265	.129	001	1.939	.526	220
30	2.318	.337	0	1.843	.664	175
35	2.240	.522	.009			1
40	1.710	.435	.086			
45	1.576	.490	.130			
50	1.672	.711	.143			

Table 9.- Aerodynamic data for down-at-tip rotation,  $\label{eq:table_stat} \text{Inboard slat on, and} \quad \delta_{\mathbf{f}} = 20^{O}$ 

l a	$c_{L,s}$	$C_{\mathrm{D,s}}$	Cm,s	C <sub>L,s</sub>	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
α, deg		$C_{T,s} = 0.90$			$C_{T,s} = 0.80$	
5	0.647	-1.363	0.281	0.726	-1.181	0.243
10	.842	-1.285	.317	.974	-1.111	.261
15	1.024	-1.208	.320	1.212	-1.017	.272
20	1.208	-1.095	.322	1.447	896	.293
25	1.378	972	.348	1.606	745	.305
30	1.460	835	.354	1.634	586	.307
35	1.532	707	.342	1.730	415	.311
40	1.605	558	.365	1.836	226	.333
45	1.694	399	.367	1.862	047	.331
50	1.726	219	.368	1.854	.095	.357
55	1.755	059	.387	1.839	.242	.378
60	1.782	.120	.410	1.845	.438	.392
65	1.788	.301	.408	1.805	.590	.421
70	1.748	.421	.429	1.734	.704	.447
75	1.684	.505	.461			
80	1.630	.605	.495			
		$C_{T,s} = 0.60$			$C_{T,S} = 0.30$	
5	0.832	-0.845	0.140	0.924	-0.369	-0.013
10	1.163	751	.143	1.341	272	028
15	1.455	641	.160	1.705	154	023
20	1.742	498	.183	2.038	.012	.023
25	1.958	319	.219	2.070	.194	.019
30	1.911	133	.187	2.284	.435	.001
35	2.014	.053	.215	2.280	.619	.012
40	2.053	.245	.213	2.194	.790	.019
45	2.070	.429	.226	2.108	.927	.021
50	2.053	.595	.242			
55	1.987	.727	.273			
60	1.837	.785	.292			

Table 10.- Aerodynamic data for down-at-tip rotation,  $\label{eq:nboard} \text{Inboard slat on, and} \quad \delta_f = 40^o$ 

α,	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{L,s}$	$C_{D,s}$	C <sub>m,s</sub>
deg		$C_{T,s} = 0.9$	0		$C_{T,S} = 0.8$	30
5	0.836	-1.237	0.221	0.974	-1.063	0.150
10	1.047	-1.160	.222	1.235	968	.162
15	1.215	-1.052	.234	1.445	837	.173
20	1.373	937	.256	1.673	692	.175
25	1.517	780	.253	1.839	513	.188
30	1.633	626	.257	1.813	356	.182
35	1.676	497	.272	1.878	177	.214
40	1.699	349	.284	1.939	.046	.207
45	1.734	180	.286	1.941	.199	.228
50	1.747	014	.298	1.846	.286	.260
55	1.759	.143	.318	1.823	.438	.287
60	1.749	.317	.308	1.807	.601	.318
65	1.726	.481	.337	1.725	.734	.340
70	1.666	.559	.370	1.635	.821	.387
75	1.610	.623	.414			
80	1.550	.726	.432			
		$C_{T,s} = 0.60$	)		$C_{T,s} = 0.3$	80
5	1.131	-0.707	0.036	1.308	-0.227	-0.136
10	1.473	601	.043	1.731	087	143
15	1.786	449	.038	2.088	.059	113
<b>2</b> 0	2.074	270	.049	2.379	.252	116
25	2.118	077	.056	2.225	.432	125
30	2.070	.102	.068	2.361	.682	127
35	2.150	.317	.091	2.311	.844	107
40	2.121	.494	.093	2.234	.988	066
45	2.080	.640	.126			
50	2.017	.771	.161			
55	1.899	.842	.195			

Table 11.- Aerodynamic data for down-at-tip rotation,  $\label{eq:nboard} \text{Inboard slat on, and} \quad \delta_f = 60^{O}$ 

$  \alpha$	C <sub>L,s</sub>	$c_{ m D,s}$	C <sub>m,s</sub>	C <sub>L,s</sub>	C <sub>D,s</sub>	$c_{ m m,s}$
deg		$C_{T,s} = 0.90$	)	$C_{T,S} = 0.80$		
5	0.970	-1.148	0.172	1.121	-0.971	0.108
10	1.190	-1.056	.169	1.368	869	.123
15	1.339	932	.189	1.616	711	.114
20	1.491	802	.208	1.828	540	.134
25	1.628	650	.208	1.959	346	.136
30	1.712	482	.210	1.943	193	.158
35	1.753	321	.221	1.966	005	.178
40	1.726	183	.231	1.986	.184	.193
45	1.757	025	.243	1.936	.327	.194
50	1.762	.137	.252	1.857	.430	.235
55	1.752	.298	.264	1.738	.501	.272
60	1.715	.426	.294	1.737	.704	.282
65	1.679	.516	.328	1.657	.818	.321
70	1.614	.621	.358	1.565	.889	.370
75	1.560	.715	.380			
80	1.488	.857	.369			
		$C_{T,S} = 0.60$	)	$C_{T,s} = 0.30$		
5	1.302	-0.599	-0.009	1.534	-0.129	-0.170
10	1.665	464	.008	1.952	.019	152
15	1.974	297	014	2.293	.212	168
20	2.222	116	.008	2.533	.394	136
<b>2</b> 5	2.235	.069	.033	2.409	.640	151
30	2.119	.256	.038	2.434	.839	130
35	2.152	.453	.058	2.372	1.014	124
40	2.101	.633	.082	2.195	1.081	074
45	2.046	.775	.101			
50	1.958	.877	.161			
55	1.852	.940	.215			

TABLE 12.- AERODYNAMIC DATA FOR DOWN-AT-TIP ROTATION, INBOARD SLAT ON, FENCES ON, AND  $\,\,\delta_f$  =  $\,20^{O}$ 

$\alpha$ ,	$C_{L,s}$	$C_{D,s}$	C <sub>m,s</sub>	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg		$C_{T,s} = 0.9$	0	$C_{T,s} = 0.80$			
5	0.623	-1.345	0.283	0.731	-1.184	0.232	
10	.837	-1.282	.299	.963	-1.111	.249	
15	1.058	-1.197	.305	1.209	-1.016	.266	
20	1.213	-1.097	.317	1.434	876	.274	
25	1.377	965	.339	1.603	724	.284	
30	1.497	818	.340	1.732	546	.284	
35	1.612	653	.338	1.842	369	.292	
40	1.724	473	.340	1.948	141	.302	
45	1.795	291	.351	2.008	.056	.312	
50	1.868	089	.367	2.056	.244	.329	
55	1.882	.083	.376	1.993	.399	.349	
60	1.860	.234	.387	1.943	.542	.378	
65	1.837	.406	.408	1.865	.633	.419	
70	1.799	.548	.424	1.806	.805	.454	
75	1.729	.652	.435	1.739	.881	.484	
80	1.668	.745	.477	1.641	.938	.515	
		$C_{T,S} = 0.60$	0	$C_{T,s} = 0.30$			
5	0.823	-0.848	0.149	0.919	-0.363	-0.016	
10	1.157	749	.152	1.345	264	001	
15	1.466	638	.166	1.702	142	.007	
20	1.743	485	.186	2.061	.034	.017	
<b>2</b> 5	1.951	296	.196	2.348	.247	.016	
30	2.110	092	.196	2.526	.496	.017	
35	2.174	.103	.201	2.568	.709	.020	
40	2.268	.327	.220	2.378	.851	.012	
45	2.284	.520	.236	2.166	.911	.023	
50	2.175	.670	.240			,	
55	2.064	.803	.260				
60	1.912	.845	.307	į		_]	

table 13.- Aerodynamic data for down-at-tip rotation, inboard slat on, fences on, and  $~\delta_f$  =  $40^{\rm o}$ 

$  \alpha$	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathrm{L,s}}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg		$C_{T,S} = 0.90$	)	$C_{T,S} = 0.80$			
5	0.822	-1.234	0.186	0.974	-1.077	0.138	
10	1.027	-1.150	.195	1.225	968	.146	
15	1.203	-1.048	.206	1.459	845	.164	
20	1.377	914	.215	1.661	674	.154	
25	1.515	768	.227	1.819	495	.156	
30	1.633	603	.226	1.939	284	.162	
35	1.730	427	.219	2.026	088	.166	
40	1.813	216	.228	2.094	.132	.175	
45	1.894	022	.246	2.113	.324	.197	
50	1.924	.150	.248	2.063	.490	.207	
55	1.908	.314	.258	2.003	.620	.241	
60	1.874	.479	.268	1.887	.715	.285	
65	1.813	.613	.296	1.799	.798	.328	
70	1.741	.723	.322	1.723	.910	.360	
75	1.659	.809	.351				
80	1.600	.878	.397				
		$C_{T,s} = 0.60$	)	$C_{T,s} = 0.30$			
5	1.120	-0.710	-0.025	1.319	-0.241	-0.129	
10	1.207	587	.011	1.764	101	128	
15	1.799	447	.037	2.121	.063	132	
20	2.065	255	.029	2.466	.256	108	
25	2,212	021	.039	2.692	.526	130	
30	2.286	.192	.041	2.758	.789	134	
35	2.335	.395	.053	2.703	.987	123	
40	2.358	.602	.075	2.668	1.156	092	
45	2.329	.774	.096	2.248	1.093	038	
50	2.168	.889	.129				
55	2.027	.959	.176				
60	1.818	.933	.249				

TABLE 14.- AERODYNAMIC DATA FOR DOWN-AT-TIP ROTATION, INBOARD SLAT ON, FENCES ON, AND  $\,\,\delta_f$  =  $60^{O}$ 

α,	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathrm{L,s}}$	C <sub>D,s</sub>	C <sub>m,s</sub>	
deg		$C_{T,s} = 0.9$	0	0		$C_{T,S} = 0.80$	
5	0.936	-1.160	0.180	1.097	-0.949	0.099	
10	1.139	-1.056	.182	1.337	839	.119	
15	1.312	939	.188	1.573	698	.118	
20	1.466	806	.194	1.783	516	.114	
25	1.608	640	.209	1,890	322	.138	
30	1.715	459	.190	1,982	127	.137	
35	1.797	278	.200	2.044	.074	.134	
40	1.857	074	.208	2.081	.286	.151	
45	1.892	.112	.213	2.078	.458	.167	
50	1.882	.271	.226	1.986	.584	.198	
55	1.838	.434	.238	1.917	.715	.233	
60	1.807	.599	.260	1.808	.808	.268	
65	1.730	.692	.284	1.703	.894	.320	
70	1.667	.802	.302	1.618	.981	.367	
75	1.586	.874	.325			ł	
80	1.494	.944	.355	1			
		$C_{T,s} = 0.66$	0	$C_{T,S} = 0.30$			
5	1.314	-0.600	-0.009	1.525	-0.122	-0.181	
10	1.652	478	018	1.947	.027	171	
15	1,978	296	014	2.304	.218	177	
20	2.179	107	0	2.539	.392	125	
25	2.315	.125	.013	2.712	.684	152	
30	2.349	.344	.026	2.734	.934	168	
35	2.354	.548	.035	2.675	1.129	150	
40	2.348	.754	.058	2.315	1.078	070	
45	2.207	.879	.091	!		}	
50	2.068	.995	.113	j			
55	1.953	1.068	.166		į		
60	1.754	.995	.247				

Table 15.- Aerodynamic data for up-at-tip rotation,  $\text{basic Leading edge, and} \quad \delta_{\mathbf{f}} = 0^{O}$ 

	$c_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	$c_{m,s}$	$c_{ m L,s}$	$C_{D,s}$	C <sub>m,s</sub>	
α, deg	L,S	D,s	m,s	L,S	1	ııı,s	
		$C_{T,s} = 0.90$		$C_{T,s} = 0.80$			
5	0.263	-1.431	0.435	0.310	-1.257	0.380	
10	.454	-1.395	.470	.529	-1.214	.421	
15	.637	-1.333	.488	.741	-1.151	.445	
20	.812	-1.259	.504	.945	-1.072	.467	
25	.981	-1.164	.512	1.131	960	.475	
30	1.137	-1.052	.508	1.273	820	.487	
35	1.256	928	.518	1.406	684	.497	
40	1.364	776	.531	1.530	510	.508	
45	1.466	634	.526	1.634	345	.519	
50	1.540	485	.536	1.714	163	.515	
55	1.609	313	.535	1.765	.011	.511	
60	1.643	152	.534	1.788	.175	.521	
65	1.655	.005	.530	1.789	.345	.522	
70	1.659	.144	.532	1.741	.468	.535	
75	1.649	.284	.543	1.641	.558	.554	
80	1.639	.440	.557	1.497	.606	.542	
		$C_{T,S} = 0.60$			$C_{T,S} = 0.30$		
5	0.365	-0.921	0.275	0.441	-0.443	0.106	
10	.605	878	.310	.715	406	.174	
15	.844	819	.357	.971	335	.218	
20	1.088	725	.363	1.204	231	.237	
25	1.289	600	.385	1.297	093	.210	
30	1.478	434	.384	1.398	.080	.195	
35	1.499	258	.357	1.437	.221	.166	
40	1.550	090	.345				

TABLE 16.- AERODYNAMIC DATA FOR UP-AT-TIP ROTATION, BASIC LEADING EDGE, AND  $\delta_{\mbox{\scriptsize f}}$  =  $20^{\mbox{\scriptsize O}}$ 

lpha, deg	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg		$C_{T,S} = 0.90$	$C_{T,S} = 0.90$		$C_{T,s} = 0.80$		
5	0.593	-1.326	0.306	0.697	-1.145	0.233	
10	.792	-1.260	.319	.941	-1.063	.248	
15	.985	-1.170	.331	1,163	960	.250	
20	1.149	-1.066	.321	1.367	~.835	.276	
25	1.313	925	.342	1.553	687	.274	
30	1.453	777	.337	1.699	515	.275	
35	1.557	616	.328	1.789	330	.272	
40	1.635	450	.327	1.852	~.143	.279	
45	1.703	280	.328	1.894	.042	.279	
50	1.736	122	.331	1.911	.206	.288	
55	1.751	.036	.326	1.902	.366	.308	
60	1.740	.174	.347	1.876	.510	.321	
65	1.730	.323	.357	1.819	.635	.340	
70	1.696	.445	.378	1.761	.705	.390	
75	1.655	.550	.399				
80	1.610	.636	.431				
		$C_{T,s} = 0.60$		$C_{T,s} = 0.30$			
5	0.856	-0.813	0.123	1.019	-0.333	-0.062	
10	1.147	731	.130	1.382	247	041	
15	1.417	602	.145	1.735	111	028	
20	1.702	451	.156	2.058	.048	018	
25	1.872	263	.141	2.233	.250	024	
30	2.002	074	.138	2.308	.467	033	
35	2.031	.106	.141	1.843	.537	054	
40	2.089	.289	.156	1.801	.692	060	
45	2.023	.484	.149				
50	1.964	.632	.170	ļ.			
55	1.798	.717	.173				
60	1.646	.753	.196				

Table 17.- Aerodynamic data for up-at-tip rotation,  $\text{Basic Leading edge, and} \quad \delta_{\mathbf{f}} = 40^{O}$ 

$\dot{ }$ $\alpha$ ,	$C_{L,s}$	$C_{\mathrm{D,s}}$	$c_{m,s}$	$c_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	
α, deg		$C_{T,S} = 0.90$		$C_{T,s} = 0.80$			
5	0.833	-1.211	0.201	0.993	-1.013	0.136	
10	1.018	-1.123	.215	1.223	910	.145	
15	1.188	-1.020	.225	1.420	785	.159	
20	1.357	880	.226	1.656	621	.148	
25	1.491	718	.228	1.816	438	.158	
30	1.629	557	.222	1.935	245	.159	
35	1.740	386	.220	1.971	067	.173	
40	1.786	202	.217	2.001	.120	.177	
45	1.810	045	.231	1.991	.280	.190	
50	1.825	.133	.244	1.963	.425	.207	
55	1.808	.272	.255	1.919	.552	.239	
60	1.757	.363	.259	1.874	.675	.256	
65	1.724	.474	.294	1.800	.771	.287	
70	1.684	.573	.325	1.713	.810	.342	
75	1.618	.638	.349	1.554	.800	.384	
80	1.572	.720	.403				
		$C_{T,S} = 0.60$		$C_{T,s} = 0.30$			
5	1.203	-0.661	0.011	1.461	-0.156	-0.183	
10	1.474	~.538	.006	1.809	030	189	
15	1.775	400	.014	2.107	.119	160	
20	2.065	213	.009	2.402	.289	148	
25	2.165	011	.014	2.598	.501	155	
30	2.248	.179	.030	2.505	.716	155	
35	2.221	.351	.033	2.401	.871	155	
40	2.185	.514	.075	1.823	.830	096	
45	2.150	.654	.088				
50	2.088	.771	.136				
55	2.012	.867	.169				
60	1.595	.810	.173		1		

Table 18.- Aerodynamic data for up-at-tip rotation,  $BASIC\ LEADING\ EDGE,\ AND\quad \delta_f=60^O$ 

α,	$c_{\mathrm{L,s}}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathtt{L},\mathtt{s}}$	C <sub>D,s</sub>	C <sub>m,s</sub>	
α, deg		$C_{T,s} = 0.90$		C <sub>T,s</sub> = 0.80			
5	0.925	-1.105	0.193	1.085	-0.897	0.100	
10	1.088	-1.016	.195	1.294	781	.106	
15	1.257	892	.195	1.505	642	.104	
20	1.401	747	.197	1.730	463	.100	
25	1.549	575	.182	1.865	290	.115	
30	1.671	393	.182	1.966	102	.129	
35	1.731	231	.184	1.966	.078	.132	
40	1.786	055	.200	1.967	.249	.142	
45	1.804	.124	.200	1.954	.400	.161	
50	1.802	.270	.213	1.901	.513	.190	
55	1.775	.400	.228	1.861	.654	.197	
60	1.735	.504	.250	1.800	.759	.225	
65	1.672	.549	.281	1.724	.841	.260	
70	1.626	.617	.319	1.632	.880	.322	
75	1.568	.650	.365	1.360	.738	.369	
80	1.498	.703	.397				
		$C_{T,s} = 0.60$		$C_{T,s} = 0.30$			
5	1.308	-0.541	-0.038	1.632	-0.004	-0.255	
10	1.610	406	047	1.908	.105	217	
15	1.835	271	022	2.166	.243	199	
20	2.060	078	019	2.440	.425	170	
25	2.212	.125	.008	2.616	.635	159	
30	2.235	.334	.005	2.446	.828	158	
35	2.167	.482	.014	2.330	.961	155	
40	2.130	.628	.049	1.764	.894	093	
45	2.080	.751	.088				
50	1.996	.847	.109			Ì	
55	1.916	.920	.146				
60	1.417	.738	.197				

Table 19.- Aerodynamic data for up-at-tip rotation,  $\text{Basic Leading edge, fences on, and} \quad \delta_{\mathbf{f}} = 0^O$ 

Г	CT	CD =	C	CT	CD -	C	
$\alpha$ ,	$c_{\mathtt{L},\mathtt{s}}$	$C_{\mathrm{D,s}}$	$C_{m,s}$	$\mathtt{c}_{\mathtt{L},\mathtt{s}}$	$C_{D,s}$	$C_{m,s}$	
deg		$C_{T,s} = 0.9$	90	$C_{T,s} = 0.80$			
5	0.247	-1.416	0.426	0.299	-1.257	0.376	
10	.459	-1.382	.459	.526	-1.224	.416	
15	.645	-1.325	.481	.722	-1.150	.432	
20	.821	-1.255	.490	.929	-1.064	.463	
25	.982	-1.153	.501	1.115	954	.467	
30	1.137	-1.034	.506	1.278	810	.474	
35	1.262	911	.510	1.418	680	.491	
40	1.378	764	.525	1.560	500	.504	
45	1.470	613	.530	1.662	331	.507	
50	1.549	467	.522	1.735	148	.494	
55	1.615	286	.523	1.772	.024	.499	
60	1.623	129	.516	1.796	.193	.503	
65	1.667	.007	.523	1.782	.337	.511	
70	1.661	.157	.534	1.741	.464	.530	
75	1.664	.327	.551	1.659	.553	.540	
80	1.637	.458	.561	1.492	.584	.534	
		$C_{T,s} = 0.$	60	$C_{T,S} = 0.30$			
5	0.361	-0.930	0.276	0.454	-0.458	0.113	
10	.606	891	.315	.719	411	.168	
15	.850	826	.362	.985	339	.219	
20	1.090	725	.362	1.231	222	.220	
25	1.321	596	.395	1.359	095	.220	
30	1.524	426	.396	1.438	.083	.190	
35	1.515	248	.340	1.497	.235	.175	
40	1.591	075	.345				
45	1.658	.102	.352				
50	1.706	.290	.357				

table 20.- Aerodynamic data for up-at-tip rotation, basic leading edge, fences on, and  $~\delta_{\rm f}$  = 20°

α,	$c_{\mathrm{L,s}}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg		$C_{T,s} = 0.9$	00	$C_{T,s} = 0.80$			
5	0.578	-1.332	0.306	0.696	-1.146	0.238	
10	.797	-1.269	.325	.933	-1.068	.256	
15	.993	-1.181	.337	1.152	965	.276	
20	1.177	-1.057	.326	1.359	833	.271	
<b>2</b> 5	1.352	915	.335	1.537	674	.278	
30	1.491	759	.335	1.696	495	.274	
35	1.593	601	.333	1.785	315	.271	
40	1.684	418	.321	1.872	111	.270	
45	1.750	240	.316	1.927	.073	.273	
50	1.791	070	.319	1.940	.244	.279	
55	1.808	.095	.338	1.924	.390	.304	
60	1.791	.229	.344	1.885	.517	.326	
65	1.761	.356	.352	1.832	.629	.350	
70	1.736	.495	.386	1.745	.711	.378	
75	1.688	.590	.420	1.624	.733	.421	
80	1.636	.671	.448	1.421	.712	.427	
		$C_{T,s} = 0.6$	0	$C_{T,s} = 0.30$			
5	0.850	-0.815	0.122	1.023	-0.339	-0.065	
10	1.134	723	.133	1.374	230	035	
15	1.426	601	.149	1.712	108	028	
20	1.694	444	.161	2.050	.058	007	
<b>2</b> 5	1.917	245	.154	2.322	.284	033	
30	2.060	038	.143	2.480	.517	051	
35	2.150	.154	.142	2.509	.714	050	
40	2.209	.371	.149	1.937	.763	063	
45	2.216	.553	.155				
50	2.178	.713	.163				
55	2.120	.854	.190				
60	1.691	.844	.190	ĺ			

Table 21.- Aerodynamic data for up-at-tip rotation,  $\text{basic Leading edge, fences on, and} \quad \delta_f = 40^o$ 

$  \alpha$	$C_{L,s}$	$c_{\mathrm{D,s}}$	$C_{m,s}$	$C_{L,s}$	$C_{D,s}$	C <sub>m,s</sub>	
deg	,	$C_{T,s} = 0.9$		$C_{T,s} = 0.80$			
5	0.834	-1.208	0.225	0.995	-1.018	0.141	
10	1.036	-1.117	.232	1.223	912	.162	
15	1.213	-1.009	.235	1.423	789	.166	
20	1.369	871	.240	1.633	615	.153	
25	1.532	712	.239	1.818	426	.153	
30	1.661	539	.237	1.932	224	.159	
35	1.755	352	.225	1.994	035	.162	
40	1.829	158	.231	2.016	.160	.159	
45	1.852	.009	.239	2.018	.320	.182	
50	1.855	.163	.246	1.994	.459	.213	
55	1.839	.319	.255	1.942	. 572	.238	
60	1.788	.421	.281	1.884	.682	.261	
65	1.746	.516	.310	1.814	.777	<b>.2</b> 88	
70	1.695	.607	.342	1.703	.816	.336	
75	1.639	.671	.383	1.568	.817	.381	
80	1.586	.733	.414	1.347	.726	.401	
		$C_{T,s} = 0.6$	0	$C_{T,s} = 0.30$			
5	1.186	-0.669	0.014	1.428	-0.166	-0.178	
10	1.469	556	.014	1.784	041	168	
15	1.761	400	.019	2.122	.100	164	
20	1.995	201	.006	2.417	.293	147	
25	2.190	.009	.011	2.638	.548	166	
30	2.270	.217	.010	2.724	.785	191	
35	2.299	.409	.019	2.693	.982	170	
40	2.304	.607	.044	2.561	1.146	153	
45	2.251	.752	.065	1.775	.975	092	
50	2.205	.903	.092				
55	2.117	1.018	.124				
60	1.584	.873	.165				

Table 22.- Aerodynamic data for up-at-tip rotation,  $\text{Basic Leading edge, fences on, and} \quad \delta_{\mathbf{f}} = 60^{O}$ 

α,	C <sub>L,s</sub>	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	C <sub>L,s</sub>	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg		$C_{T,S} = 0.9$	90	$C_{T,s} = 0.80$			
5	0.934	-1.110	0.198	1.082	-0.919	0.115	
10	1.109	-1.014	.210	1.308	801	.135	
15	1.272	908	.223	1.523	648	.118	
20	1.417	755	.216	1.728	459	.100	
25	1.603	564	.192	1.859	275	.125	
30	1.710	381	.188	1.965	086	.134	
35	1.795	192	.196	1.982	.096	.140	
40	1.835	016	.206	1.994	.278	.147	
45	1.839	.141	.207	1.990	.437	.156	
50	1.837	.315	.213	1.929	.542	.188	
55	1.808	.450	.237	1.868	.652	.214	
60	1.743	.515	.260	1.810	.760	.235	
65	1.699	.587	.287	1.729	.845	.263	
70	1.639	.639	.332	1.635	.896	,316	
75	1.584	.684	.380	1.420	.801	,365	
80	1.531	.720	.417	1.270	.728	.395	
		$C_{T,s} = 0.6$	0	$C_{T,s} = 0.30$			
5	1.288	-0.554	-0.016	1.635	-0.017	-0,241	
10	1.608	420	009	1.907	.104	197	
15	1.860	277	005	2.209	.242	-,183	
20	2.073	078	.004	2.445	.434	180	
25	2.216	.140	.009	2.626	.677	149	
30	2.278	.355	.008	2.646	.896	140	
35	2.269	.534	.018	2.578	1.070	-,105	
40	2,234	.695	.058	1.879	.952	047	
45	2.180	.823	.086				
50	2.107	.954	.098				
55	1.818	.980	.124				
60	1.457	.825	.182				

TABLE 23.- AERODYNAMIC DATA FOR UP-AT-TIP ROTATION, INBOARD SLAT ON, AND  $\,\,\delta_f$  = 200

α,	$c_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
deg	$C_{T,s} = 0.90$			$C_{T,s} = 0.80$		
5	0.496	-1.283	0.335	0.582	-1.139	0.278
10	.712	-1.258	.356	.819	-1.076	.297
15	.905	-1.190	.379	1.070	988	.296
20	1.091	-1.094	.371	1.321	855	.289
25	1.260	957	.367	1.555	697	.274
30	1.409	808	.360	1.688	522	.266
35	1.551	650	.355	1.778	341	.266
40	1.680	447	.337	1.943	120	.271
45	1.749	281	.327	1.976	.060	.279
50	1.780	114	.337	1.988	.230	.288
55	1.786	.040	.346	1.955	.387	.311
60	1.769	.172	.345	1.929	.527	.326
65	1.753	.317	.359	1.880	.642	.369
70	1.709	.425	.386	1.810	.735	.397
75	1.682	.546	.407	1.715	.774	.425
80	1.641	.632	.444	1.479	.740	.441
	$C_{T,s} = 0.60$		$C_{T,s} = 0.30$			
5	0.704	-0.808	0.149	0.839	-0.345	-0.012
10	1.028	734	.157	1.272	250	023
15	1.335	619	.158	1.644	135	010
20	1.680	472	.151	2.021	.027	.001
25	1.893	267	.152	2.231	.212	010
30	1.906	125	.152	2.181	.390	030
35	1.913	.031	.163	2.082	.570	019
40	1.964	.209	.190			
45	2.040	.454	.179			
50	2.010	.641	.178			
55	1.823	.724	.183			

TABLE 24.- AERODYNAMIC DATA FOR UP-AT-TIP ROTATION,  $\label{eq:table_scale} \text{INBOARD SLAT ON, AND} \quad \delta_{\mathbf{f}} = 40^{O}$ 

α, deg	$c_{\mathrm{L,s}}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
	$C_{T,s} = 0.90$			$C_{T,s} = 0.80$		
5	0,689	-1.218	0.285	0.818	-1,052	0.204
10	.885	-1.154	.289	1.067	948	.200
15	1.068	-1.060	.297	1.331	823	.191
20	1.250	926	.286	1.587	643	.158
25	1.443	763	.269	1.804	459	.149
30	1.580	~.585	.235	1.928	246	.159
35	1.703	400	.228	2.019	055	.156
40	1.789	~.198	.222	2.059	.146	.160
45	1.817	034	.229	2.042	.302	.174
50	1.820	.108	.241	1.996	.441	.205
55	1.793	.234	.261	1.958	.568	.228
60	1.772	.361	.276	1.901	.675	.254
65	1.725	.462	.301	1.837	.777	.305
70	1.679	.545	.340	1.755	.818	.358
75	1.630	.631	.374	1.628	.832	.381
80	1.568	.699	.401			
	$C_{T,s} = 0.60$			$C_{T,s} = 0.30$		
5	0.968	-0.694	0.047	1.225	-0.196	-0.154
10	1.321	591	.049	1.674	075	201
15	1.693	432	.021	2.061	.098	167
20	2.042	227	004	2.423	.286	159
<b>2</b> 5	2.209	022	.020	2.564	.497	162
30	2.108	.119	.035	2.399	.649	146
35	2.057	.241	.075	2.448	.879	143
40	2.038	.389	.099	1.946	.875	077
45	2.159	.636	.108		1	
50	2.133	.800	.134			
55	1.752	.815	.126		ł	
60	1.592	.814	.189			

Table 25.- Aerodynamic data for up-at-tip rotation,  $\label{eq:nboard} \text{Inboard slat on, and} \quad \delta_f = 60^O$ 

$\alpha$ , deg	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$\mathtt{c}_{\mathtt{L,s}}$	$\mathtt{c}_{\mathtt{D,s}}$	C <sub>m,s</sub>	
deg	$C_{T,s} = 0.90$				$C_{T,s} = 0.80$		
5	0.758	-1.152	0.263	0.879	-0.960	0.174	
10	.954	-1.079	.276	1.132	856	.163	
15	1.135	977	.257	1.394	703	.151	
20	1.309	822	.253	1.651	495	.116	
25	1.475	632	.230	1.849	300	.114	
30	1.645	426	.195	1.961	112	.121	
35	1.722	249	.196	2.029	.088	.124	
40	1.772	069	.203	2.059	.279	.144	
45	1.787	.089	.207	2.003	.427	.150	
50	1.787	.248	.221	1.944	.548	.182	
55	1.752	.362	.232	1.898	.669	.212	
60	1.705	.439	.257	1.854	.786	.243	
65	1.663	.530	.295	1.757	.852	.265	
70	1.607	.584	.336	1,674	.864	.363	
75	1.549	.635	.365	1.542	.848	.377	
80	1.502	.676	.407				
		$C_{T,S} = 0.66$	0		$C_{T,S} = 0.3$	30	
5	1.093	-0.605	0.037	1.399	-0.107	-0.169	
10	1.453	467	.050	1.809	.061	182	
15	1.788	289	.054	2.145	.215	196	
20	2.090	090	.040	2.450	.416	163	
25	2.258	.136	.043	2.579	.626	170	
30	2.111	.260	.073	2.324	.739	118	
35	2.020	.333	.074	2.378	.972	116	
40	1.989	.465	.112	1.849	.928	070	
45	2.084	.732	.095				
50	1.776	.769	.121				

TABLE 26.- AERODYNAMIC DATA FOR UP-AT-TIP ROTATION, INBOARD SLAT ON, FENCES ON, AND  $\,\,\delta_f^{}=20^{O}$ 

α,	$C_{L,s}$	$c_{D,s}$	$C_{m,s}$	$C_{\mathrm{L,s}}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>		
deg		$C_{T,S} = 0.9$	0		$C_{T,s} = 0.80$			
5	0.498	-1.300	0.342	0.566	-1.125	0.277		
10	.688	-1.259	.355	.786	-1.072	.303		
15	.864	-1.177	.369	1.045	987	.306		
20	1.060	-1.079	.362	1.282	847	.291		
25	1.229	953	.365	1.482	697	.294		
30	1.386	794	.356	1.650	502	.272		
35	1.516	641	.353	1.750	307	.256		
40	1.619	463	.344	1.853	105	.262		
45	1.686	286	.339	1.897	.079	.267		
50	1.746	112	.336	1.912	.247	.270		
55	1.767	.048	.337	1.909	.398	.292		
60	1.738	.181	.342	1.876	.531	.313		
65	1.713	.309	.359	1.816	.647	.349		
70	1.683	.424	.378	1.725	.714	.364		
75	1.653	.560	.423	1.592	.720	.407		
80	1.605	.658	.458					
		$C_{T,s} = 0.60$	)	$C_{T,s} = 0.30$				
5	0.694	-0.798	0.153	0.810	-0.343	-0.019		
10	1.005	729	.155	1.240	251	018		
15	1.336	616	.157	1.642	121	006		
20	1.663	453	.136	1.915	.032	013		
<b>2</b> 5	1.929	251	.145	1.911	.189	048		
30	2.084	039	.136	1.691	.400	044		
35	2.139	.159	.137					
40	2.173	.365	.129					
45	2.158	.562	.145		,			

Table 27.- Aerodynamic data for up-at-tip rotation, inboard slat on, fences on, and  $~\delta_f$  =  $40^{\rm o}$ 

α,	$\mathtt{c_{L,s}}$	C <sub>D,s</sub>	C <sub>m,s</sub>	$c_{L,s}$	C <sub>D,s</sub>	C <sub>m,s</sub>	
deg		$C_{T,s} = 0.9$	0	$C_{T,s} = 0.80$			
5	0.663	-1.189	0.268	0.703	-1.037	0.238	
10	.850	-1.147	.295	.952	973	.262	
15	1.036	-1.056	.292	1.215	845	.236	
20	1.219	926	.285	1.482	677	.229	
25	1.389	772	.289	1.706	475	.189	
30	1.559	578	.249	1.881	238	.181	
35	1.662	405	.231	1.948	051	.174	
40	1.746	211	.232	1.982	.137	.181	
45	1.808	032	.239	1.995	.303	.201	
50	1.818	.130	.250	1.957	.430	.229	
55	1.807	.252	.266	1.895	.540	.246	
60	1.777	.363	.291	1.843	.645	.283	
65	1.736	.466	.311	1.778	.747	.307	
70	1.675	.548	.343	1.681	.802	.354	
75	1.633	.644	.389	1.601	.826	.413	
80	1.580	.719	.425				
		$C_{T,s} = 0.66$	Ö	$C_{T,s} = 0.30$			
5	0.985	-0.687	-0.062	1.222	-0.212	-0.132	
10	1.314	585	.064	1.650	071	151	
15	1.687	414	.028	2.021	.099	158	
20	1.996	203	.004	2.380	.280	135	
<b>2</b> 5	2.194	.019	.015	2.312	.461	135	
30	2.293	.245	.005	2.333	.673	164	
35	2.312	.435	.023	2.223	.852	147	
40	2.313	.621	.056				
45	2.239	.755	.076				
50	1.983	.845	.084				
55	1.818	.886	.126		İ		

TABLE 28.- AERODYNAMIC DATA FOR UP-AT-TIP ROTATION, INBOARD SLAT ON, FENCES ON, AND  $\,\,\delta_f^{}=\,60^{O}$ 

α,	$C_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{L,s}$	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg		$C_{T,s} = 0.90$	)	$C_{T,s} = 0.80$			
5	0.705	-1.138	0.257	0.870	-0.948	0.178	
10	.905	-1.076	.267	1.127	860	.177	
15	1.083	968	.259	1.384	700	.151	
20	1.257	833	.261	1.671	506	.118	
25	1.416	632	.234	1.835	299	.118	
30	1.585	445	.203	1.930	107	.132	
35	1.665	258	.191	1.968	.088	.129	
40	1.723	082	.192	1.990	<b>.2</b> 78	.133	
45	1.785	.105	.206	1.955	.417	.156	
50	1.801	.263	.213	1.915	.524	.185	
55	1.773	.408	.223	1.838	.644	.202	
60	1.745	.521	.250	1.802	.752	.239	
65	1.678	.553	.292	1.735	.849	.265	
70	1.625	.607	.337	1.639	.888	.312	
75	1.580	.680	.374	1.526	.851	.369	
80	1,508	.719	.421		1		
		$C_{T,S} = 0.60$	)		$C_{T,s} = 0.3$	30	
5	1.097	-0.593	0.044	1.432	-0.071	-0.183	
10	1.448	456	.019	1.815	.077	183	
15	1.773	286	003	2.151	.212	164	
20	2.044	082	014	2.471	.430	158	
25	2.225	.145	004	2.388	.611	181	
30	2.312	.374	001	2.370	.827	182	
35	2.317	.554	.008	2.269	.986	162	
40	2.291	.715	.046				
45	2.220	.827	.092				
50	2.157	.956	.111				
55	2.050	1.045	.145				
60	1.532	.890	.183				

TABLE 29.- AERODYNAMIC DATA FOR UP-AT-TIP ROTATION, FULL-SPAN SLAT ON, FENCES ON, AND  $\,\,\delta_f$  =  $20^{O}$ 

$\alpha$ ,	CL,s	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	$c_{L,s}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
deg	$C_{T,s} = 0.90$			$C_{T,s} = 0.80$		
5	0.476	-1.292	0.351	0.543	-1.121	0.279
10	.670	-1.239	.349	.781	-1.065	.293
15	.847	-1.168	.362	1.028	968	.299
20	1.039	-1.073	.362	1.280	841	.293
25	1.216	948	.353	1.492	681	.288
30	1,363	801	.364	1.672	500	.272
35	1.499	637	.347	1.792	300	.267
40	1.600	467	.341	1.872	104	.268
45	1.678	285	.331	1.915	.075	.283
50	1.719	111	.328	1.925	.240	.290
55	1.747	.047	.341	1.926	.396	.310
60	1.727	.179	.342	1.895	.536	.340
65	1.702	.304	.367	1.841	.654	.373
70	1.677	.440	.380	1.766	.751	.391
75	1.654	.559	.424	1.672	.781	.445
80	1,612	.676	.458	1.580	.820	.475
		$C_{T,s} = 0.6$	0		$C_{T,s} = 0.$	30
5	0.650	-0.810	0.149	0.704	-0.340	0.001
10	.980	734	.150	1.190	251	035
15	1.319	620	.156	1.619	119	021
20	1.660	439	.150	2.019	.045	015
25	1.937	270	.162	2.356	.282	025
30	2.077	036	.146	2.546	.542	018
35	2.157	.159	.152	2.562	.761	025
40	2.229	.372	.169	2.597	.952	.006
45	2.247	.558	.183	2,565	1.115	.021
50	2.214	.709	.205	2.505	1.241	.069
55	2.179	.870	.230	1.997	1.118	.085
60	2.131	.989	.272			
65	2.027	1.068	.303			

Table 30.- Aerodynamic data for up-at-tip rotation,  $\mbox{full-span slat on, fences on, and} \quad \delta_f = 40^{O}$ 

$\alpha$ ,	C <sub>L,s</sub>	$C_{\mathrm{D,s}}$	C <sub>m,s</sub>	$C_{\mathrm{L,s}}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>
deg		$C_{T,S} = 0.9$	0		$C_{T,s} = 0.$	80
5	0,628	-1.213	0.279	0.714	-1.040	0.197
10	.819	-1.145	.288	.971	950	.212
15	1,005	-1.062	.290	1.247	821	.189
20	1.197	935	.278	1.515	653	.171
25	1.371	775	.277	1.744	443	.148
30	1.534	587	.252	1.896	223	.154
35	1.641	410	.225	1.961	033	.144
40	1.746	195	.227	1.997	.153	.163
45	1.792	016	.228	2.009	.329	.179
50	1.813	.143	.241	1.968	.461	.213
55	1.794	.279	.256	1.933	.581	.245
60	1.742	.384	.269	1.855	.693	.247
65	1.706	.486	.304	1.807	.795	.287
70	1.657	.580	.327	1.721	.861	.338
75	1.611	.662	.384	1.626	.867	.403
80	1.555	.738	.418			
•		$C_{\mathrm{T,s}} = 0.60$	)	·	$C_{T,S} = 0.$	30
5	0.878	-0.703	0.075	1.041	-0.238	-0.098
10	1.257	601	.062	1.585	081	147
15	1.648	435	.032	2.035	.080	152
20	1.987	211	.012	2.419	.293	139
25	2.194	.013	.014	2.679	.541	140
30	2.304	.246	.013	2.745	.815	157
35	2.355	.447	.027	2.731	1.014	118
40	2.341	<b>.62</b> 8	.058	2.701	1.187	091
45	2.299	.766	.098	2.620	1.312	029
50	2.230	.906	.127			
55	2.177	1.036	.179			
60	<b>2.</b> 086	1.118	.223			
65	1.894	1.117	.263			
70	1.520	1.000	.273			

table 31.- Aerodynamic data for up-at-tip rotation, full-span slat on, fences on, and  $~\delta_{\rm f}$  =  $60^{\rm o}$ 

$  \alpha$	$C_{L,s}$	$c_{\mathrm{D,s}}$	$c_{m,s}$	$\mathtt{c}_{\mathtt{L},\mathtt{s}}$	$c_{\mathrm{D,s}}$	C <sub>m,s</sub>	
deg	$C_{T,s} = 0.90$			$C_{T,s} = 0.80$			
5	0.686	-1.154	0.263	0.799	-0.966	0.198	
10	.874	-1.065	.272	1.085	867	.187	
15	1.075	973	.272	1.353	696	.151	
20	1.266	814	.258	1.635	499	.129	
25	1.441	637	.243	1.829	286	.126	
30	1.597	428	.206	1.920	098	.137	
35	1.706	241	.214	1.941	.088	.138	
40	1.766	048	.210	1.989	.288	.149	
45	1.793	.107	.231	1.951	.425	.175	
50	1.783	.259	.240	1.903	.535	.201	
55	1.771	.405	.254	1.843	.658	.214	
60	1.717	.493	.269	1.796	.771	.248	
65	1.660	.535	.311	1.732	.870	.276	
70	1.609	.610	.344	1.627	.913	.328	
75	1.551	.664	.384	1.542	.891	.389	
80	1.500	.722	.431				
		$C_{T,s} = 0.6$	30	$C_{T,s} = 0.30$			
5	0.990	-0.630	0.048	1.278	-0.122	-0.135	
10	1.402	491	.031	1.736	.027	178	
15	1.772	294	006	2.140	.207	165	
20	2.033	095	.006	2.493	.412	143	
25	2.214	.144	.015	2.678	.669	144	
30	2.310	.370	.023	2.683	.923	149	
35	2.314	.564	.039	2.655	1.111	129	
40	2.279	.719	.074	2.657	1.284	083	
45	2.208	.837	.115	2.523	1.372	028	
50	2.153	.966	.153				
55	2.073	1.062	.180		l		

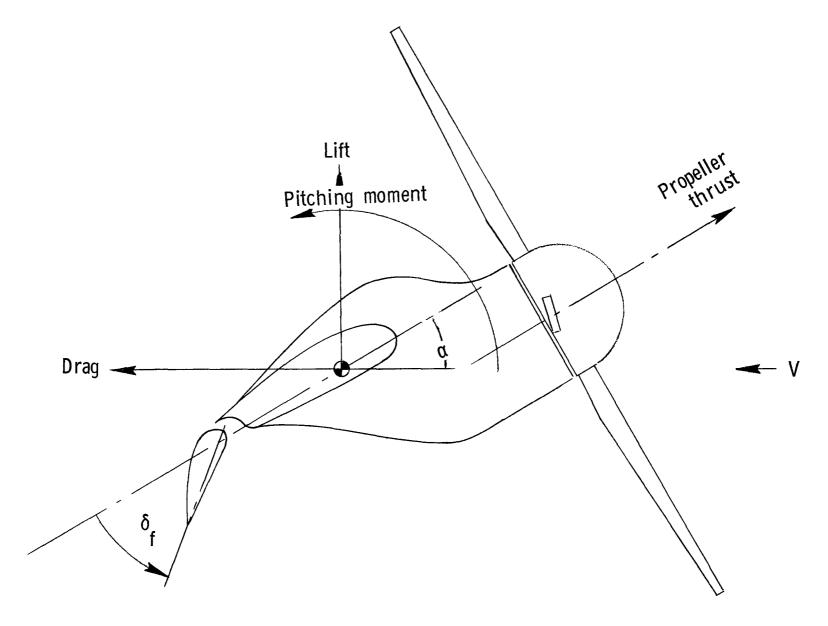
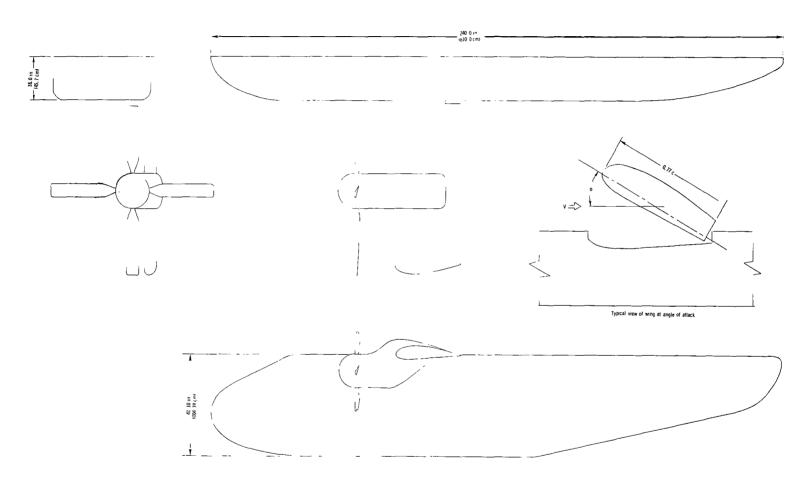
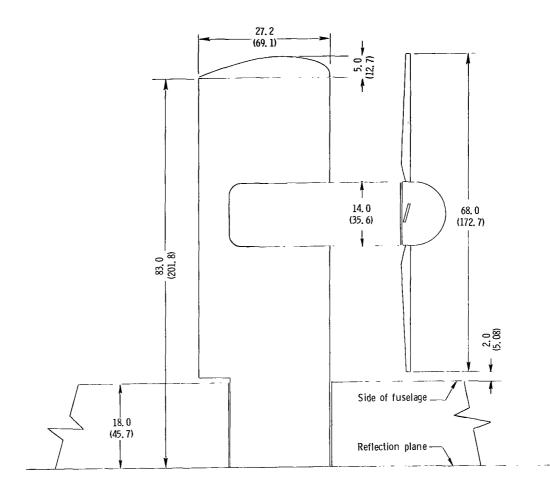


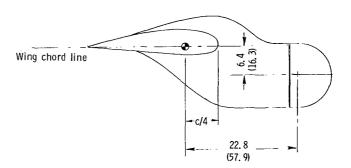
Figure 1.- The positive sense of forces, moments, and angles.



(a) Three-view drawing of the wing and fuselage.

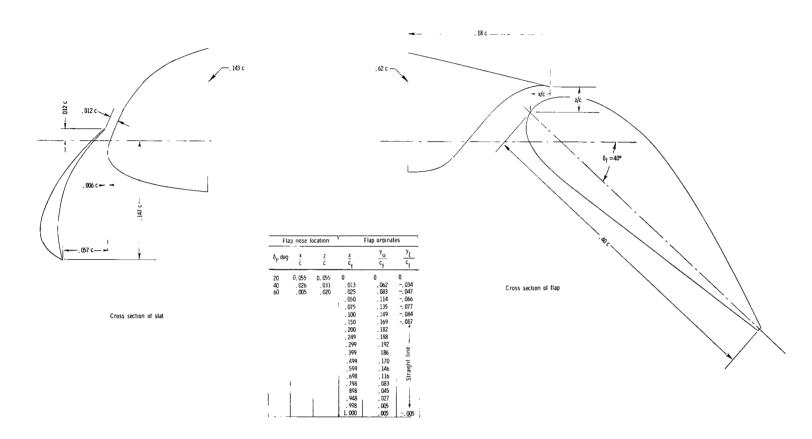
Figure 2.- Three-view drawing and principal dimensions of the model.





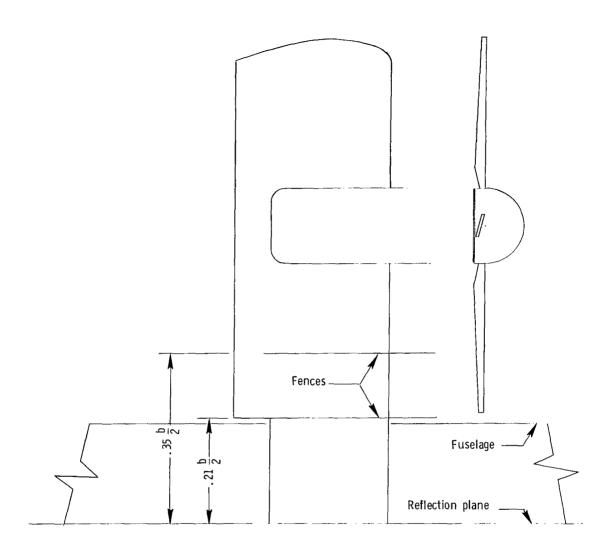
(b) Principal dimensions of wing in inches and parenthetically in centimeters.

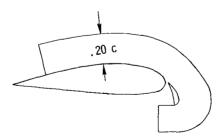
Figure 2.- Concluded.



(a) Cross-sectional view of the slat and flap.

Figure 3.- Cross-sectional views of the slat, flap, and fences and fence location.

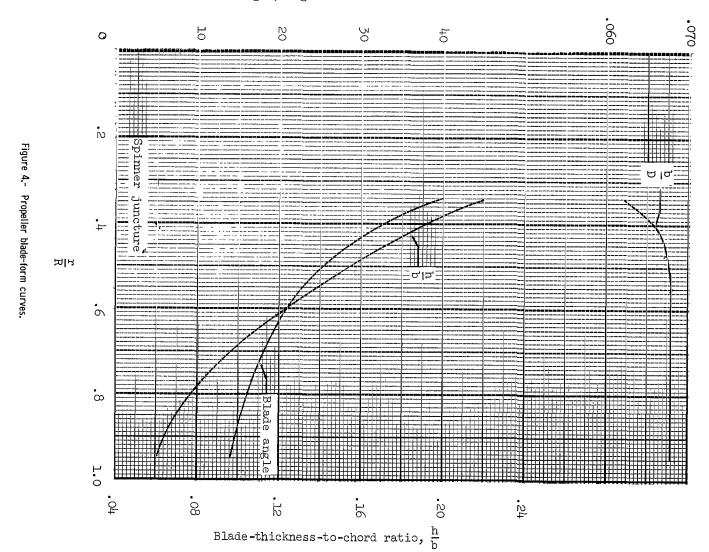




(b) Sectional view and location of fences.

Figure 3.- Concluded.

Blade angle, deg



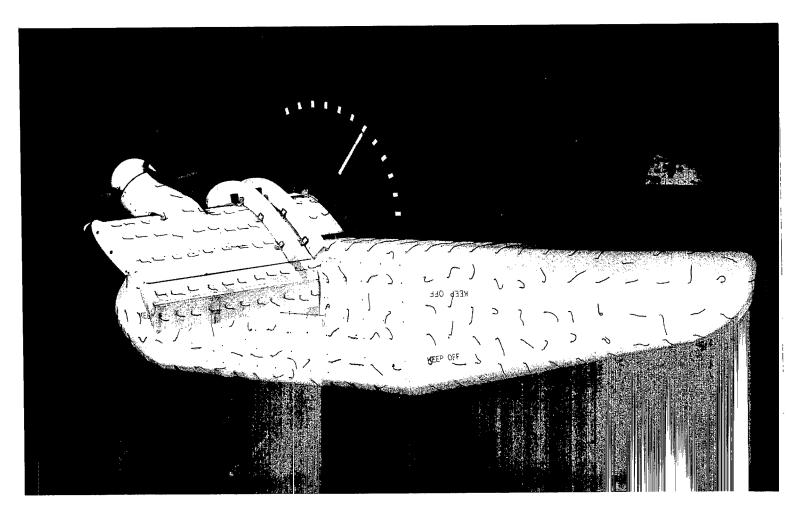
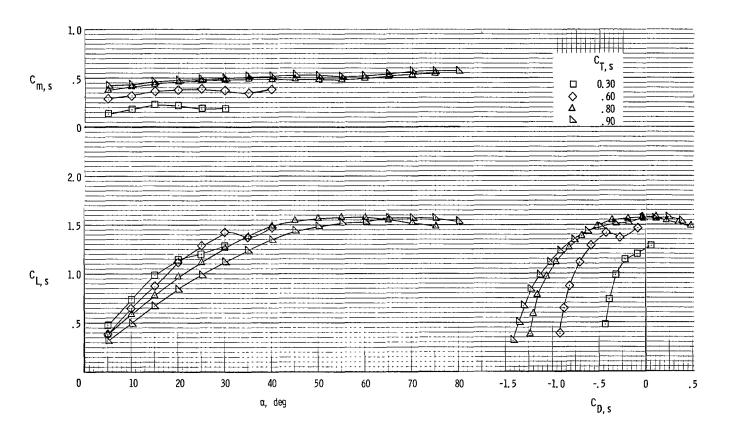
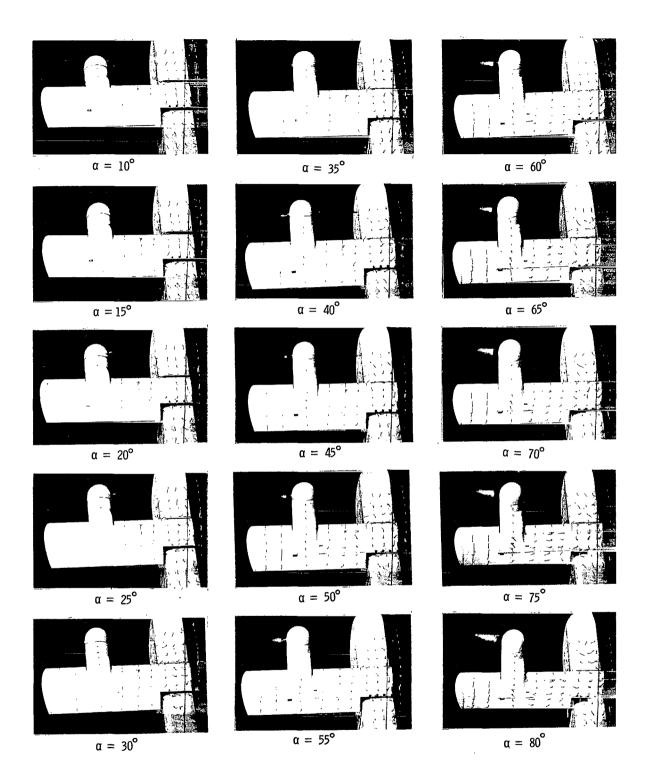


Figure 5.- Photograph of model.

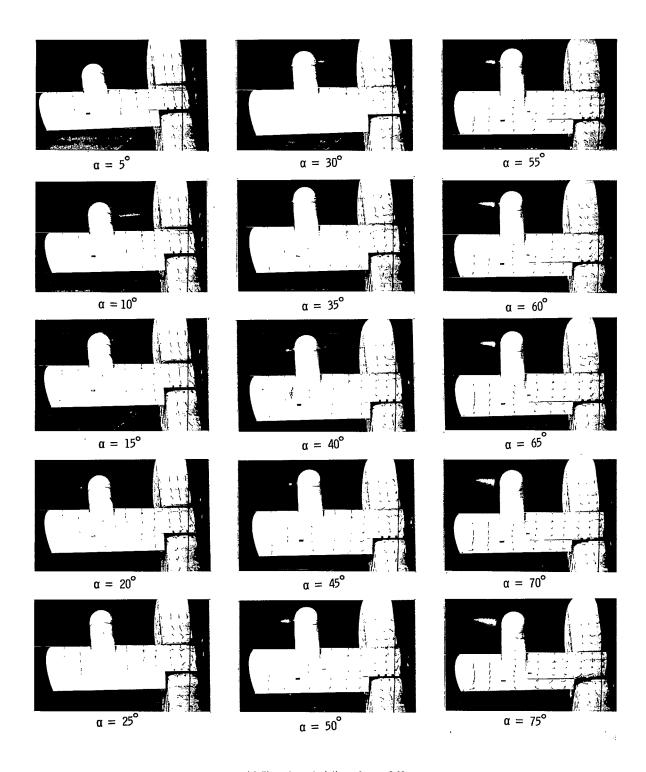


(a) Aerodynamic characteristics.

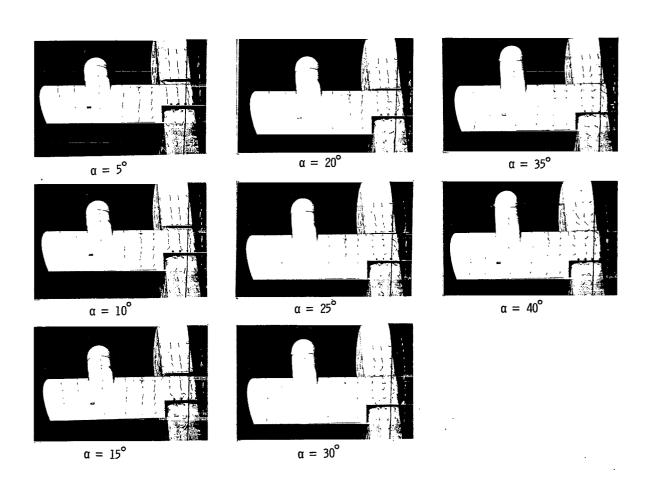
Figure 6.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, and  $\delta_f = 0^\circ$ .



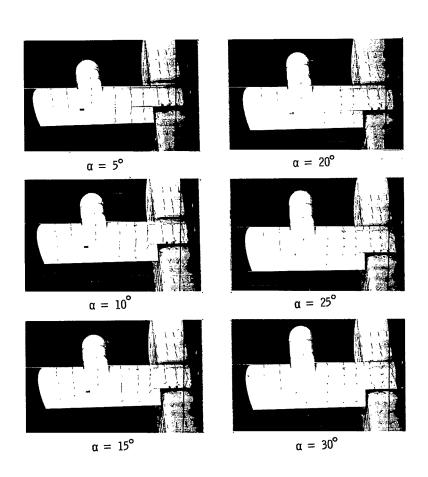
(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 6.- Continued.



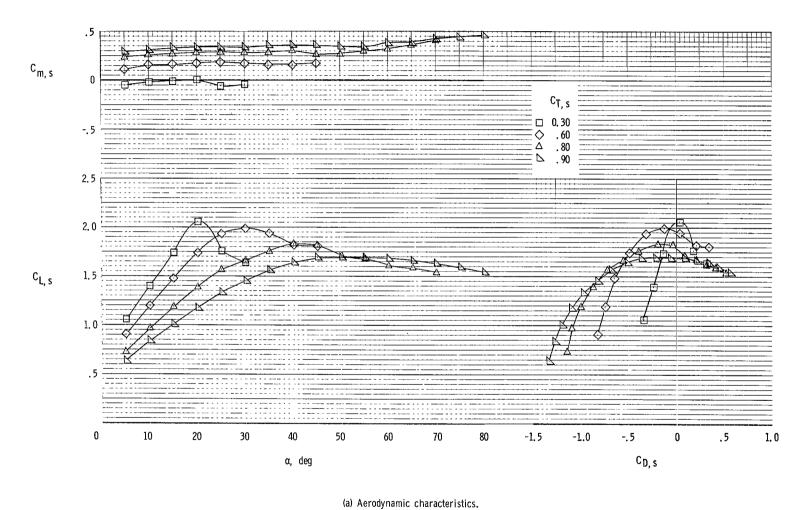
(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 6.- Continued.



(d) Flow characteristics;  $C_{\text{T,S}} = 0.60$ . Figure 6.- Continued,

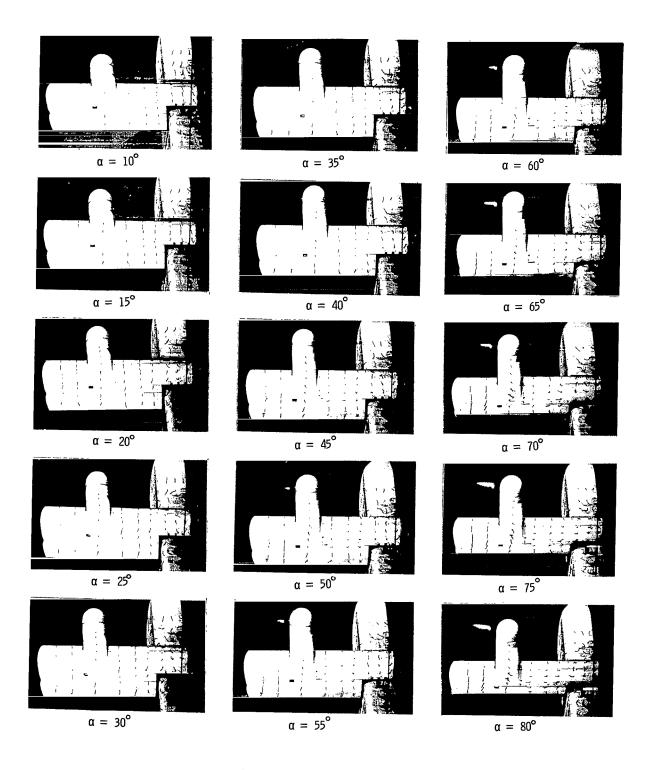


(e) Flow characteristics;  $C_{\mbox{\scriptsize T,S}}=0.30.$  Figure 6.- Concluded.

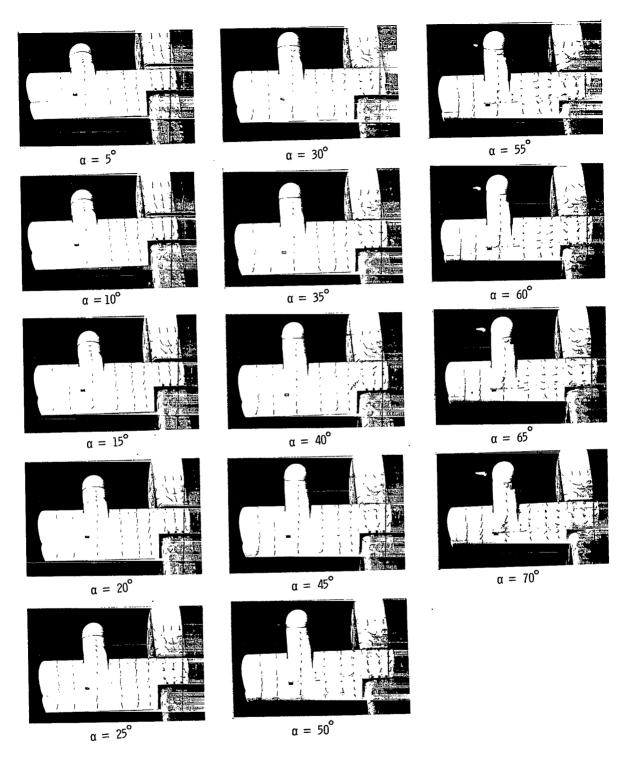


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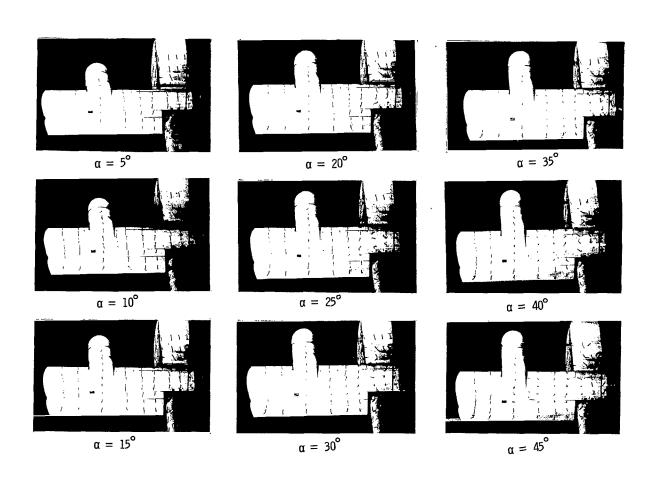
Figure 7.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, and  $\delta_f = 20^\circ$ .



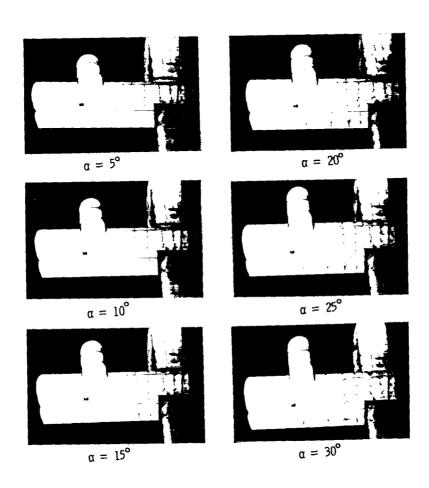
(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 7.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 7.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 7.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 7.- Concluded.

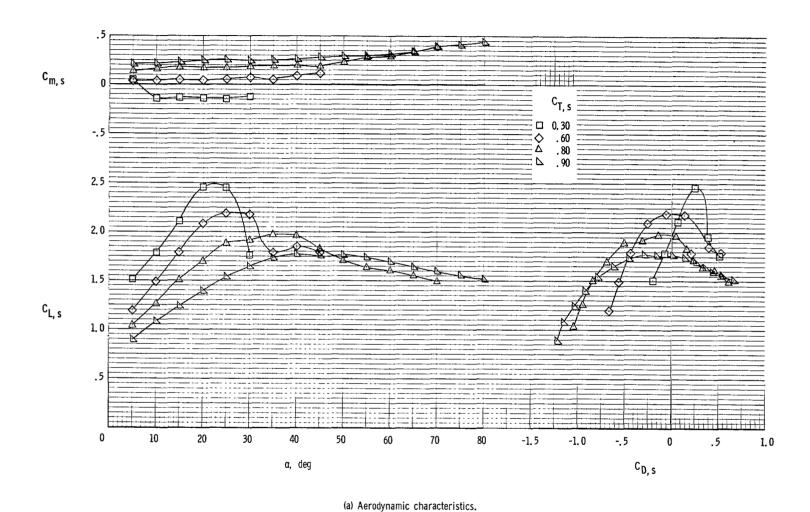
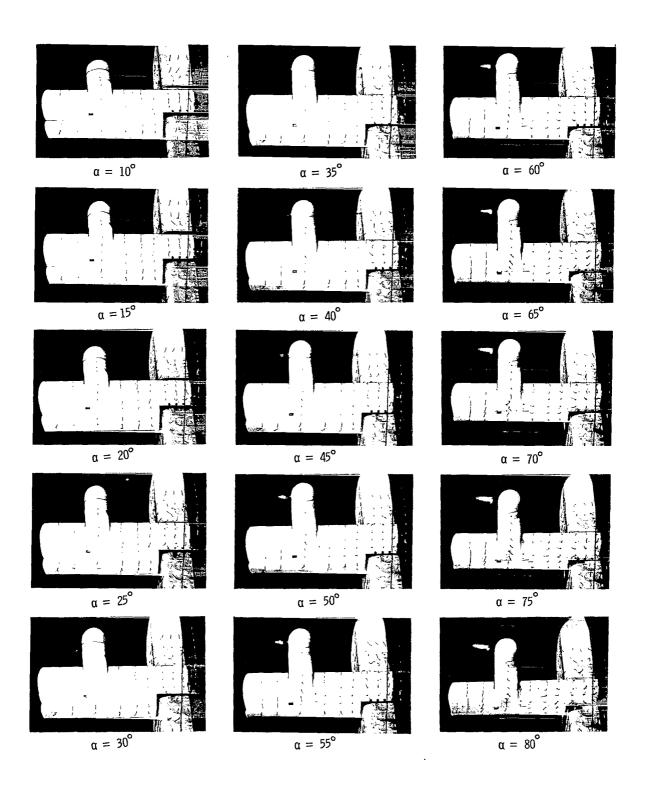
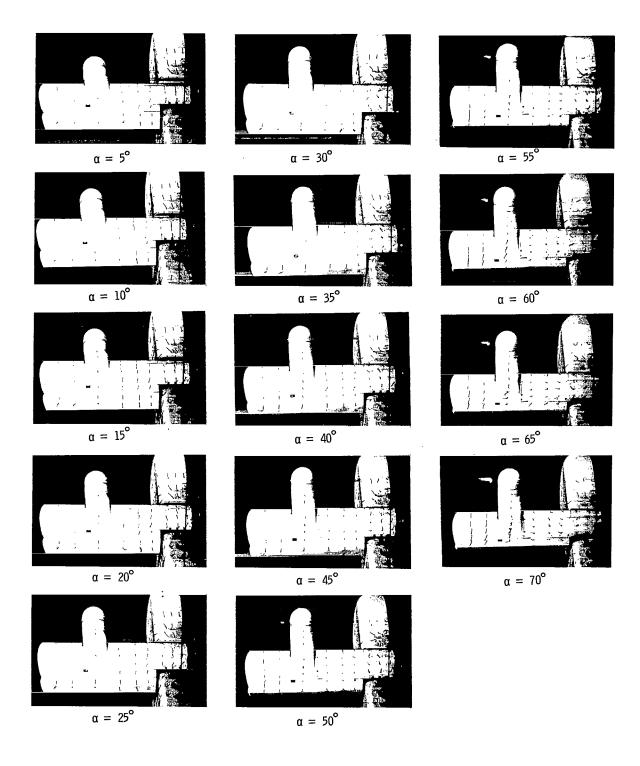


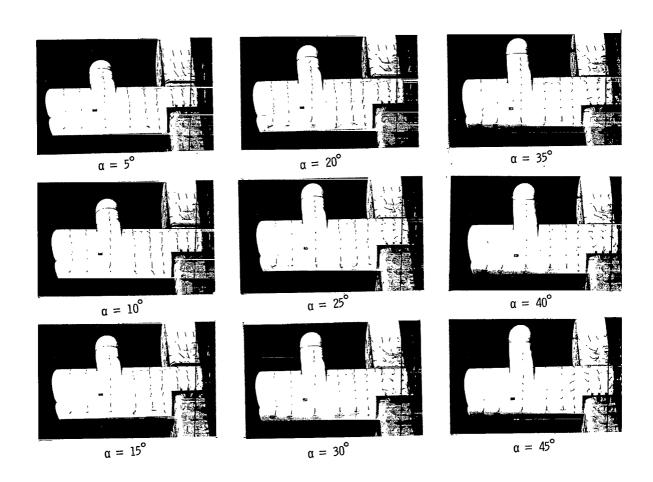
Figure 8.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, and  $\delta_f = 40^\circ$ .



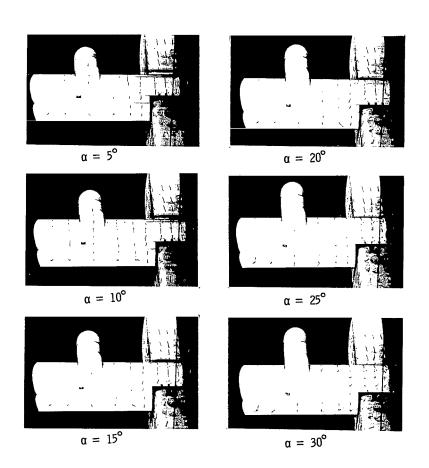
(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 8.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 8.- Continued.



(d) Flow characteristics;  $C_{\mbox{\scriptsize T,S}}=0.60.$  Figure 8.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ .

Figure 8.- Concluded.

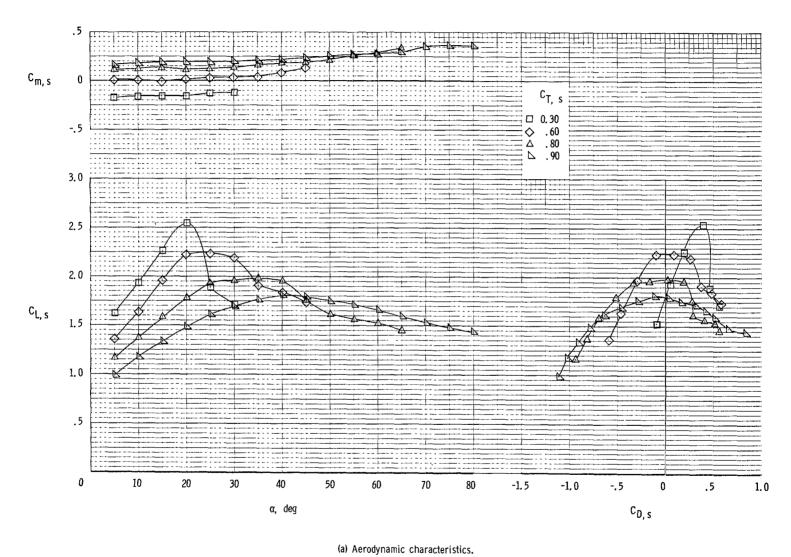
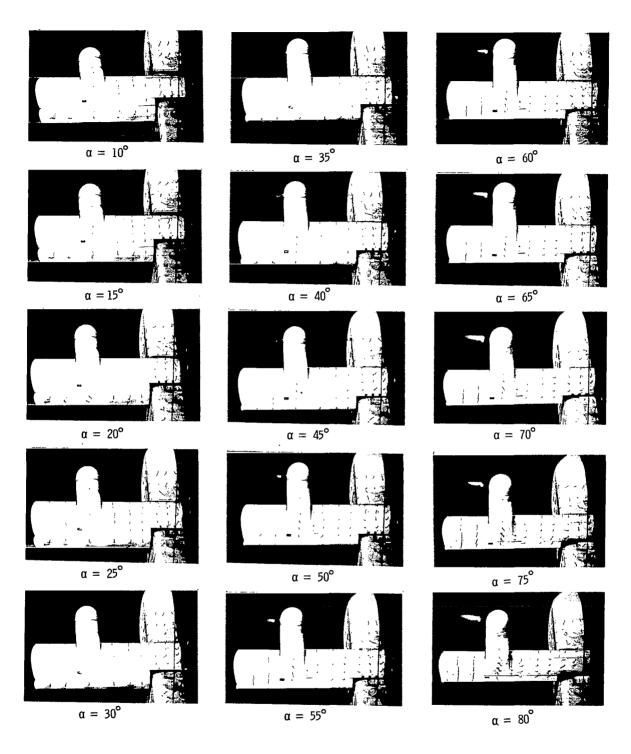
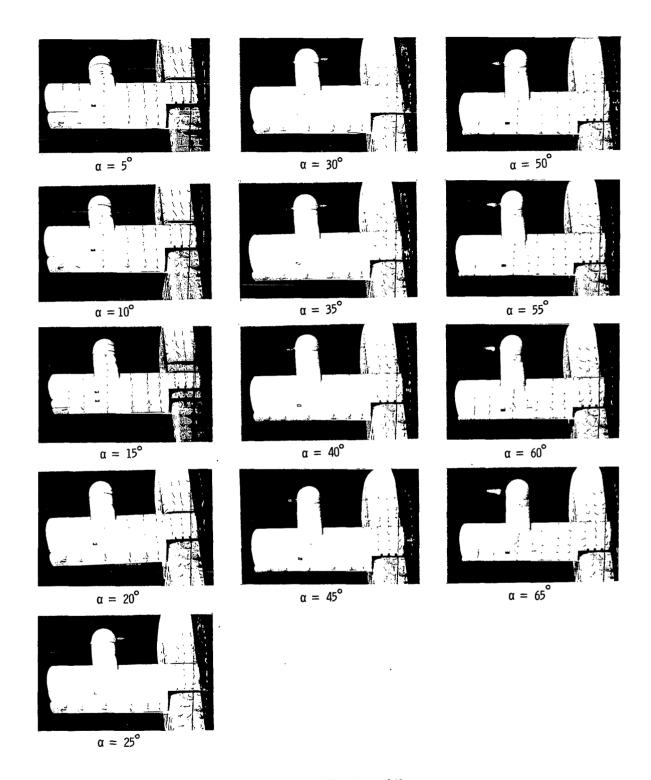


Figure 9.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, and  $\delta_f = 60^\circ$ .

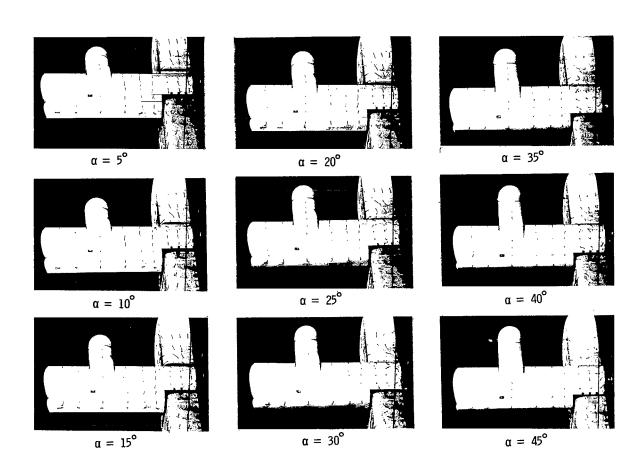


(b) Flow characteristics;  $C_{\text{T,S}} = 0.90$ . Figure 9.- Continued.

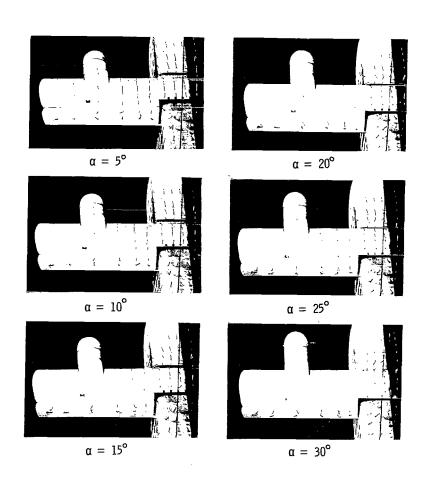
**J**\_\_



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 9.- Continued.

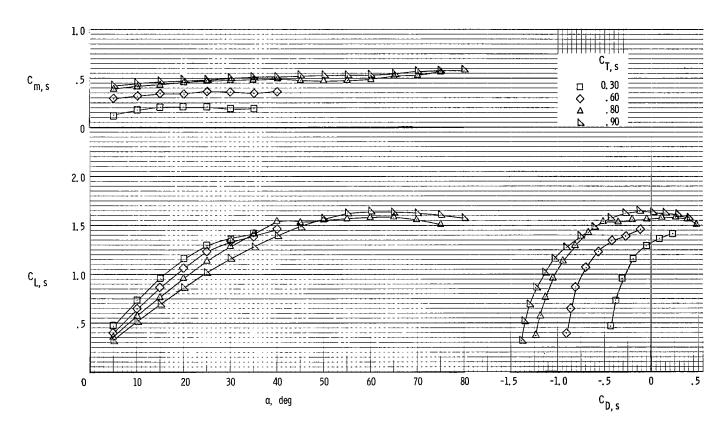


(d) Flow characteristics;  $C_{T,s} = 0.60$ . Figure 9.- Continued.



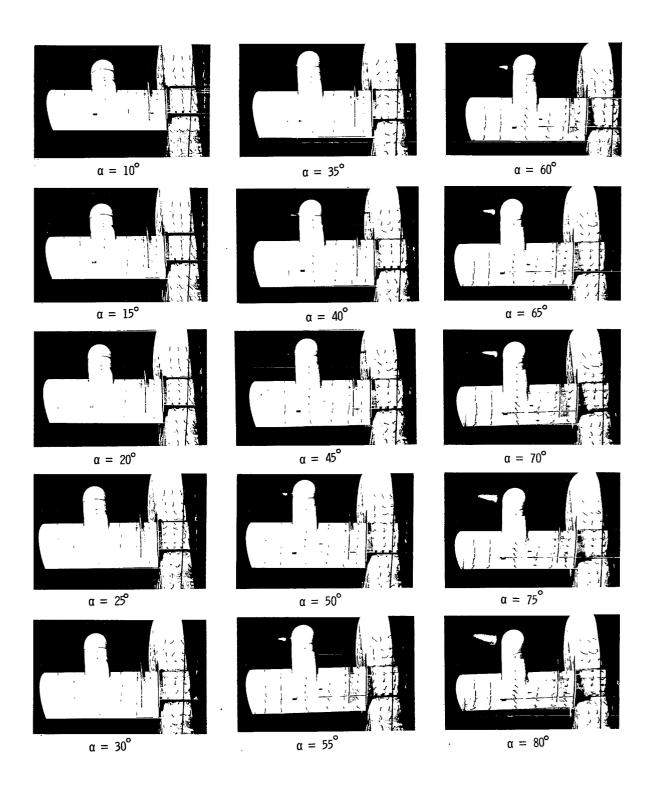
(e) Flow characteristics;  $C_{T,S} = 0.30$ .

Figure 9.- Concluded.

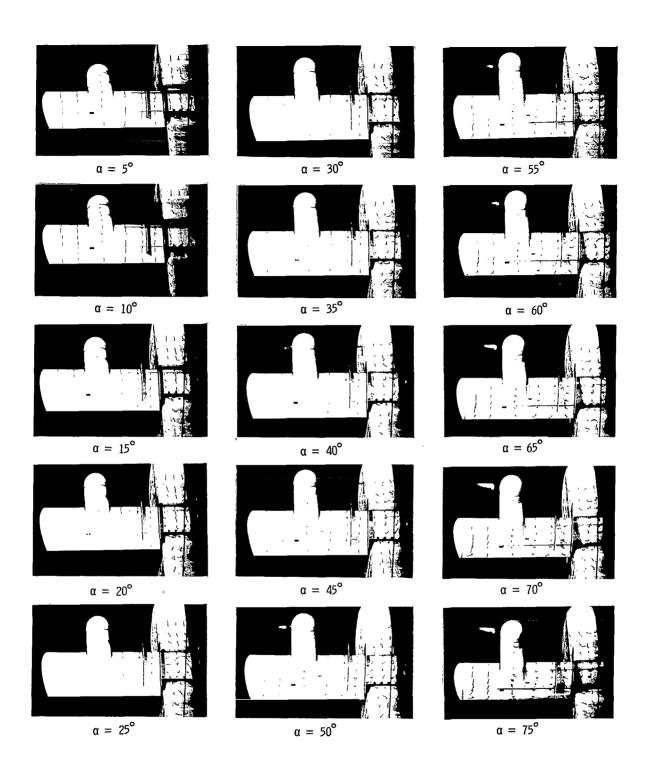


(a) Aerodynamic characteristics.

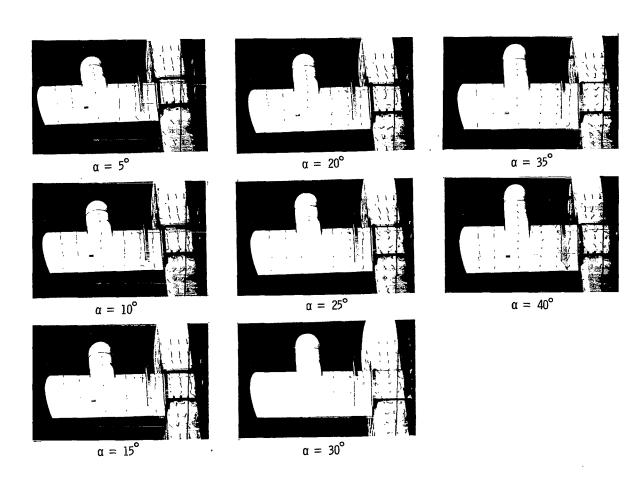
Figure 10.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, fences on, and  $\delta_f = 0^\circ$ .



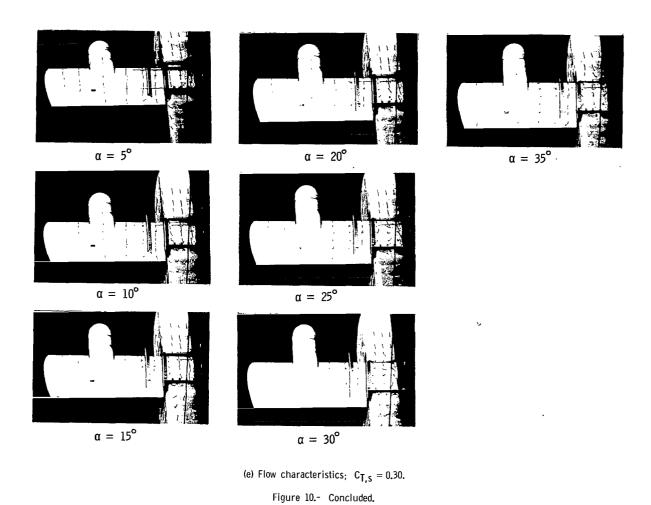
(b) Flow characteristics;  $C_{\text{T,S}} = 0.90$ . Figure 10.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 10.- Continued.



(d) Flow characteristics;  $C_{T,S}=0.60$ . Figure 10.- Continued.



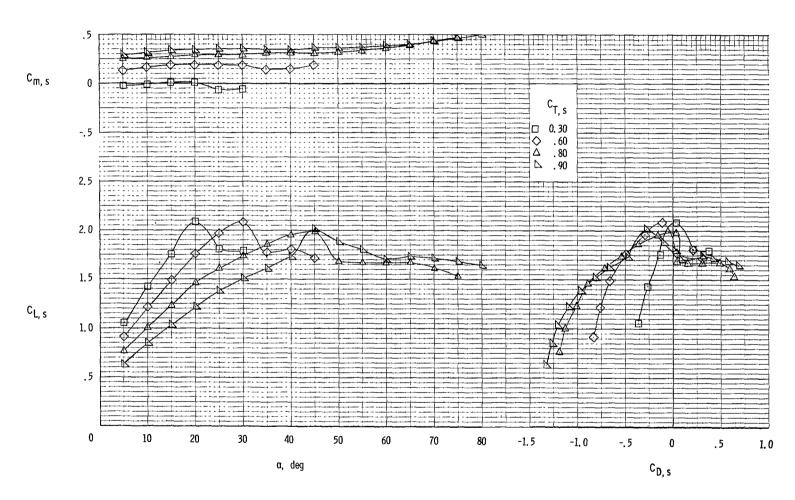
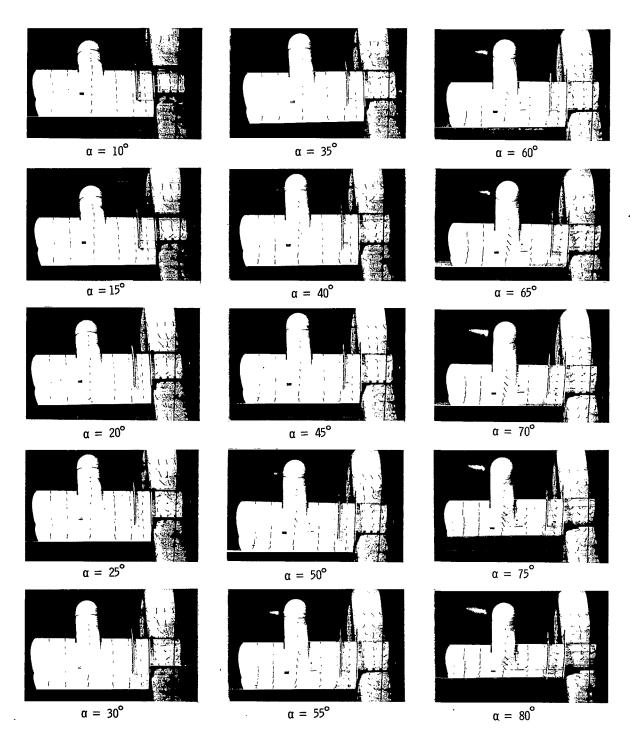
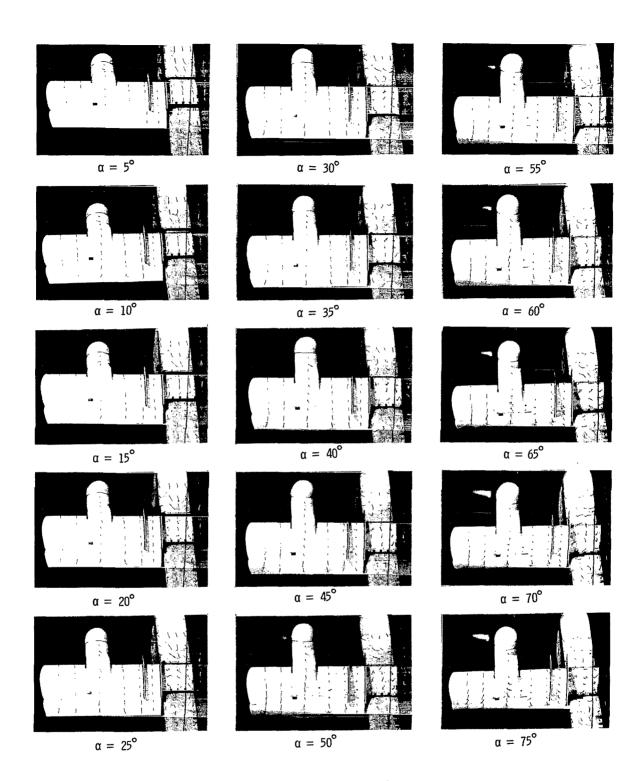


Figure 11.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, fences on, and  $\delta_f = 20^{\circ}$ .

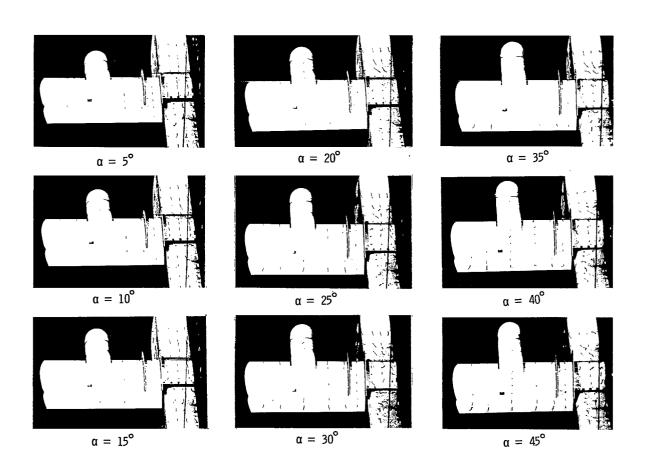


(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 11.- Continued.

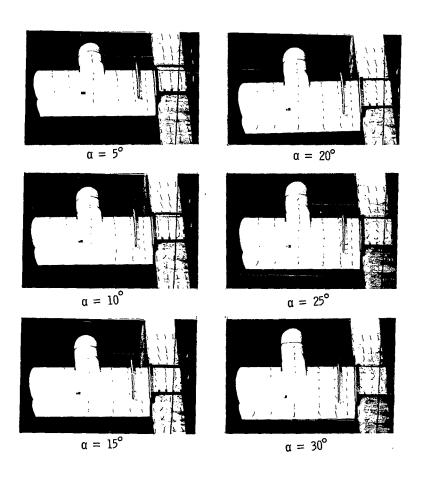


(c) Flow characteristics;  $C_{T,s} = 0.80$ . Figure 11.- Continued.

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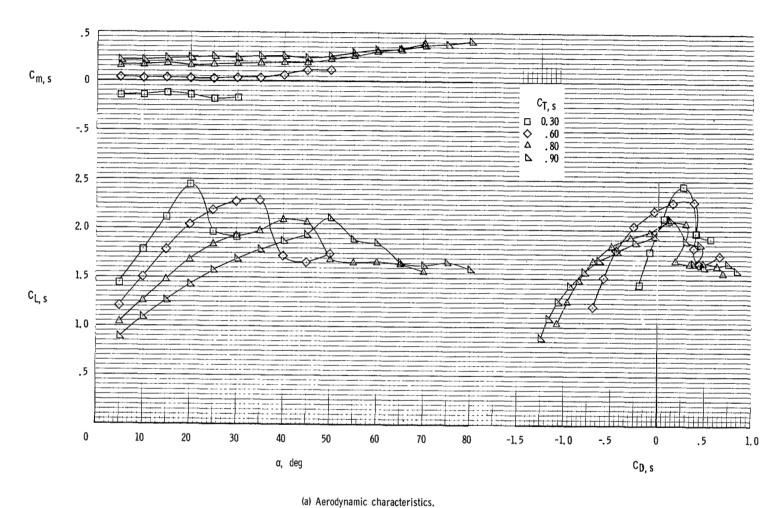


(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 11.- Continued.



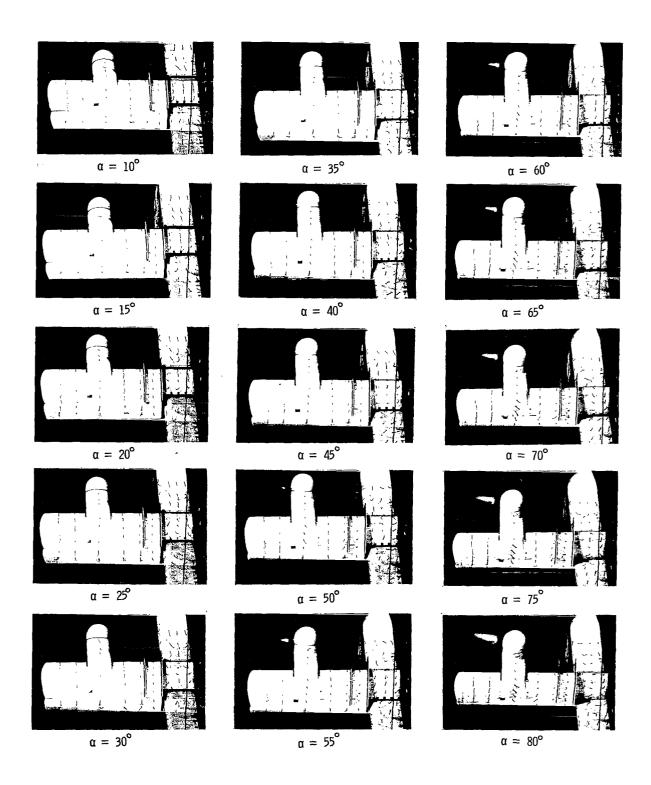
(e) Flow characteristics;  $C_{T,s} = 0.30$ .

Figure 11.- Concluded.

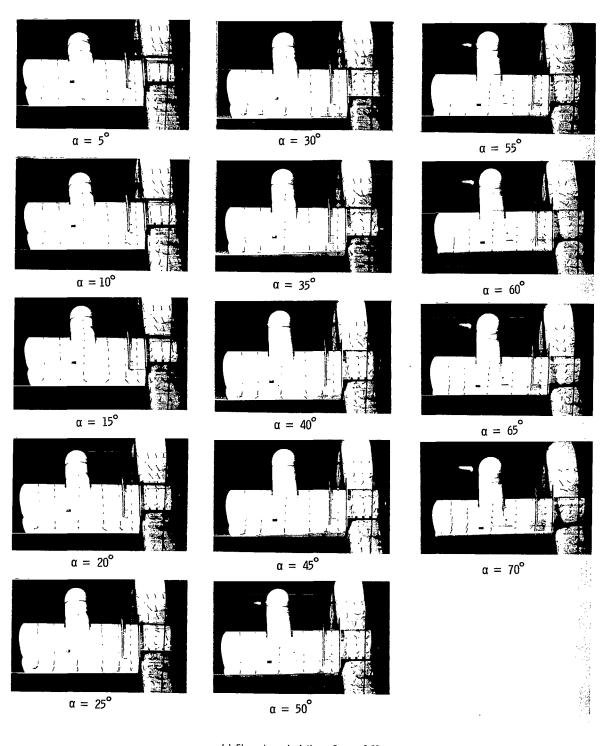


tar Aerodynamic Characteristics.

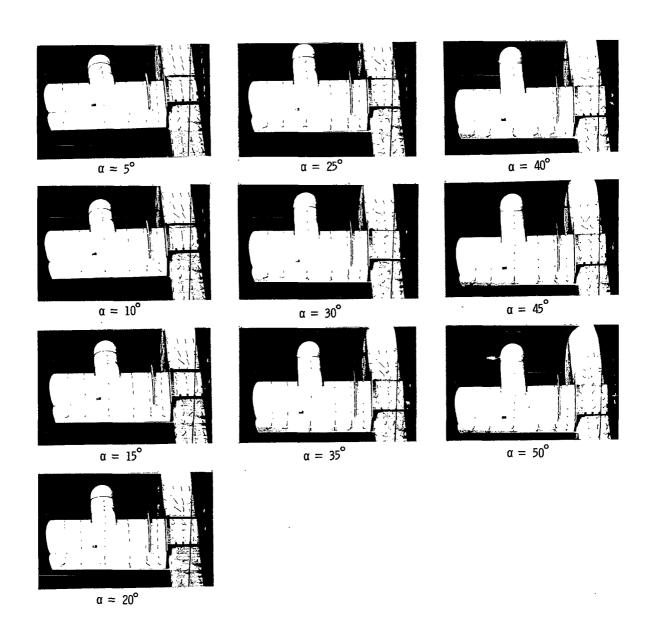
Figure 12.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, fences on, and  $\delta_f = 40^\circ$ .



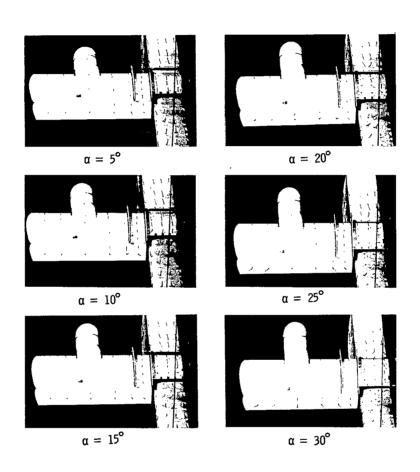
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 12.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 12.- Continued.



(d) Flow characteristics;  $c_{T,s} = 0.60$ . Figure 12.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ .

Figure 12.- Concluded.

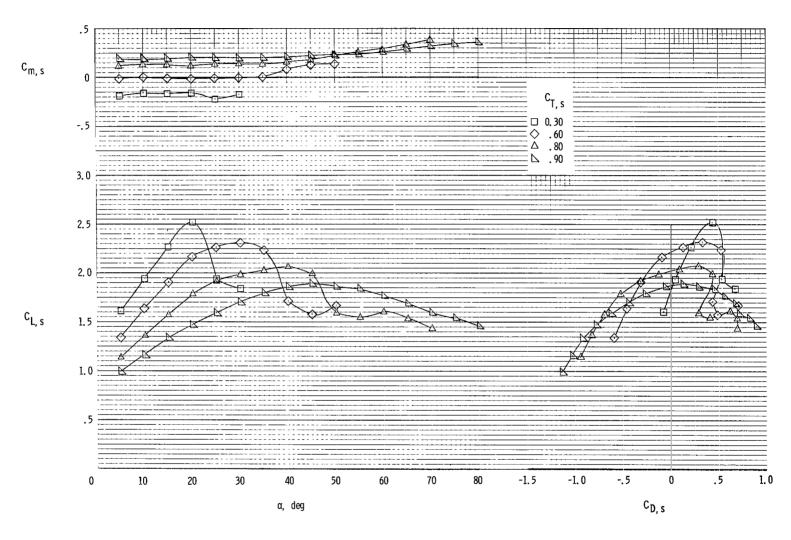
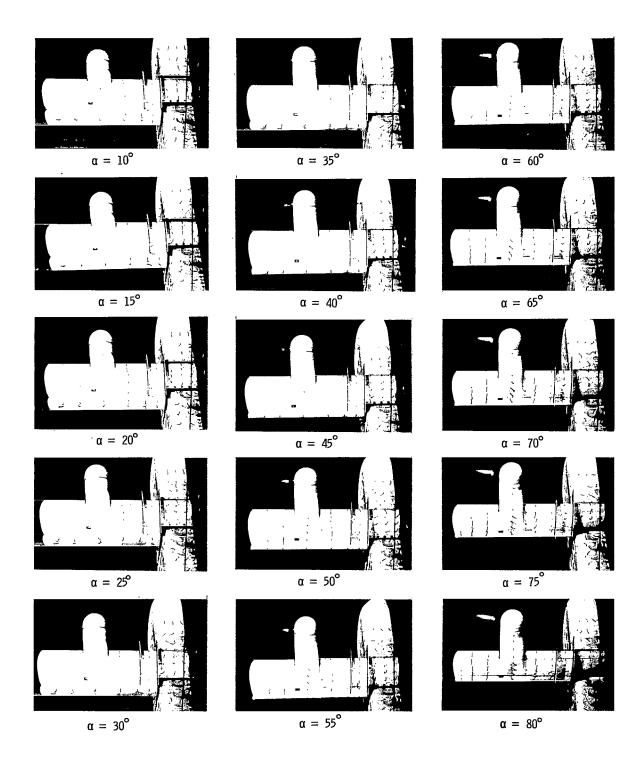
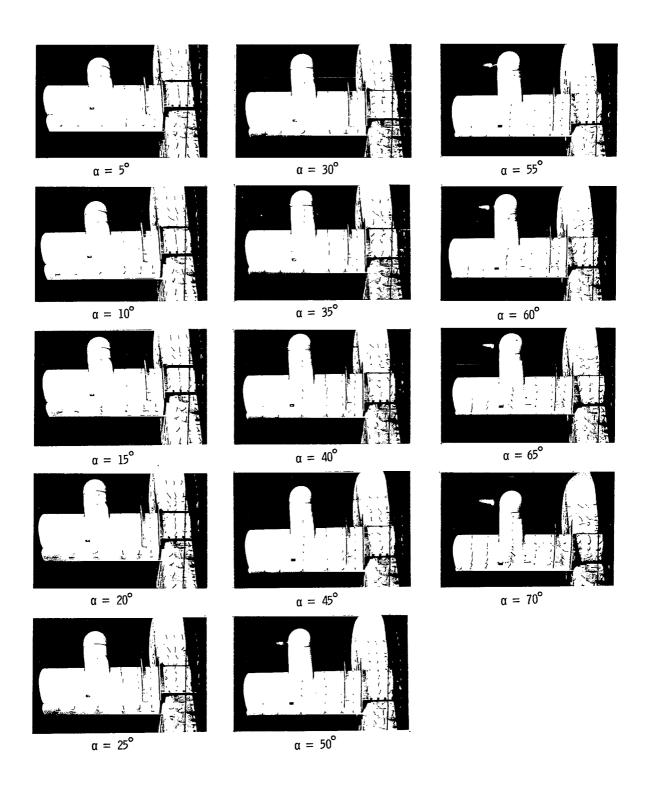


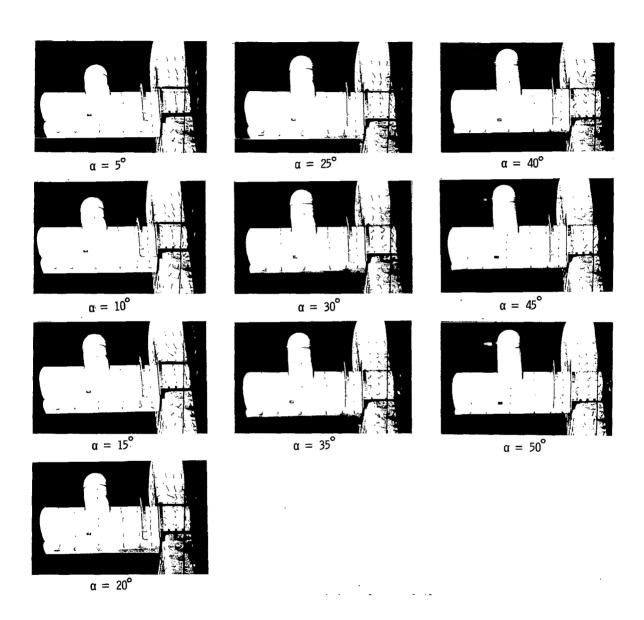
Figure 13.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, basic leading edge, fences on, and  $\delta_f = 60^\circ$ .



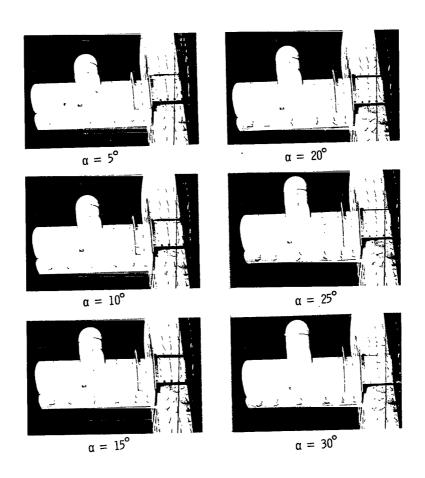
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 13.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 13.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 13.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 13.- Concluded.

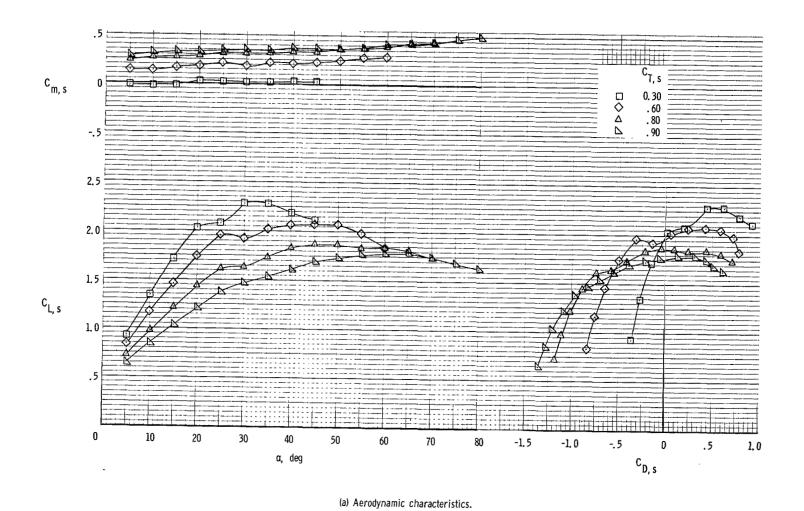
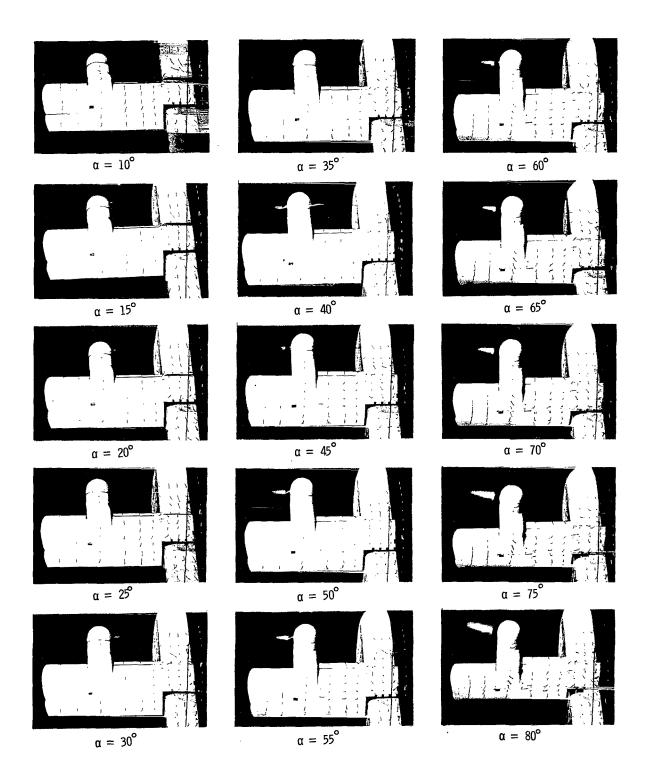
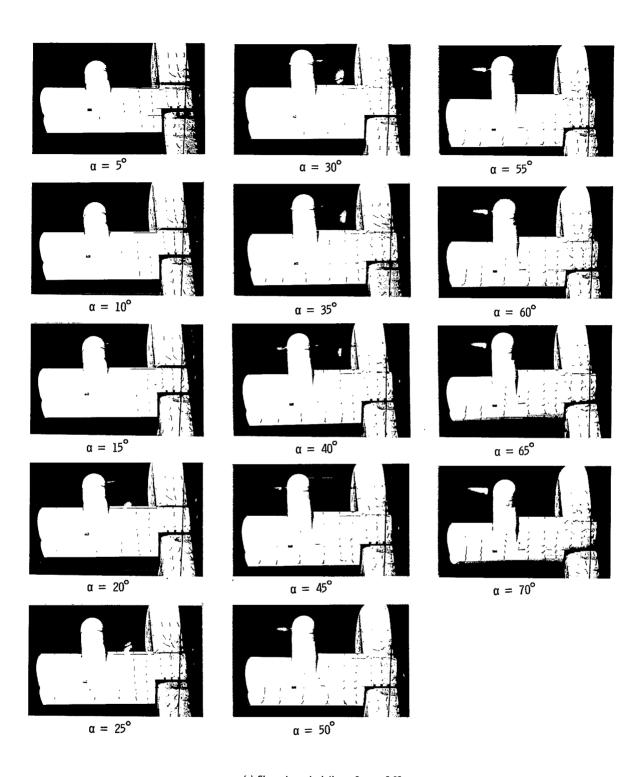


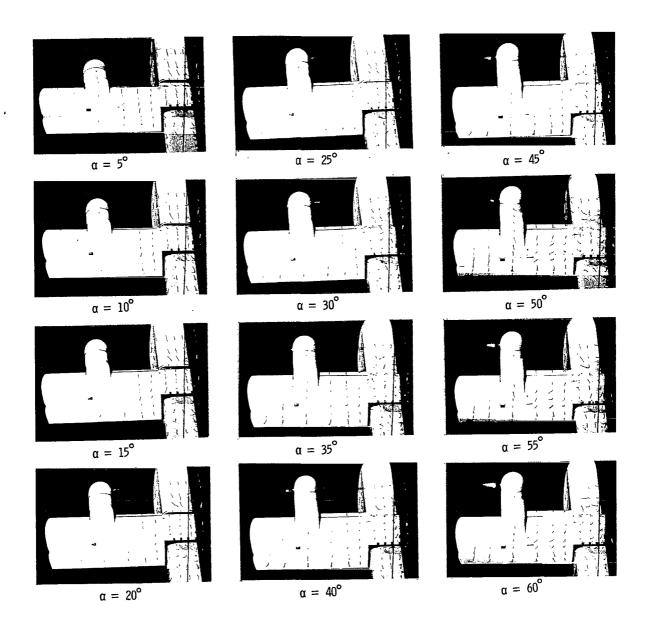
Figure 14.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, inboard slat on, and  $\delta_f=20^\circ$ .



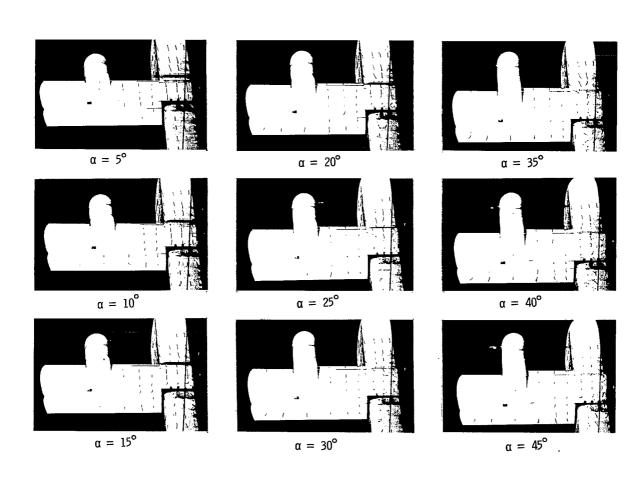
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 14.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 14.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 14.- Continued.



(e) Flow characteristics;  $C_{\mbox{\scriptsize T,S}}=0.30$ . Figure 14.- Concluded.

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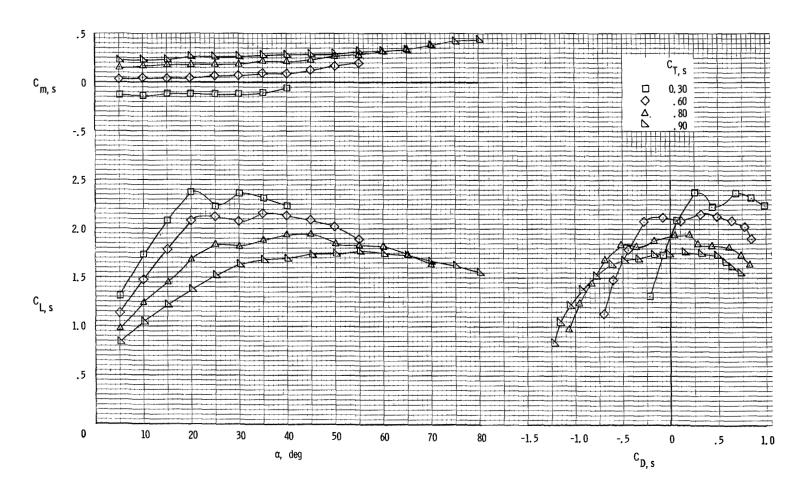
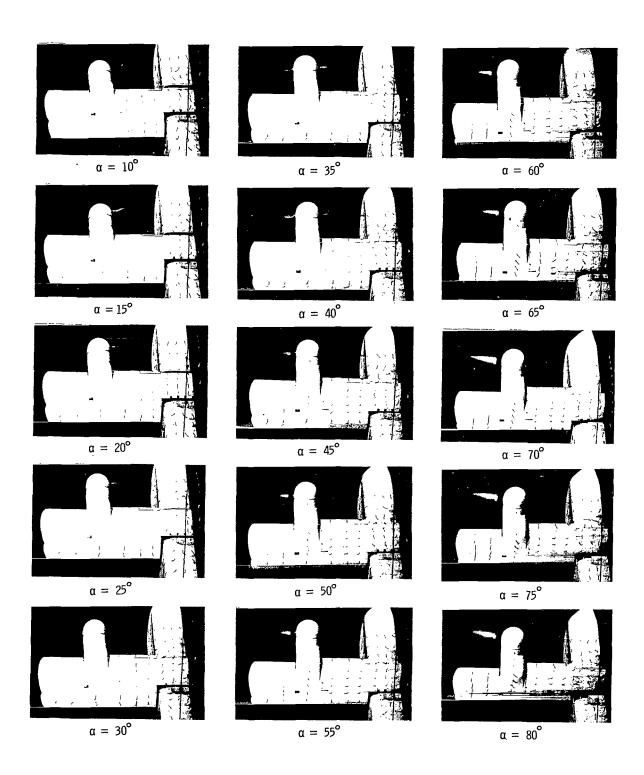
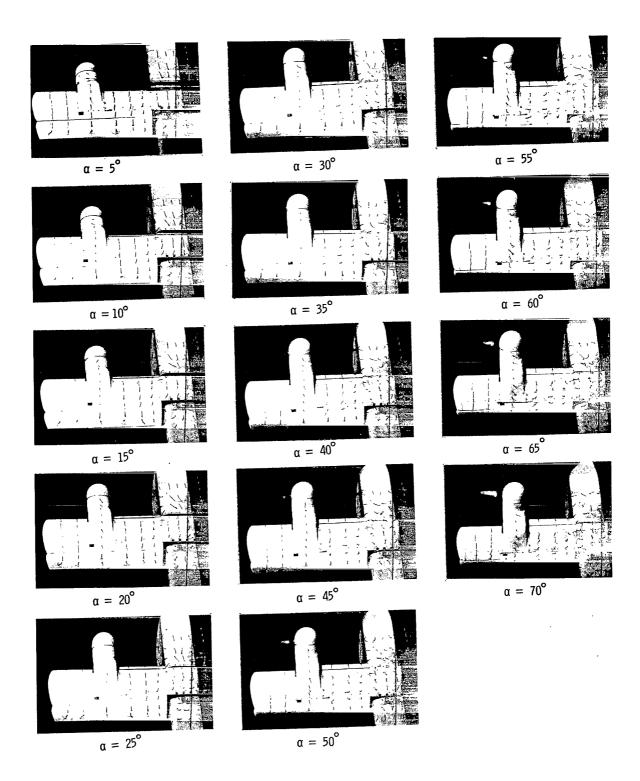


Figure 15.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, inboard slat on, and  $\delta_f = 40^\circ$ .



(b) Flow characteristics;  $C_{\text{T,S}} = 0.90$ . Figure 15.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 15.- Continued.

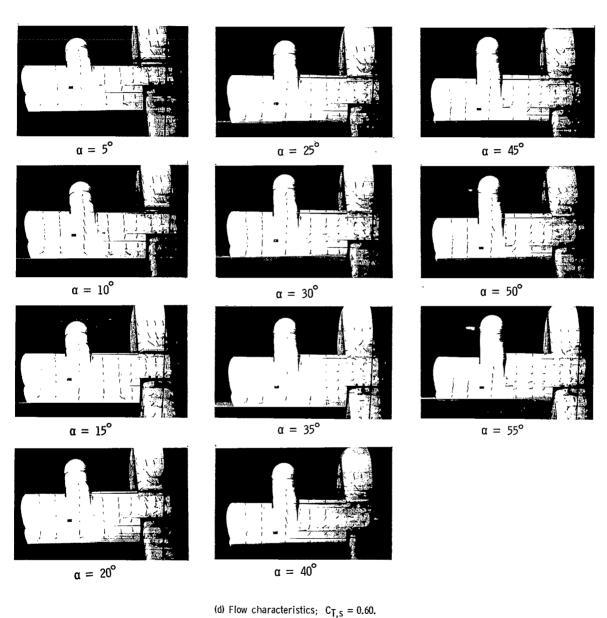
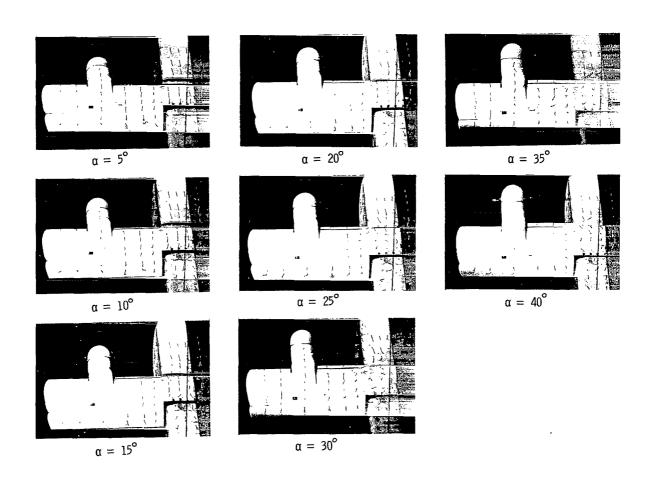


Figure 15.- Continued.



(e) Flow characteristics;  $C_{T,S}=0.30$ . Figure 15.- Concluded.

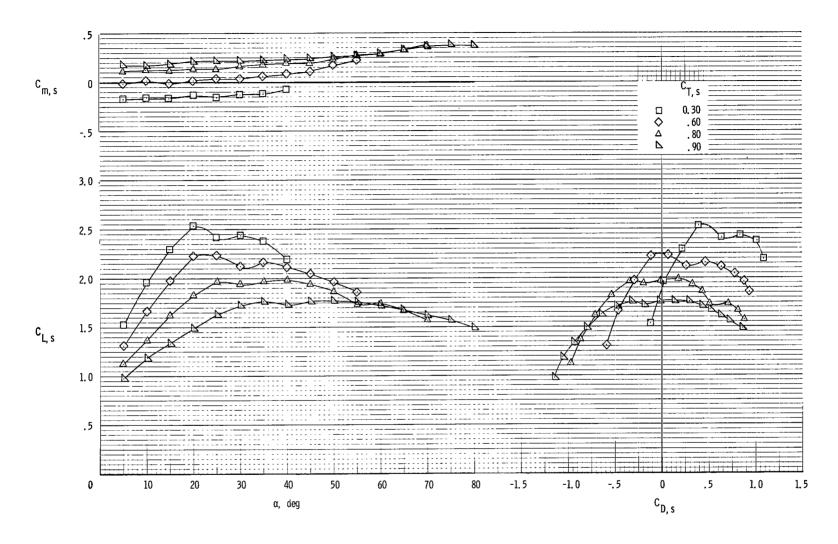
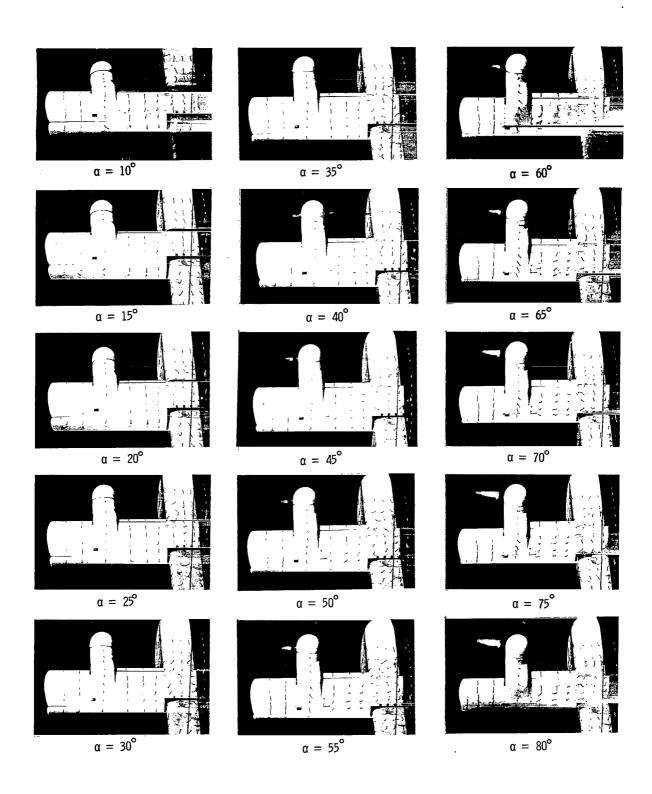
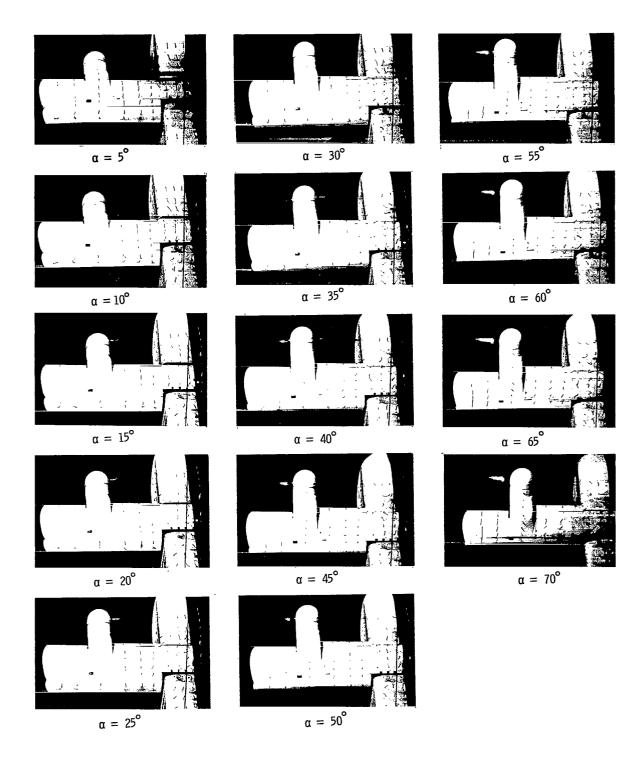


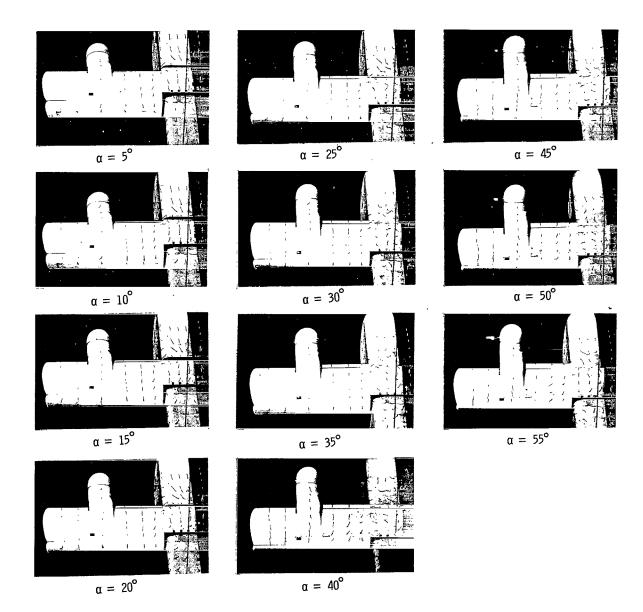
Figure 16.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, inboard slat on, and  $\delta_f = 60^\circ$ .



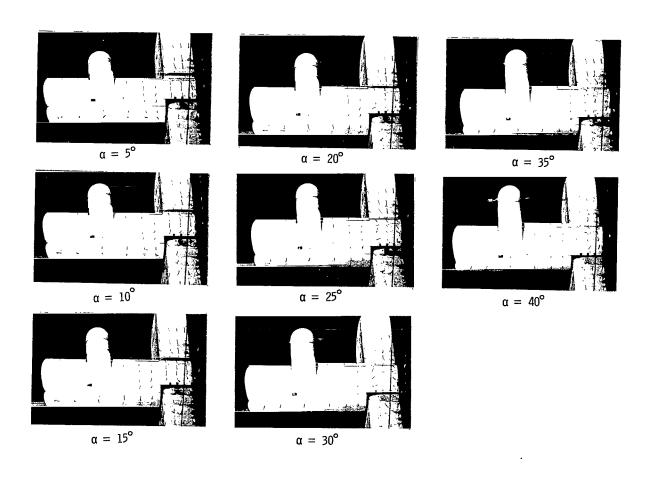
(b) Flow characteristics;  $C_{T,S}=0.90$ . Figure 16.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 16.- Continued.



(d) Flow characteristics;  $C_{\mbox{\scriptsize T,S}}=0.60.$  Figure 16.- Continued.



(e) Flow characteristics;  $C_{\mbox{\scriptsize T,S}}=0.30.$  Figure 16.- Concluded.

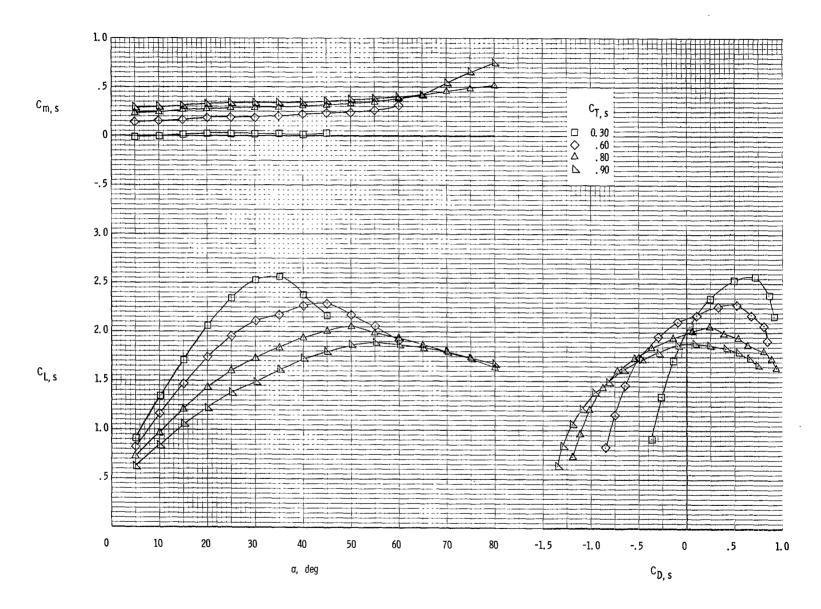
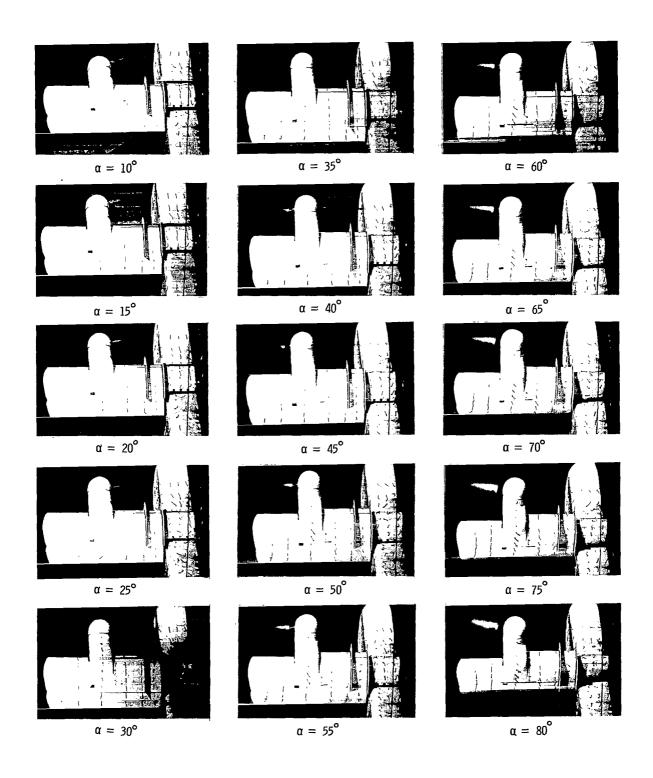
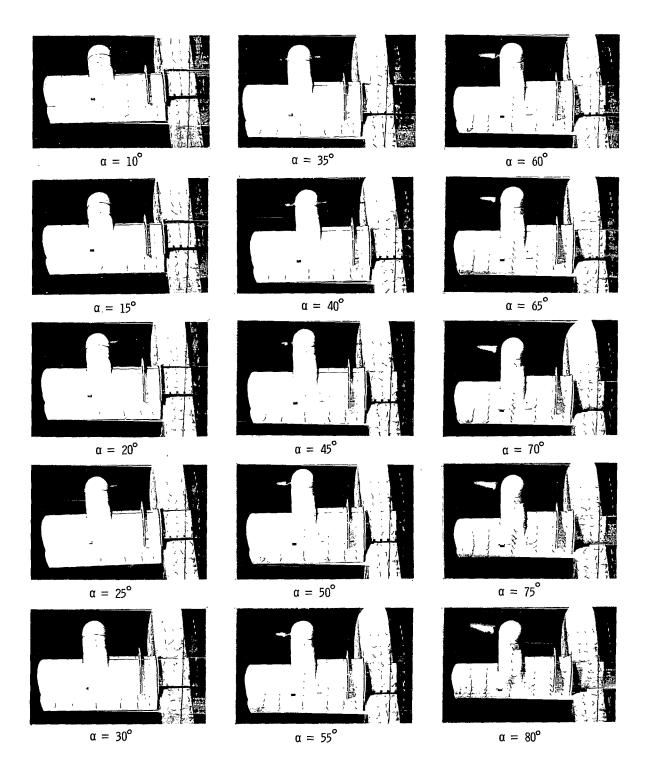


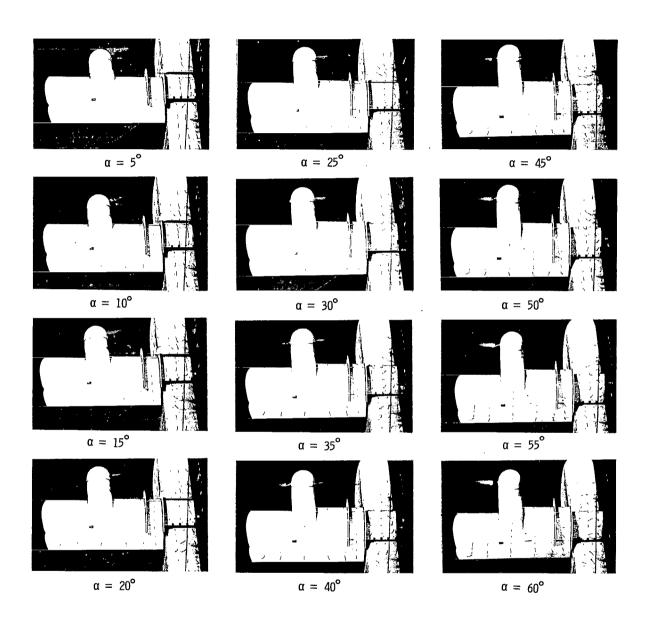
Figure 17.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, inboard slat on, fences on, and  $\delta_f = 20^\circ$ .



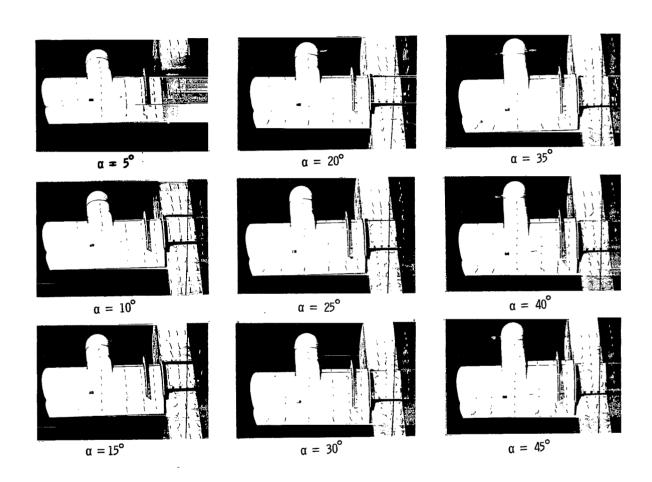
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 17.- Continued.



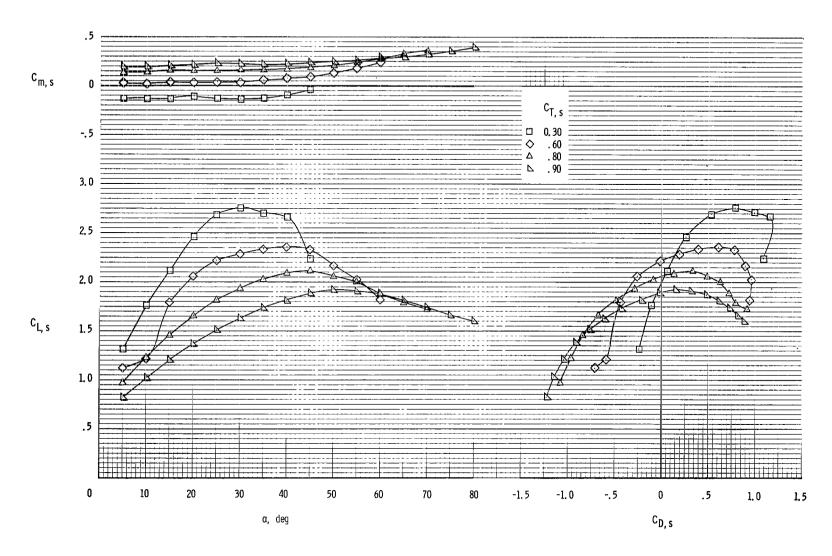
(c) Flow characteristics;  ${\rm C_{T,S}} = 0.80$ . Figure 17.- Continued.



(d) Flow characteristics;  $C_{\text{T,S}} = 0.60$ . Figure 17.- Continued.

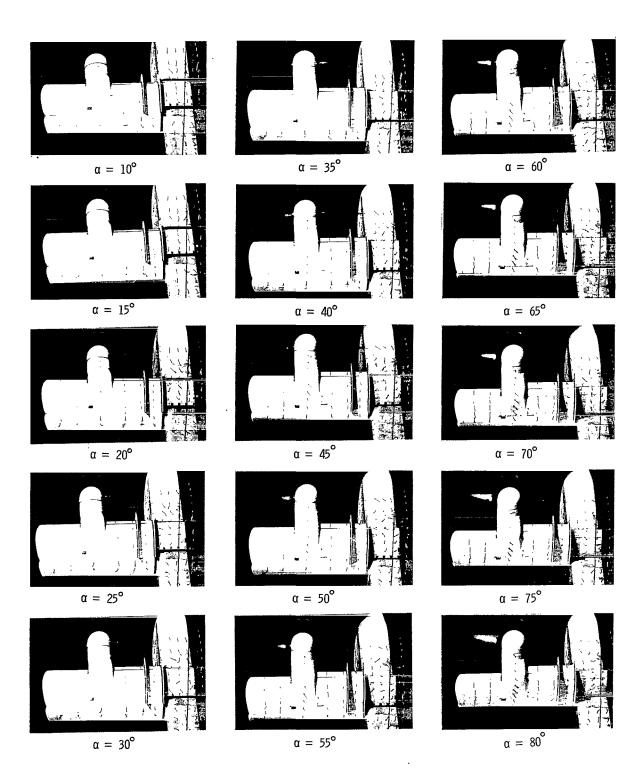


(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 17.- Concluded.

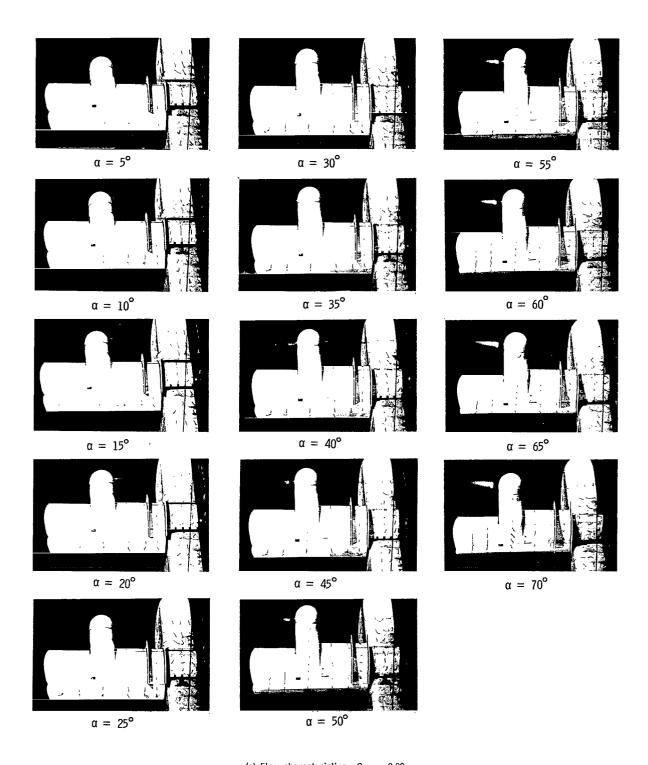


(a) Aerodynamic characteristics.

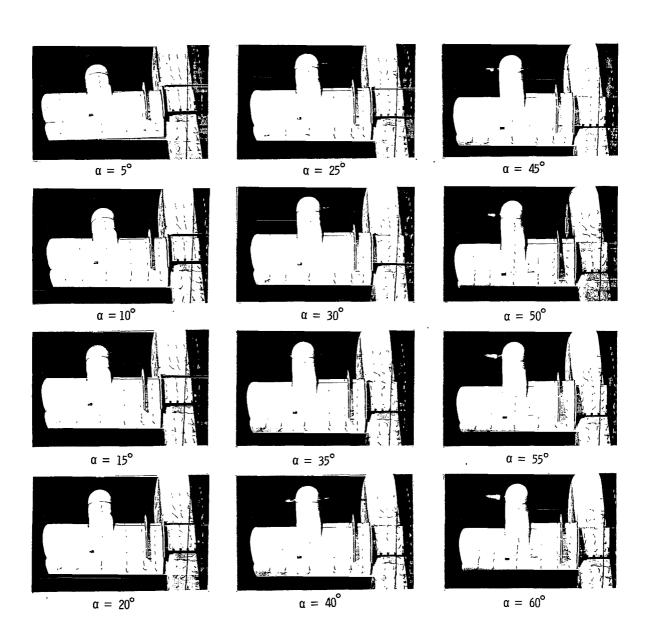
Figure 18.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, inboard slat on, fences on, and  $\delta_f = 40^\circ$ .



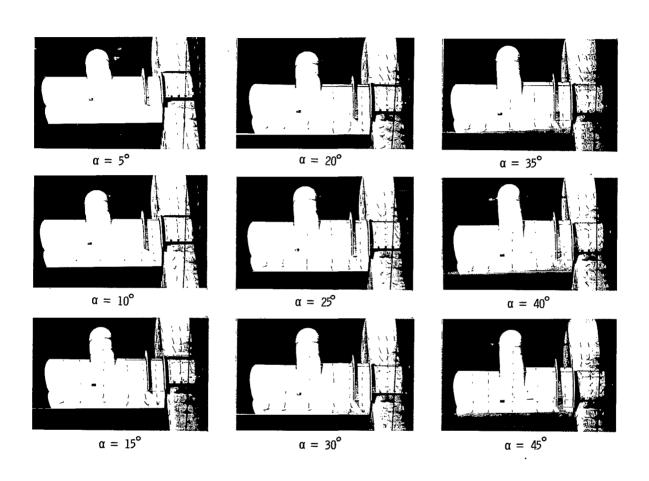
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 18.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 18.- Continued.



(d) Flow characteristics;  $C_{\mbox{\scriptsize T,S}}=0.60.$  Figure 18.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 18.- Concluded.

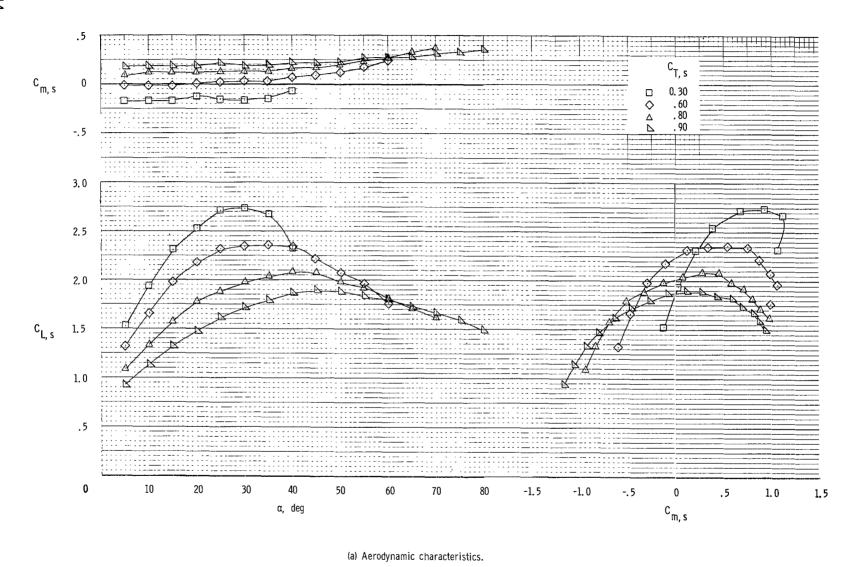
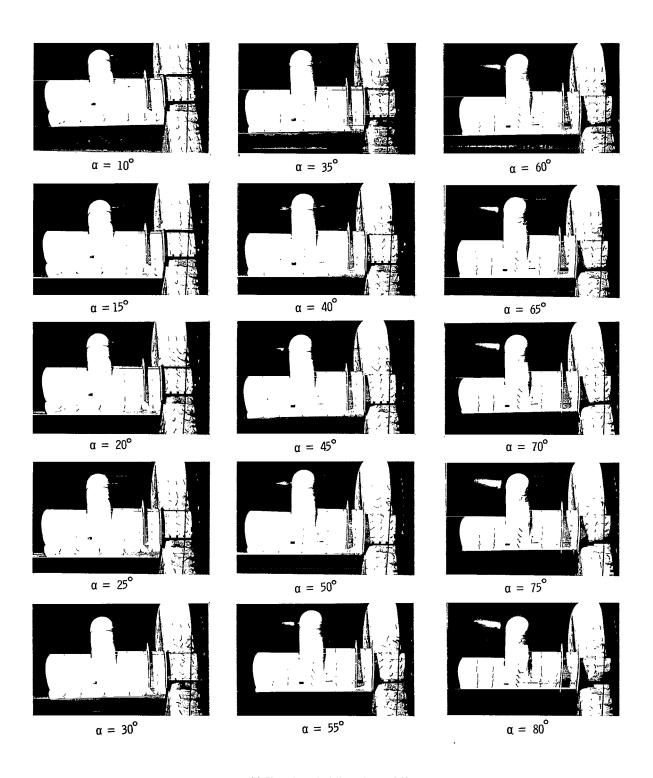
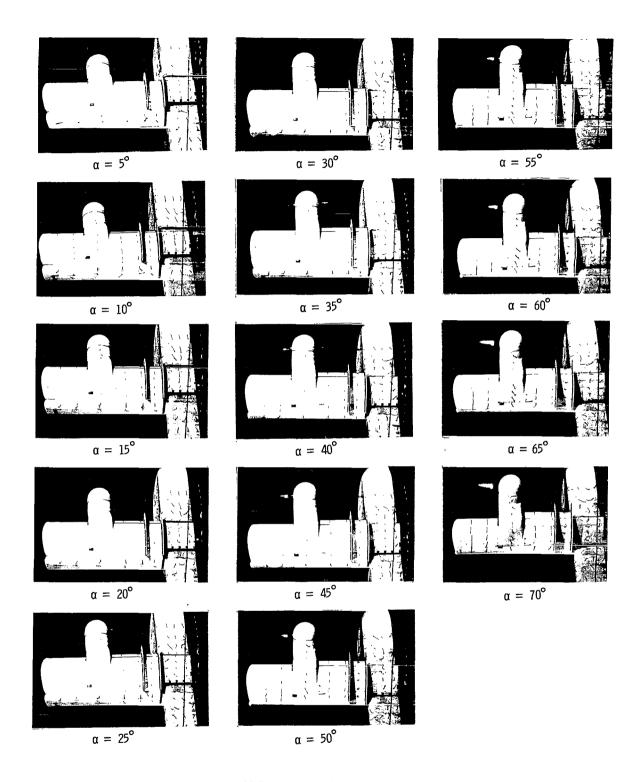


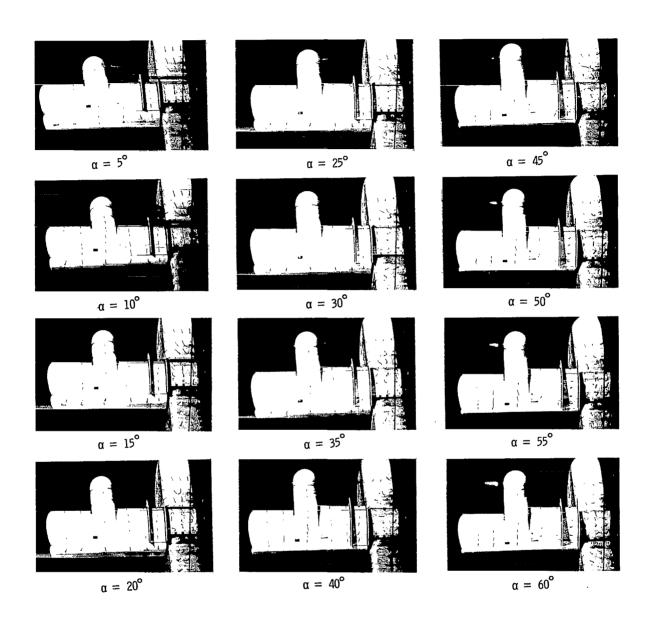
Figure 19.- Aerodynamic and flow characteristics of the wing with the propeller rotating down at the tip, inboard slat on, fences on, and  $\delta_f = 60^\circ$ .



(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 19.- Continued.

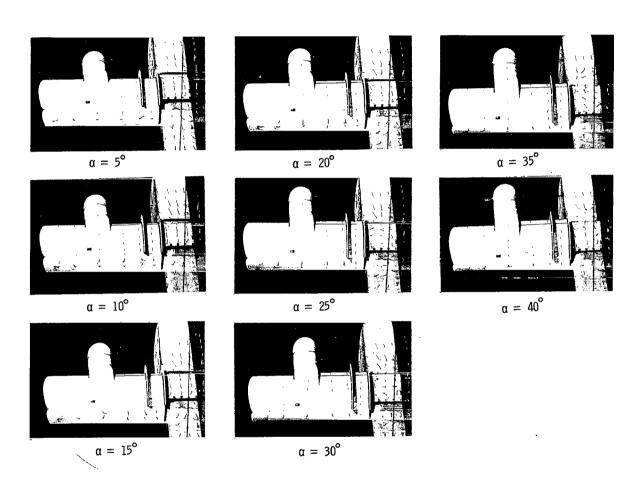


(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 19.- Continued.



(d) Flow characteristics;  $C_{T,s} = 0.60$ . Figure 19.- Continued.

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(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 19.- Concluded.

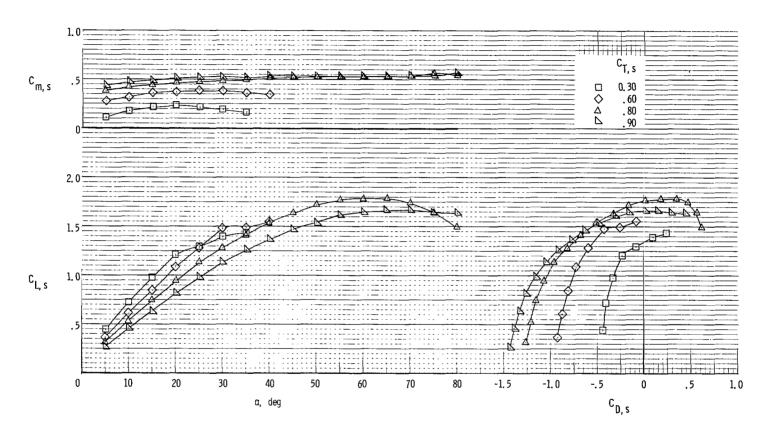
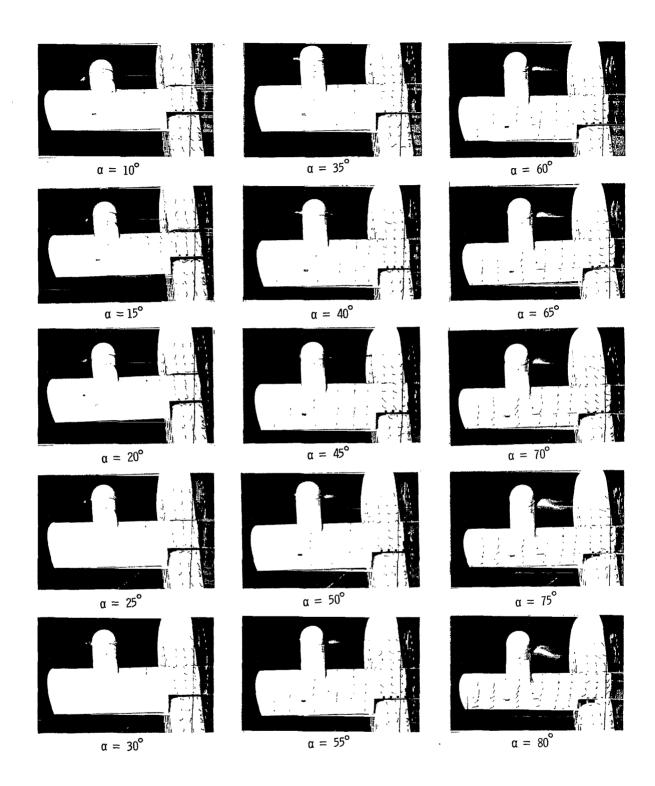
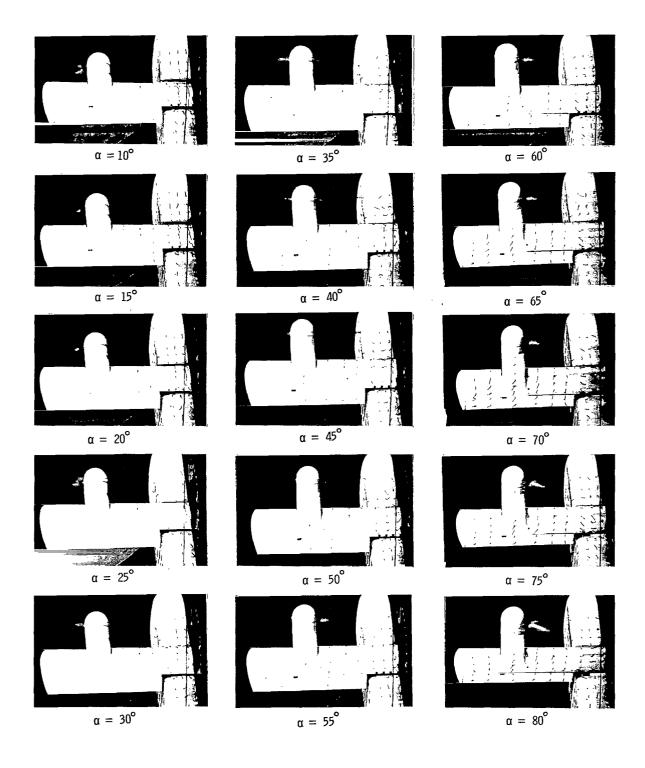


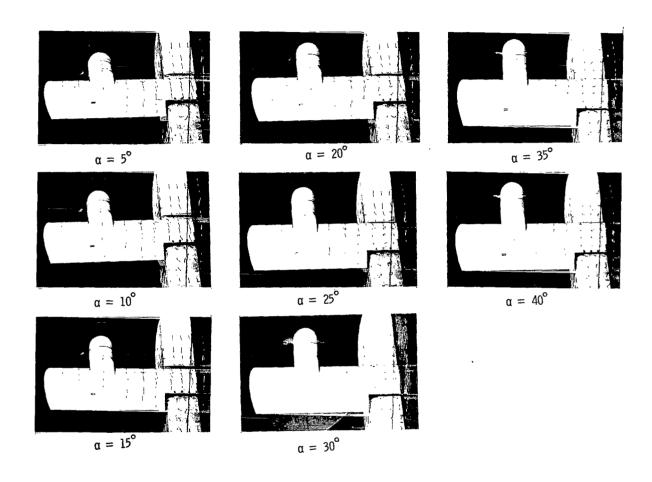
Figure 20.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, and  $\delta_f = 0^{\circ}$ .



(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 20.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 20.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 20.- Continued.

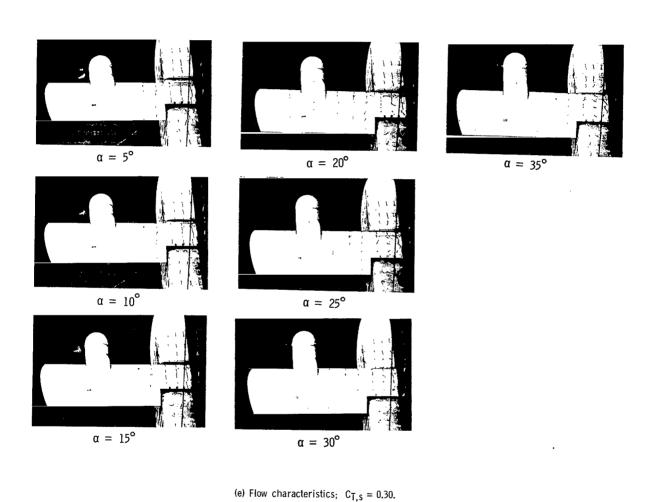


Figure 20.- Concluded.

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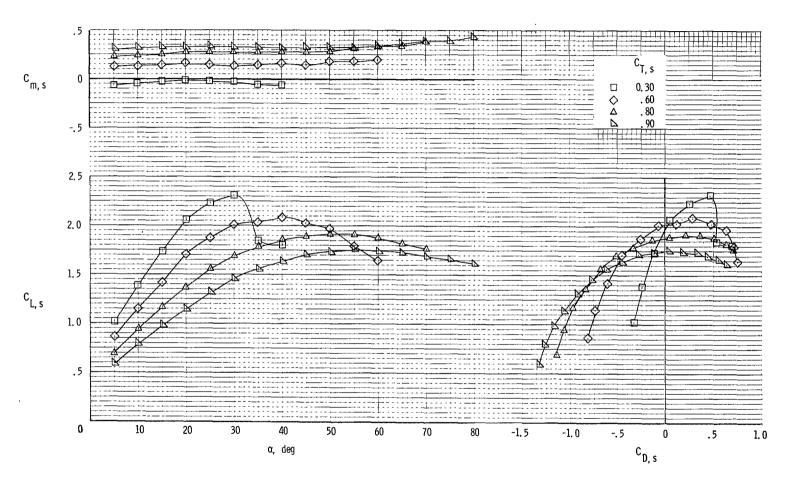
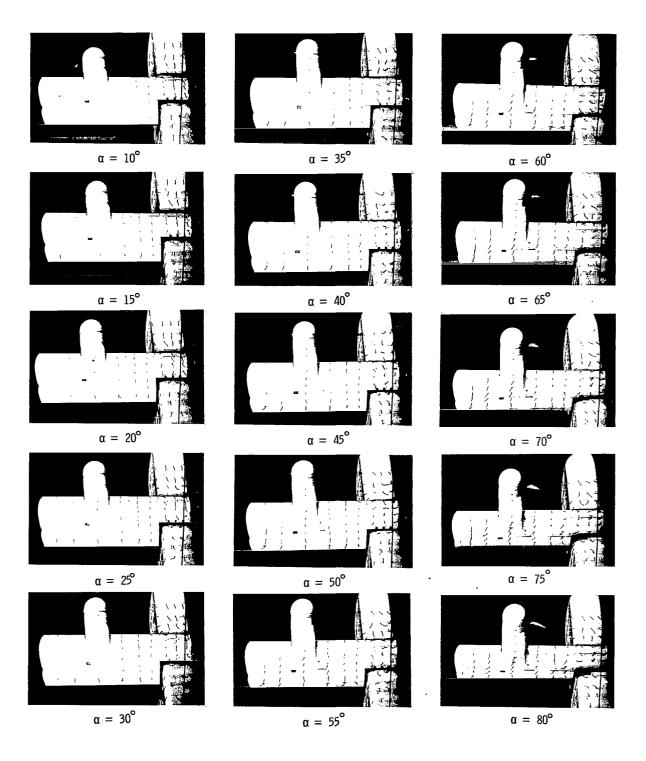
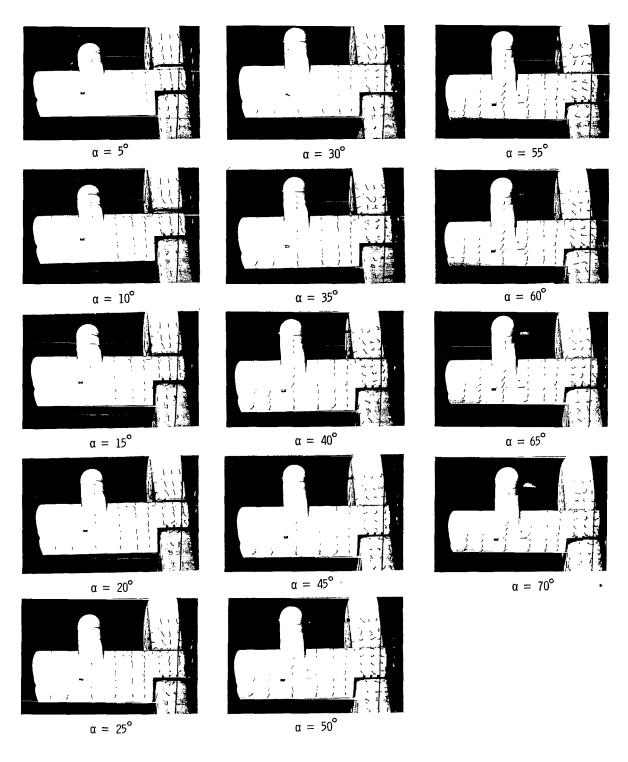


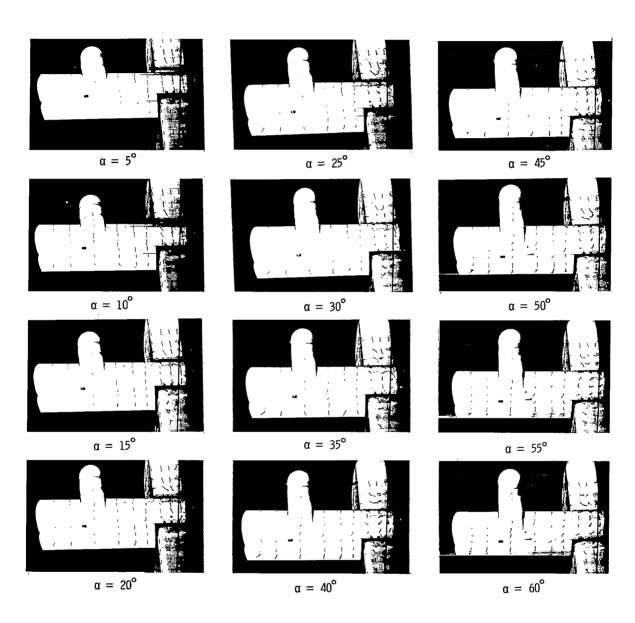
Figure 21.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, and  $\delta_f = 20^\circ$ .



(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 21.- Continued.

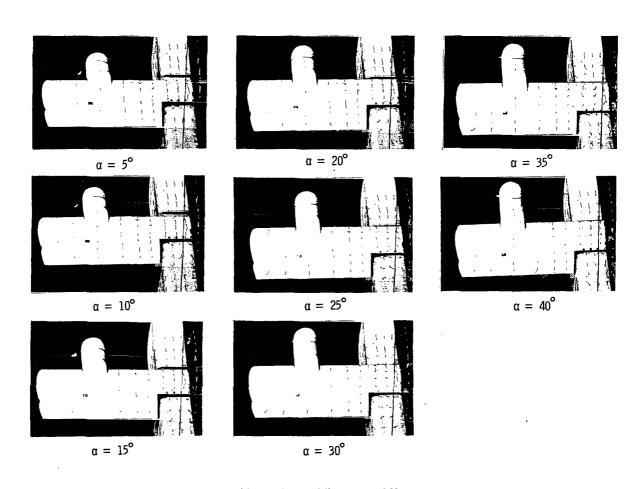


(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 21.- Continued.



(d) Flow characteristics;  $C_{\text{T,S}} = 0.60$ . Figure 21.- Continued.





(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 21.- Concluded.

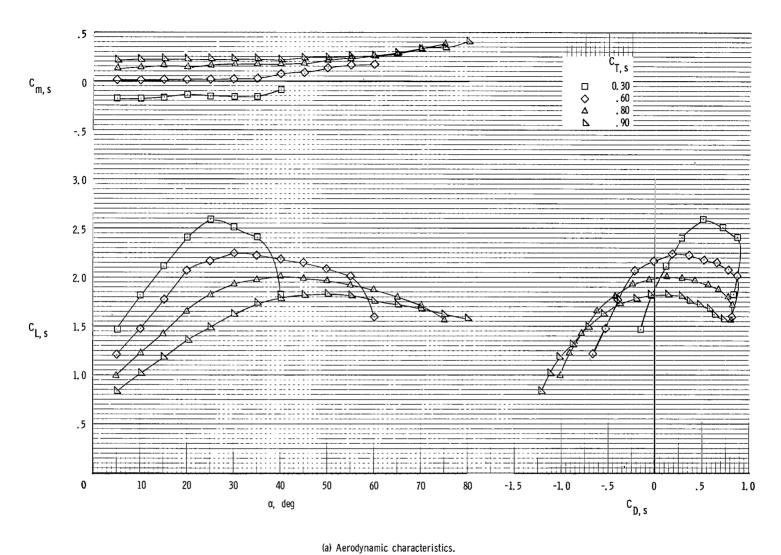
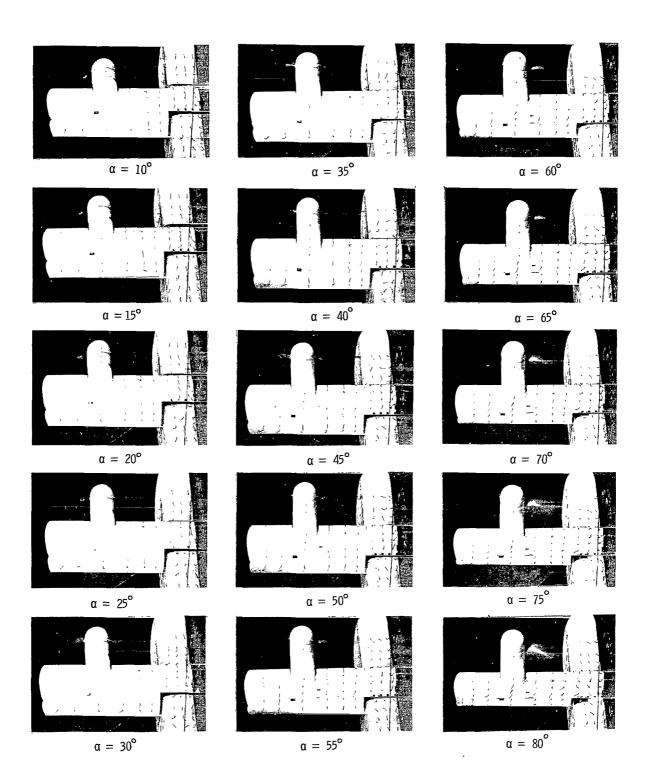
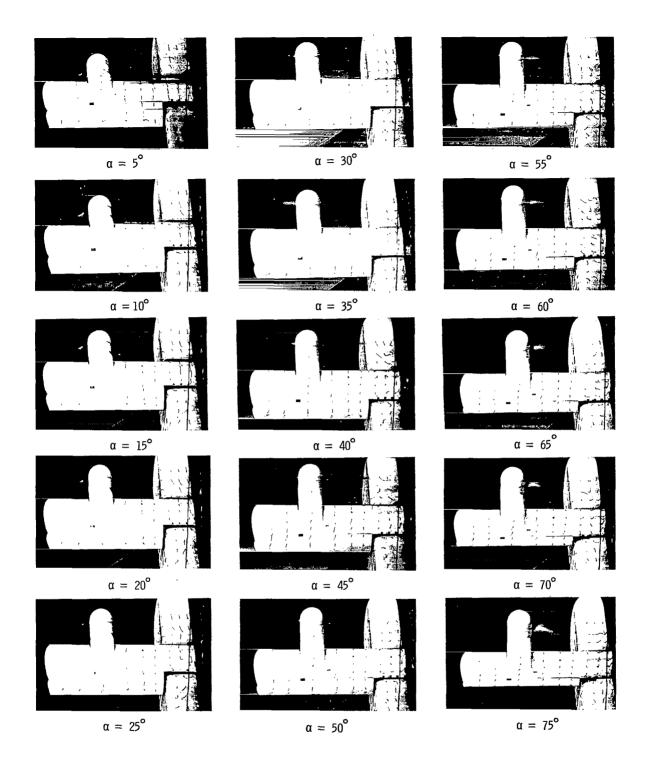


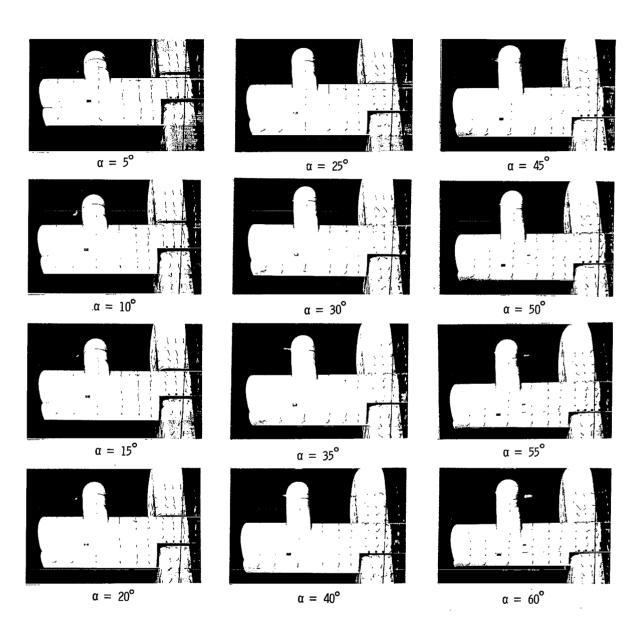
Figure 22.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, and  $\delta_f = 40^\circ$ .



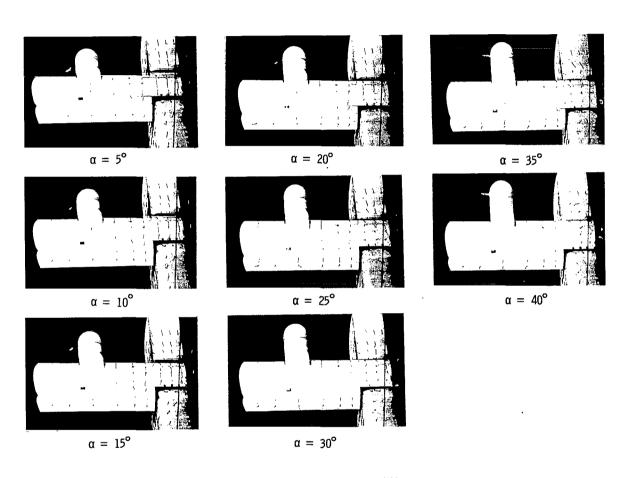
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 22.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 22.- Continued.



(d) Flow characteristics;  $C_{T,s} = 0.60$ . Figure 22.- Continued.



(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 22.- Concluded.

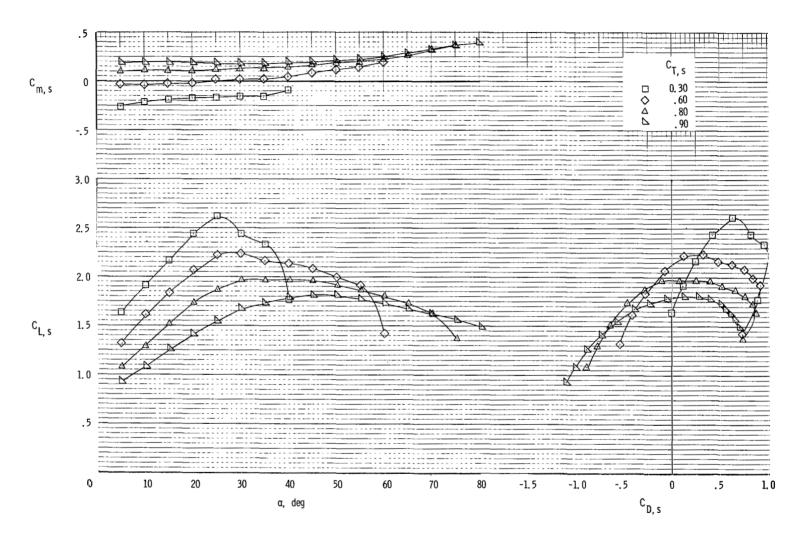
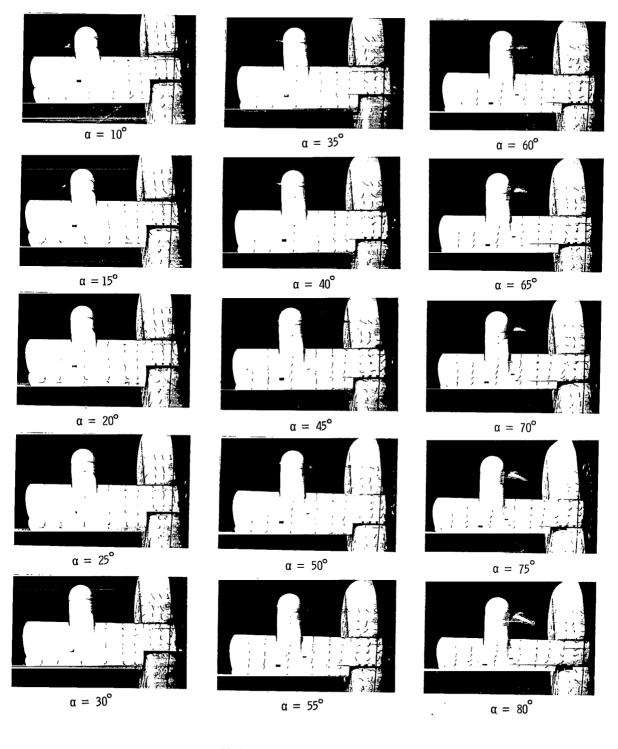
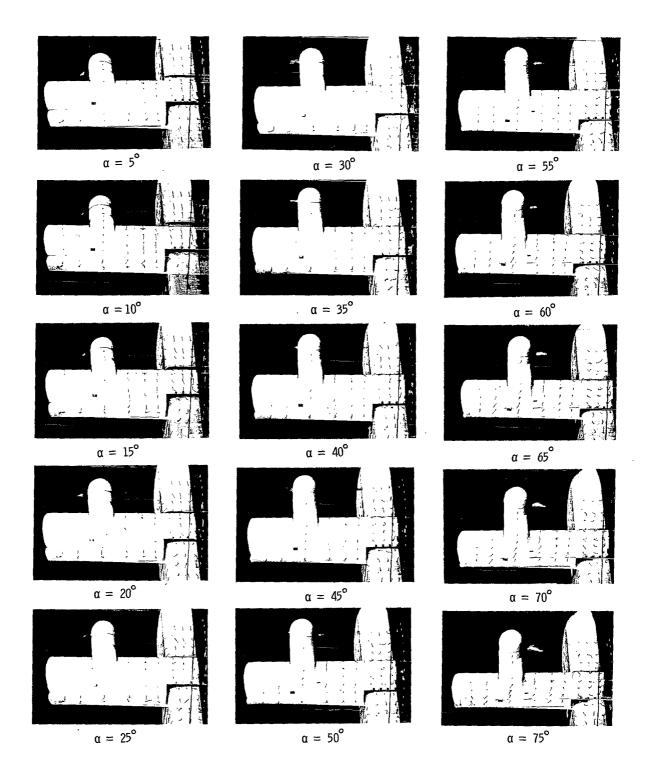


Figure 23.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, and  $\delta_f = 60^\circ$ .

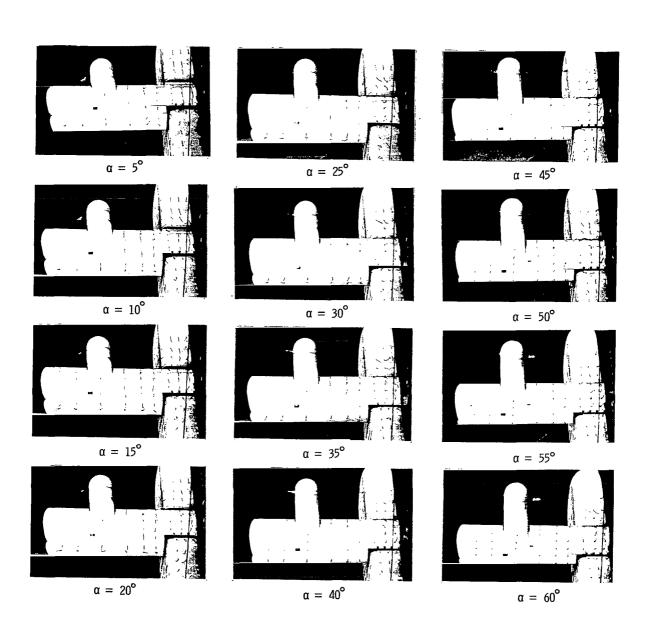


(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 23.- Continued.

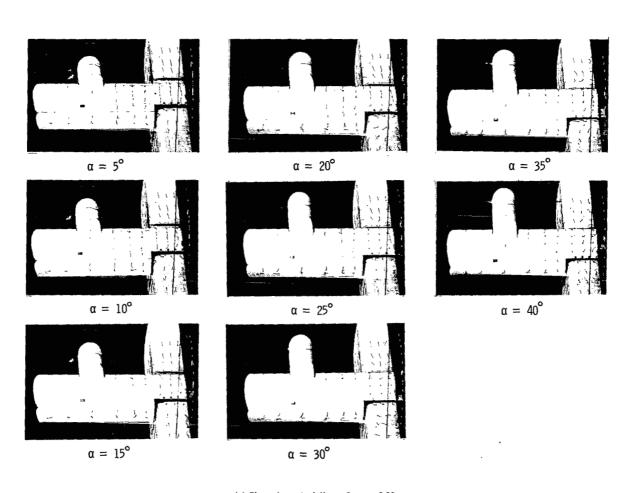
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(c) Flow characteristics;  $C_{T,s} = 0.80$ . Figure 23.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 23.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 23.- Concluded.

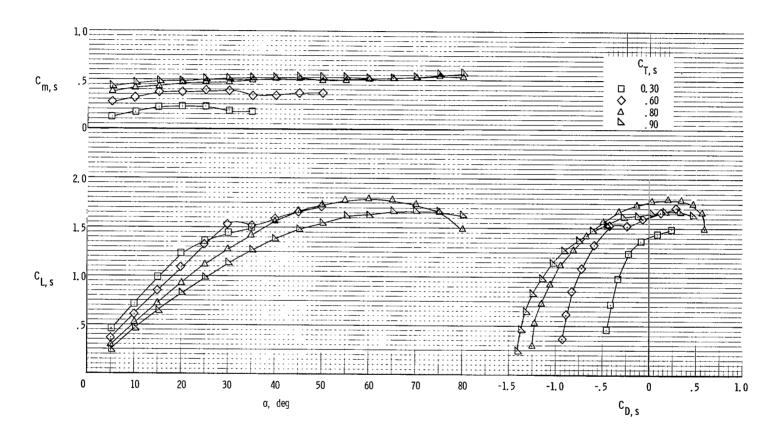
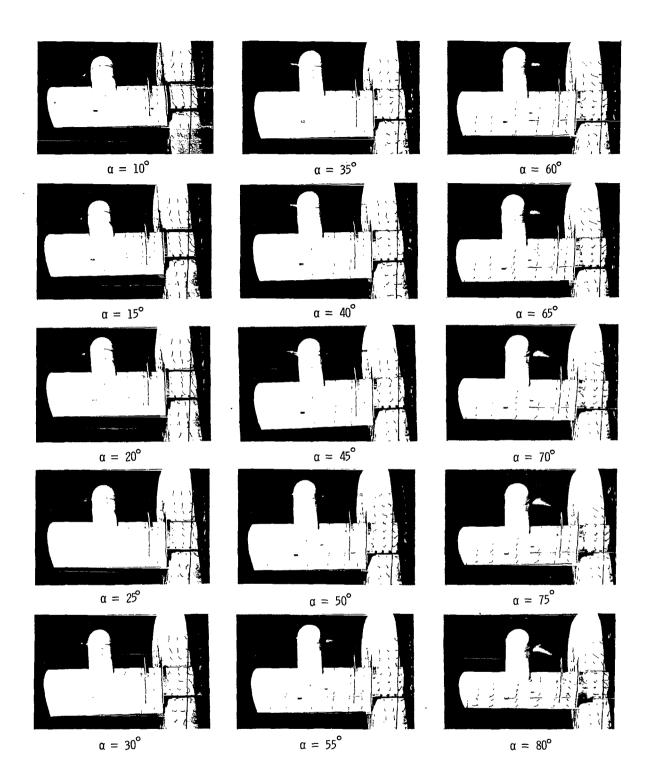
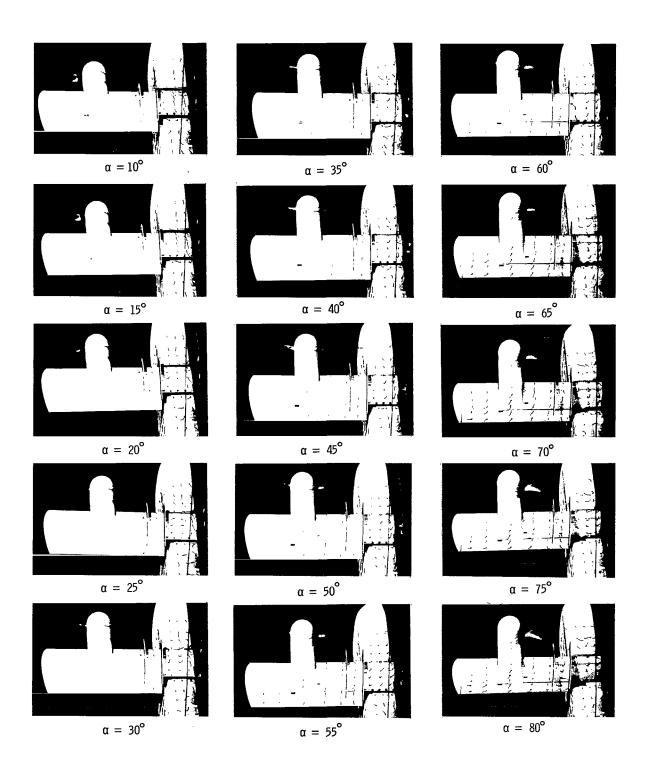


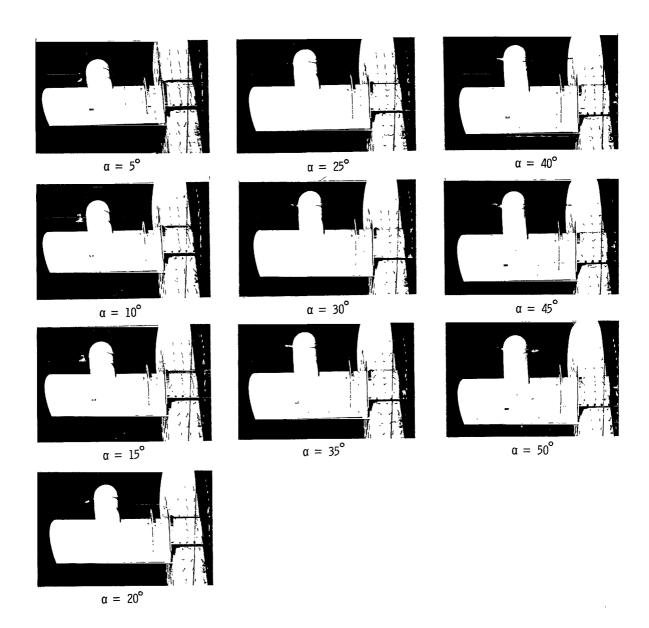
Figure 24.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, fences on, and  $\delta_f = 0^{\circ}$ .



(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 24.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 24.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 24.- Continued.

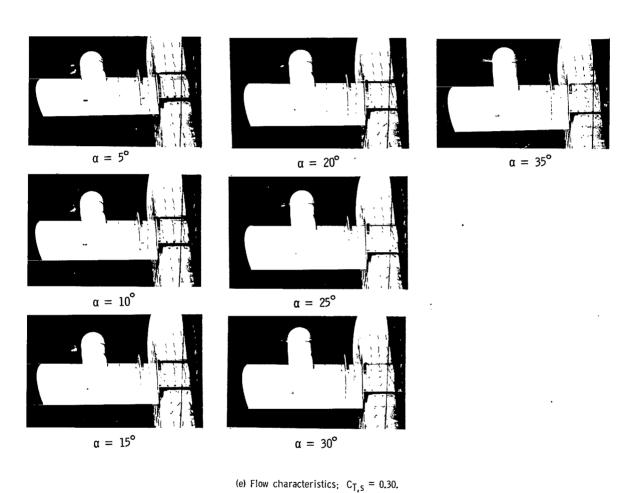


Figure 24.- Concluded.

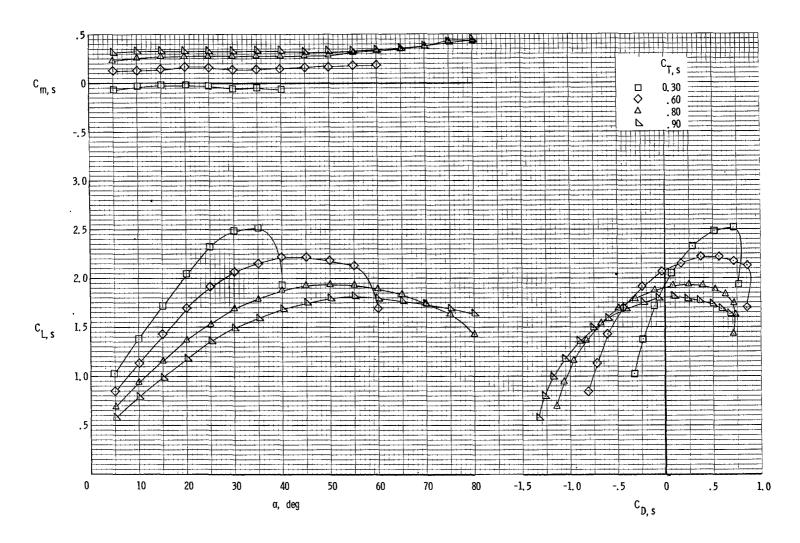
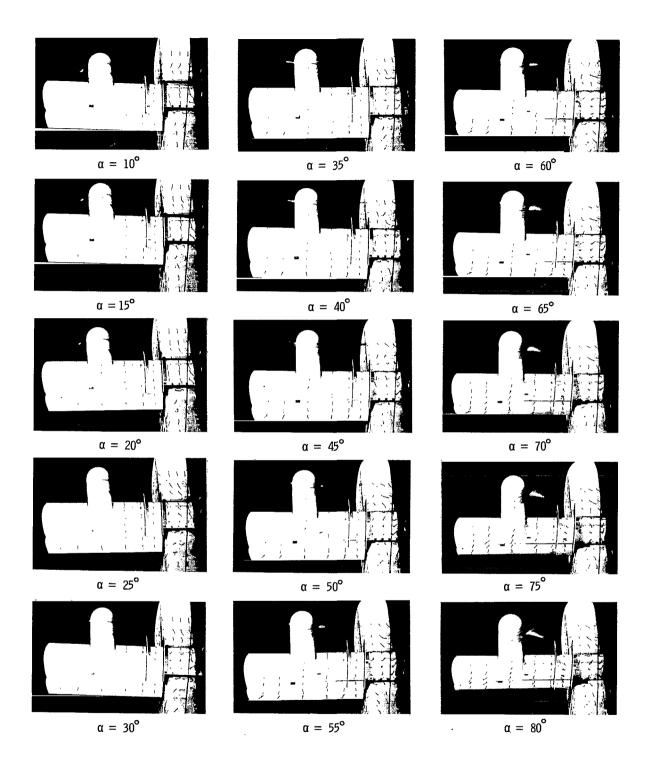
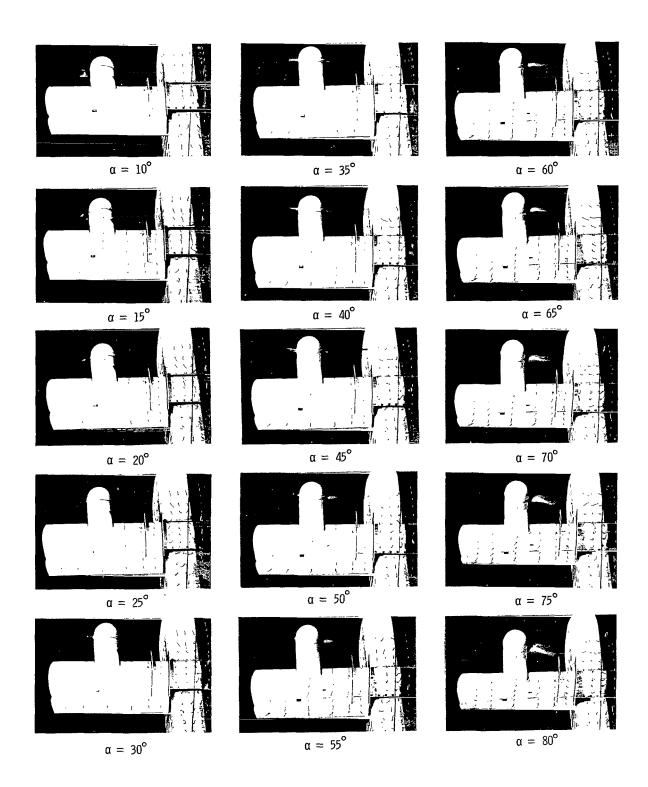


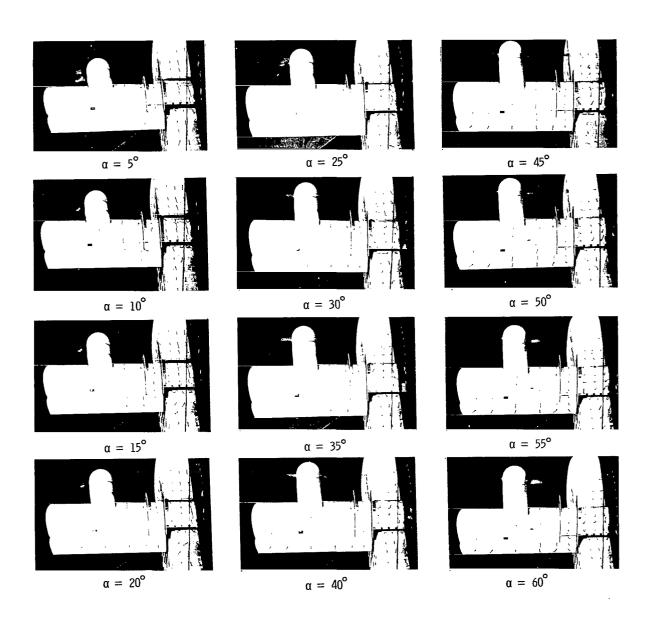
Figure 25.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, fences on, and  $\delta_f = 20^\circ$ .



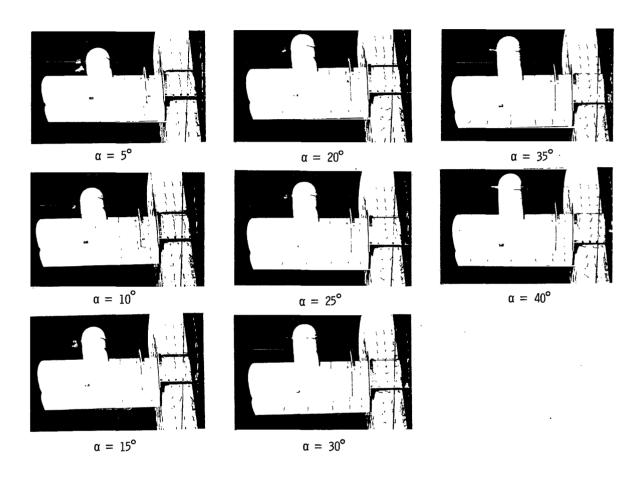
(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 25.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 25.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 25.- Continued.



(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 25.- Concluded.

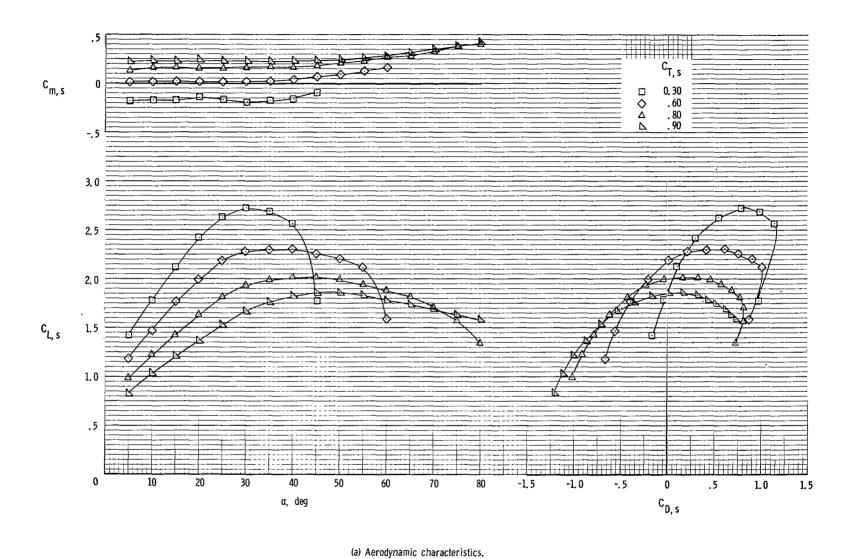
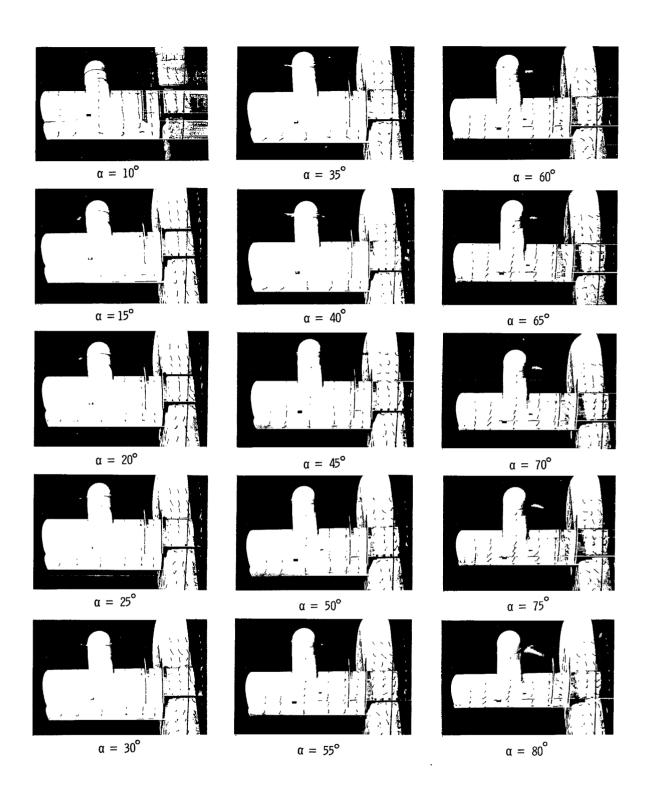
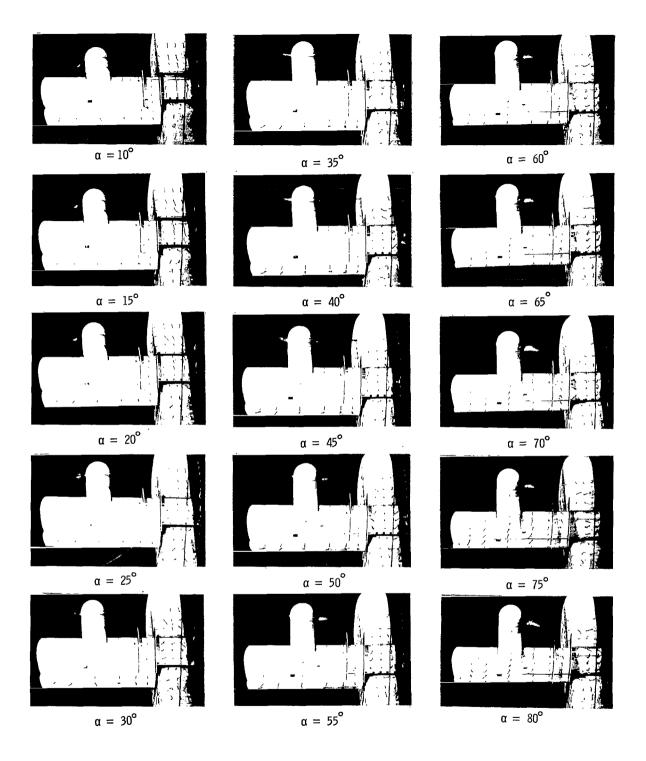


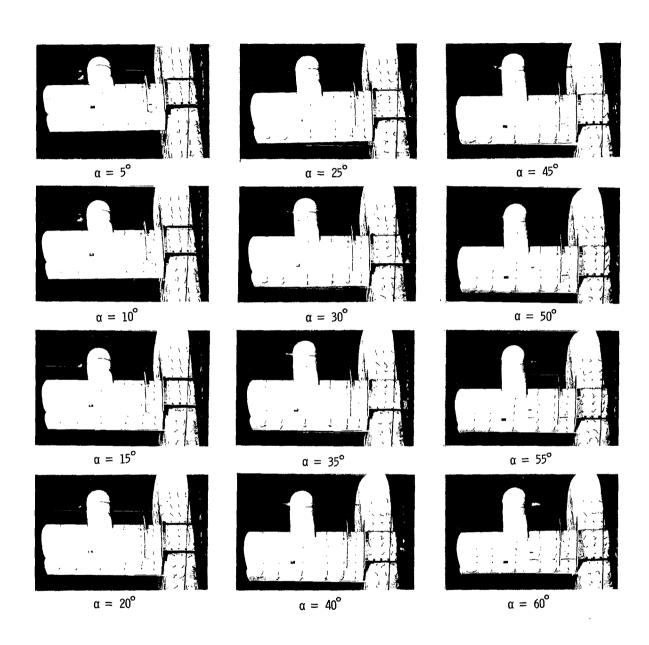
Figure 26.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, fences on, and  $\delta_f = 40^\circ$ .



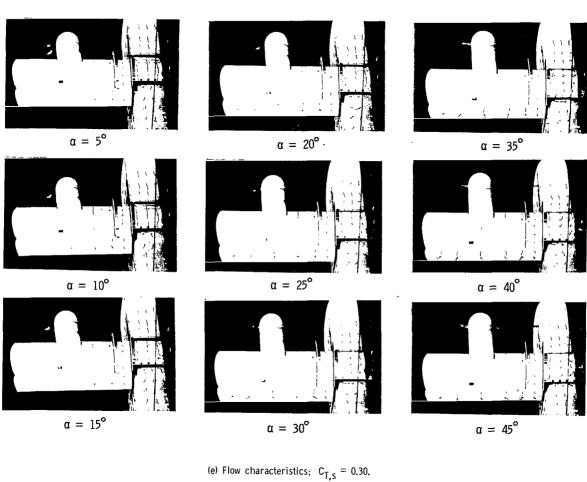
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 26.- Continued.



(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 26.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 26.- Continued.



Flow characteristics;  $C_{T,s} = 0.30$ . Figure 26.- Concluded.

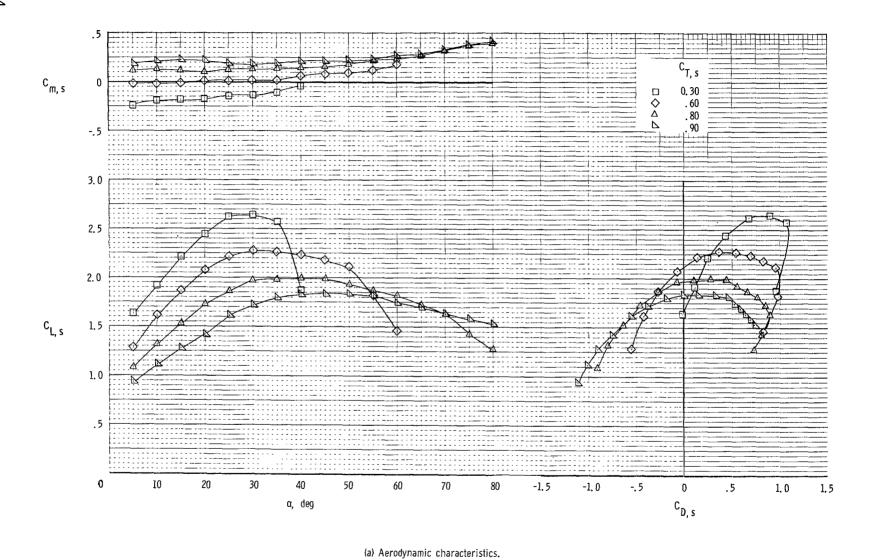
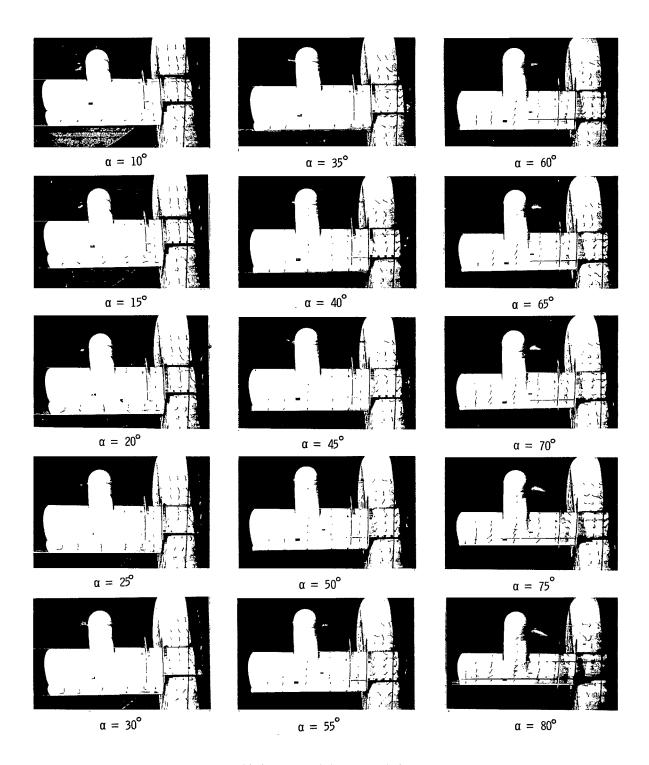
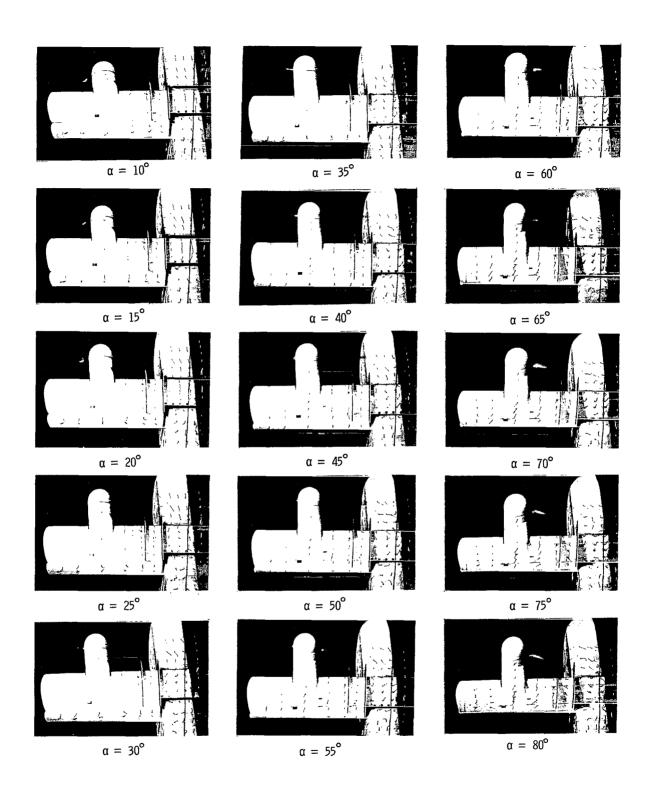


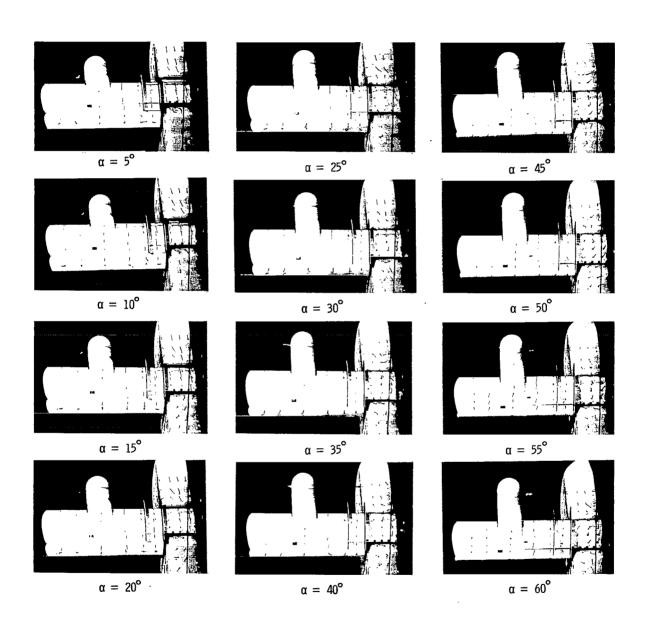
Figure 27.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, basic leading edge, fences on, and  $\delta_f = 60^{\circ}$ .



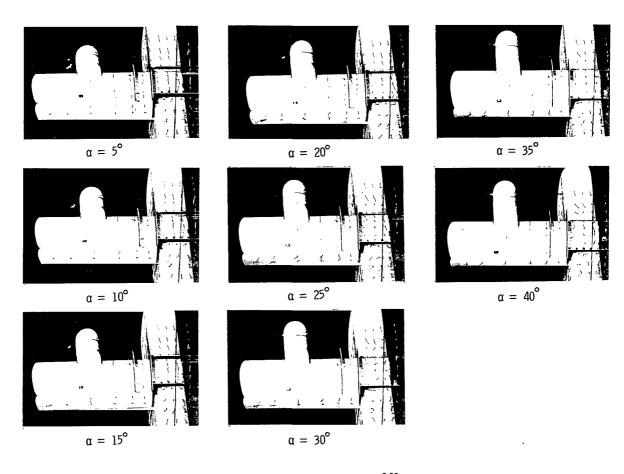
(b) Flow characteristics;  $c_{T,s} = 0.90$ . Figure 27.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 27.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 27.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 27.- Concluded.

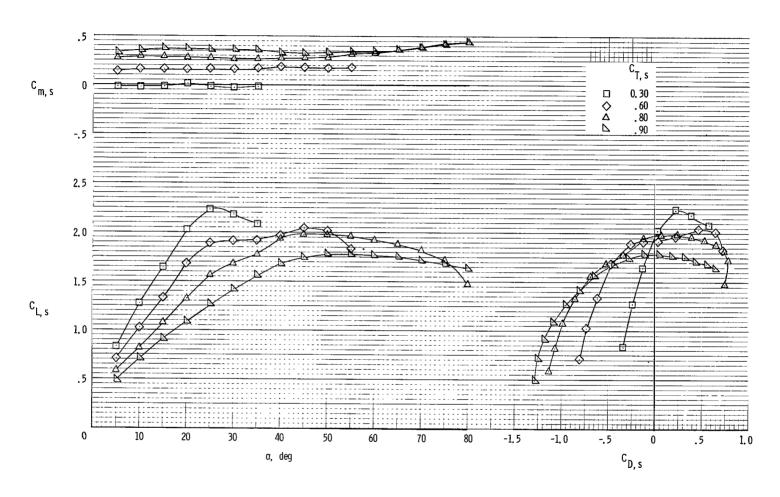
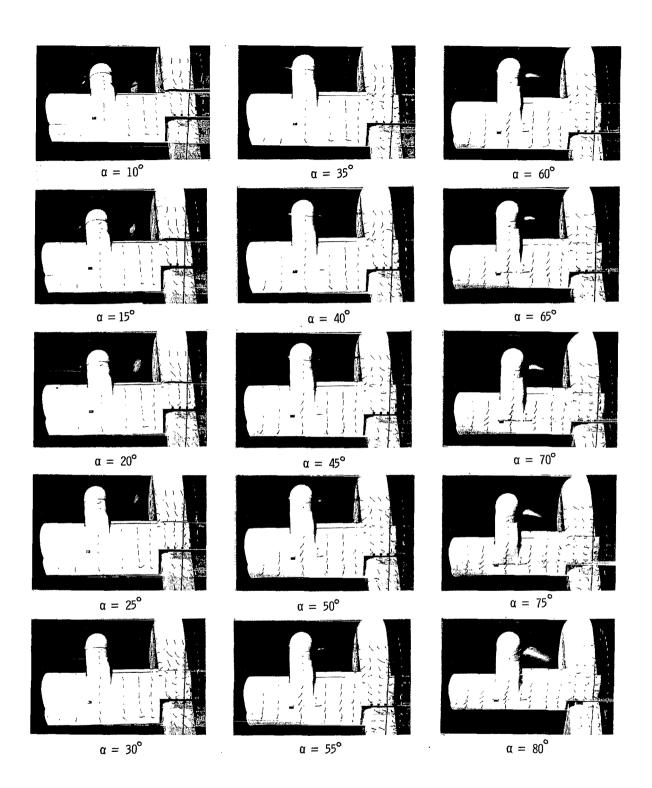
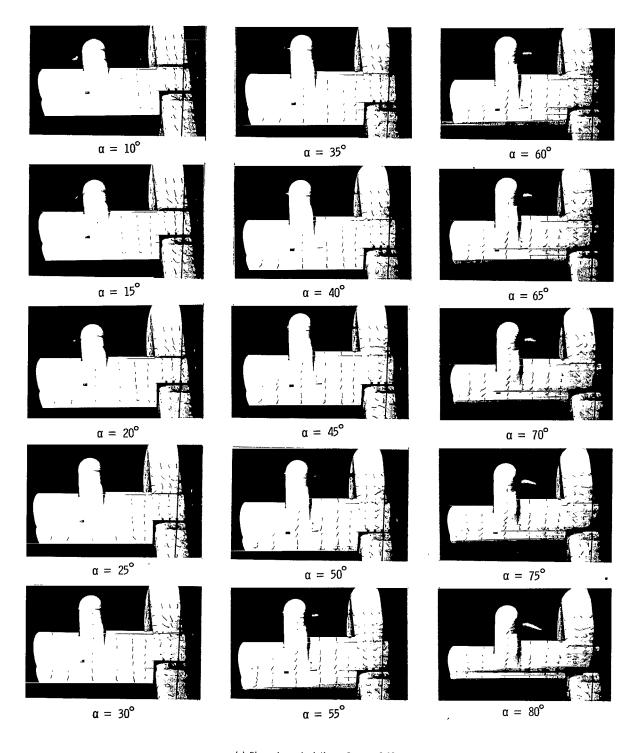


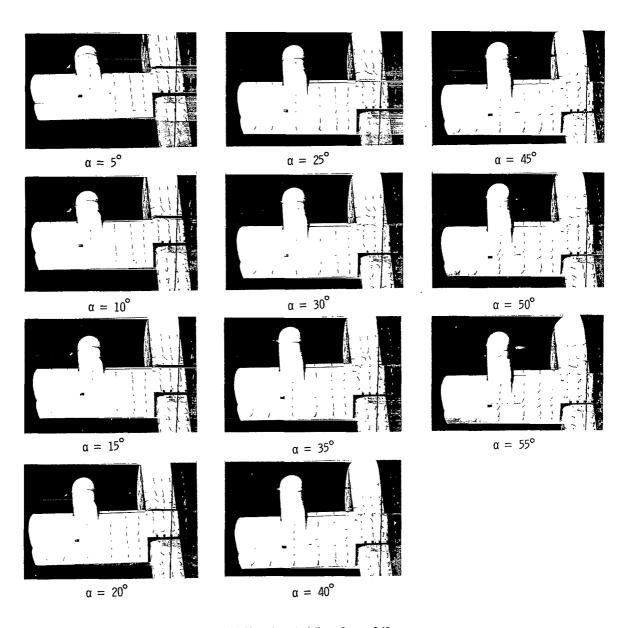
Figure 28.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, inboard slat on, and  $\delta_f = 20^\circ$ .



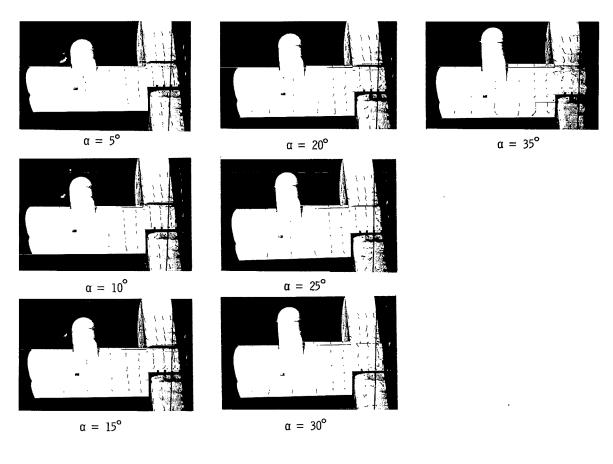
(b) Flow characteristics;  $c_{T,s} \approx 0.90$ . Figure 28.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 28.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 28.- Continued.



(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 28.- Concluded.

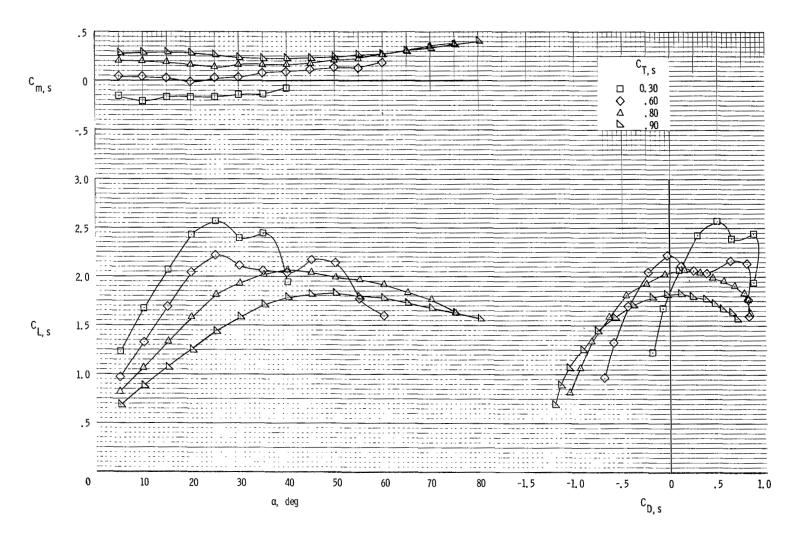
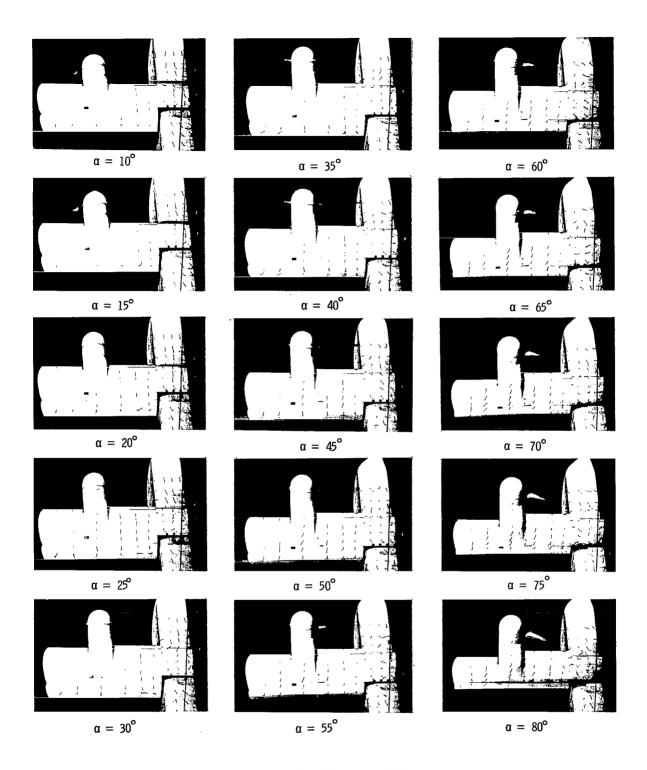
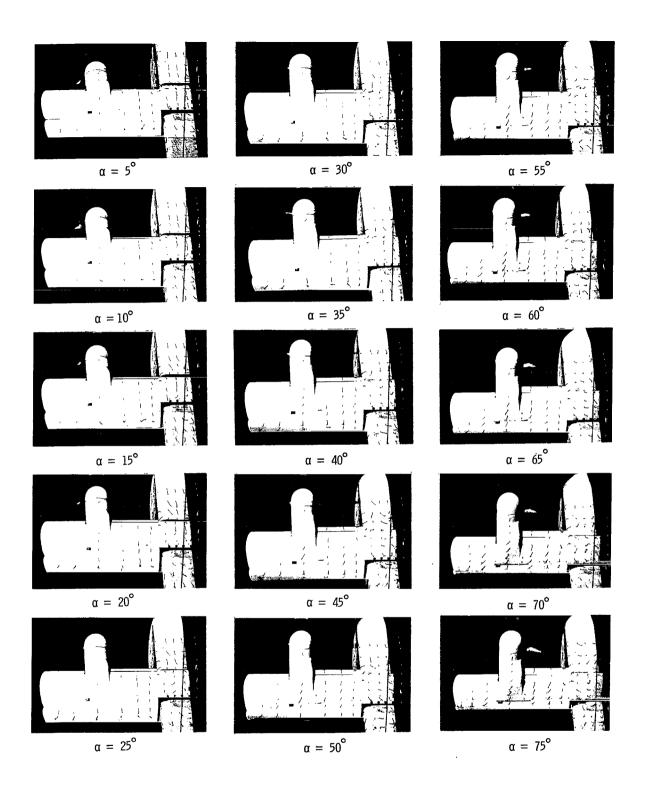


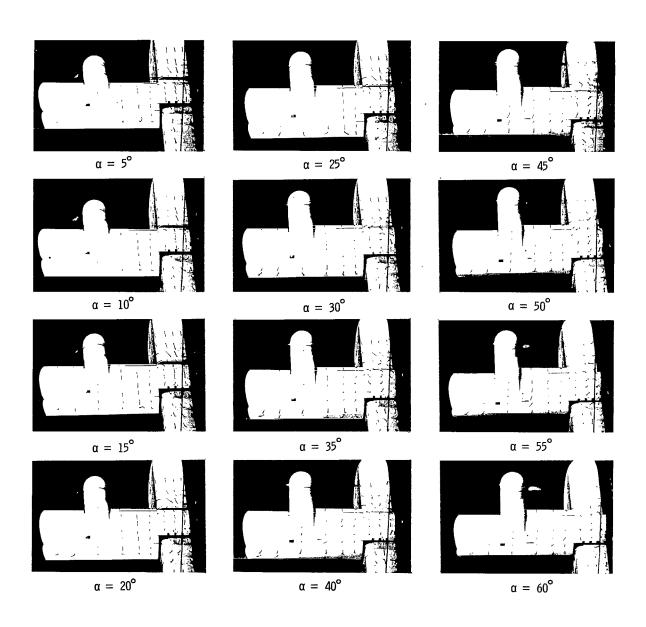
Figure 29.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, inboard slat on, and  $\delta_f=400$ .



(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 29.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 29.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 29.- Continued.

(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 29.- Concluded.

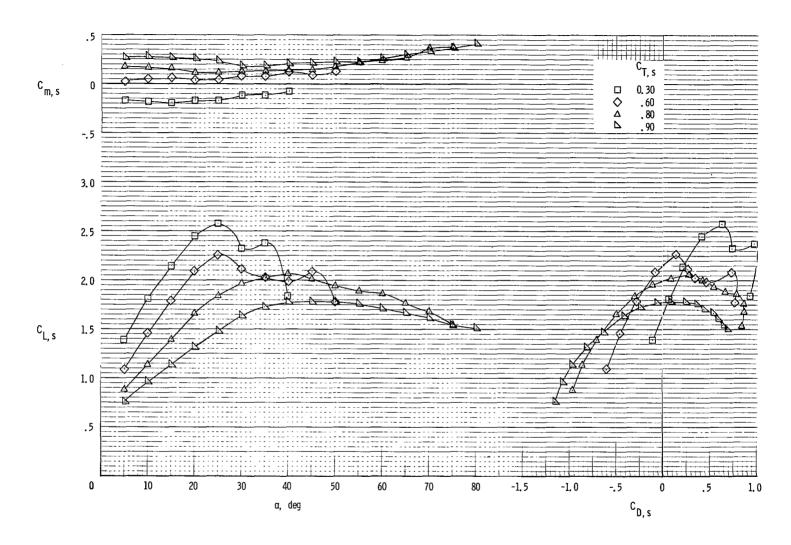
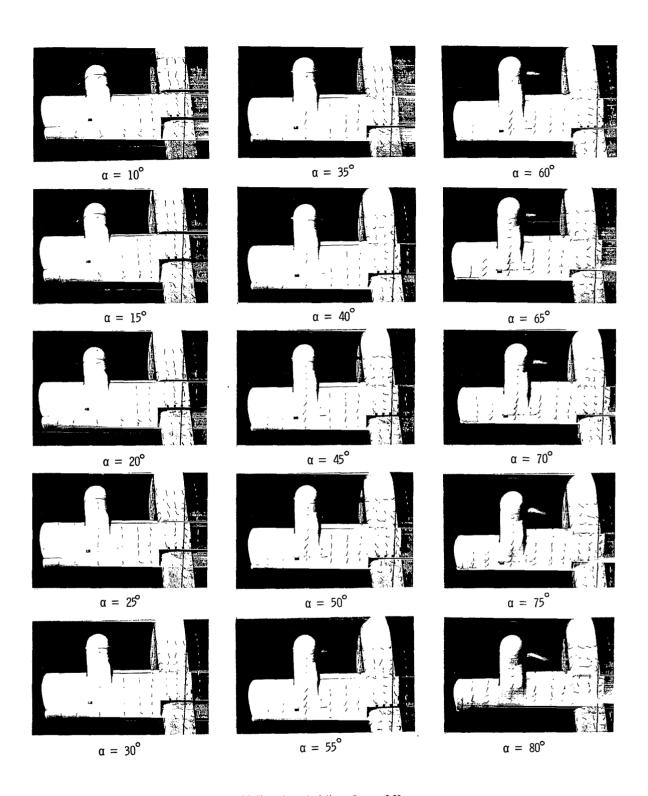
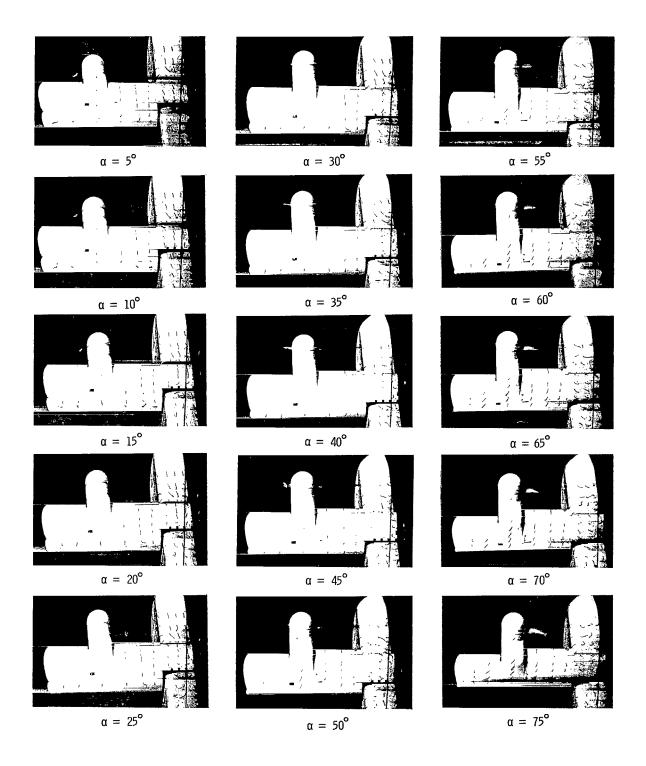


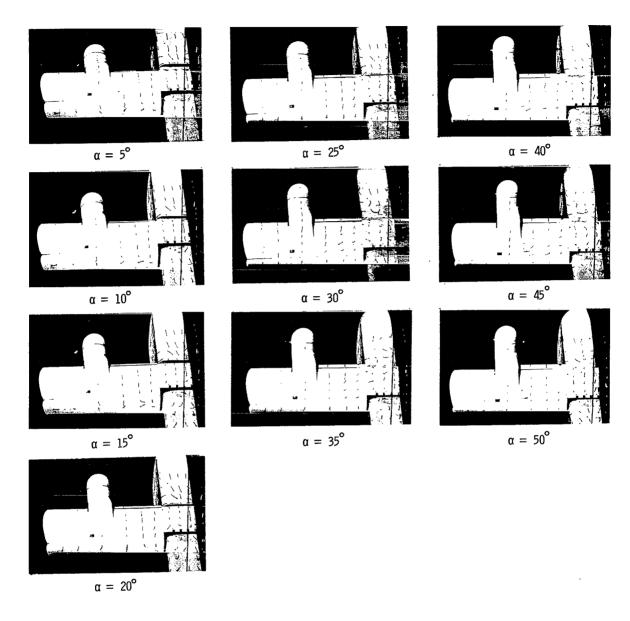
Figure 30.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, inboard slat on, and  $\delta_f = 60^\circ$ .



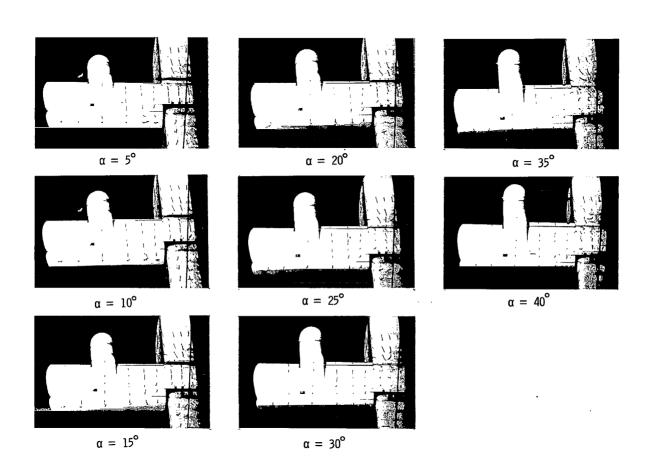
(b) Flow characteristics;  $c_{T,s} = 0.90$ . Figure 30.- Continued.



(c) Flow characteristics;  $C_{T,s} = 0.80$ . Figure 30.- Continued.



(d) Flow characteristics;  $c_{T,s} = 0.60$ . Figure 30.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 30.- Concluded.

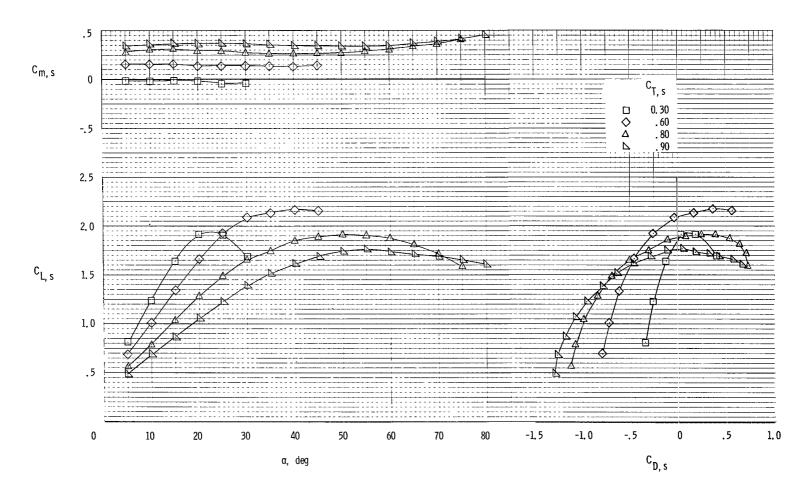
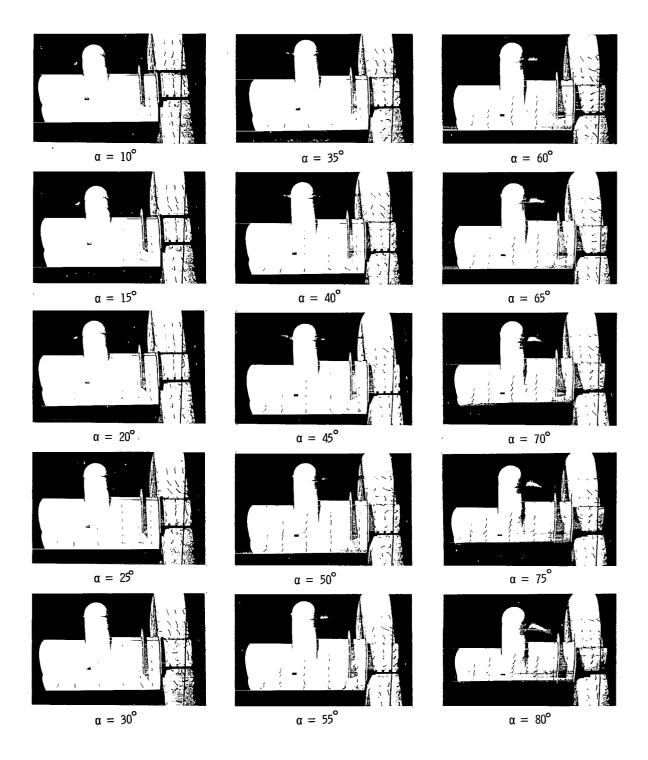
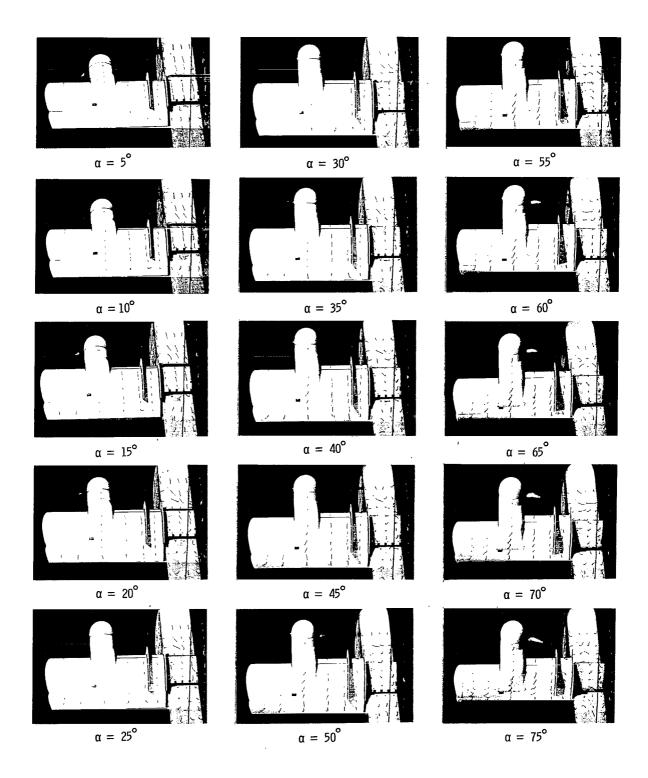


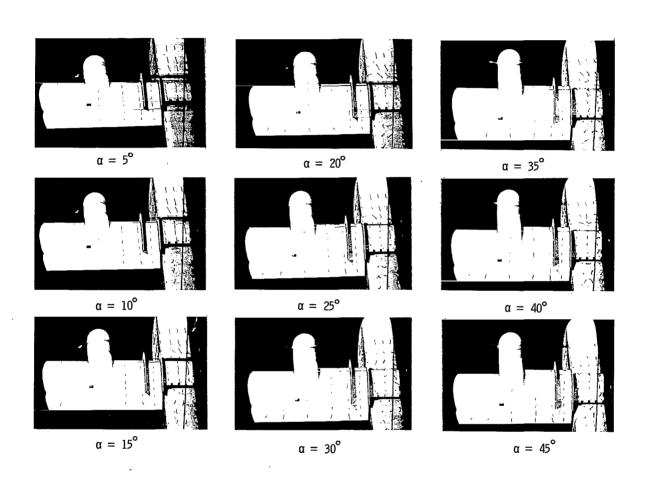
Figure 31.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, inboard slat on, fences on, and  $\delta_f = 20^\circ$ .



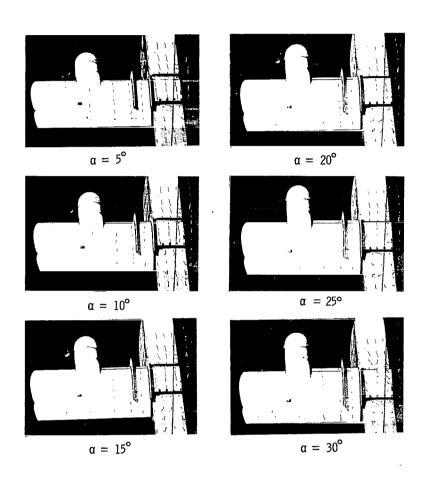
(b) Flow characteristics;  $c_{T,s} = 0.90$ . Figure 31.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 31.- Continued.



(d) Flow characteristics;  $C_{T,s} = 0.60$ . Figure 31.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 31.- Concluded.

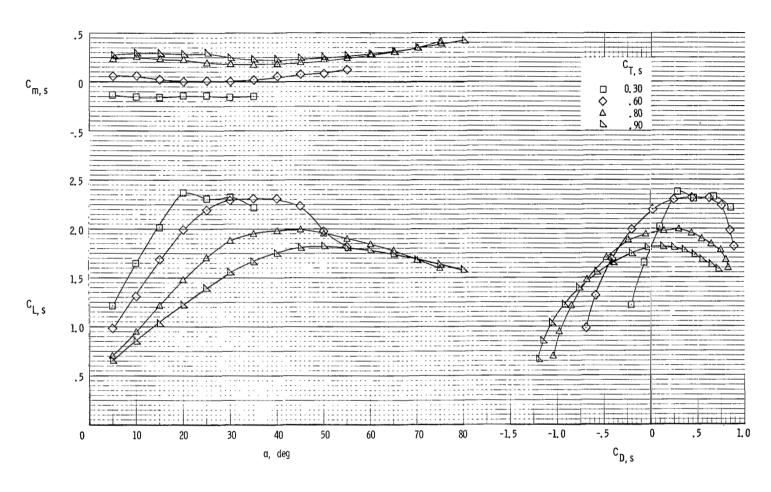
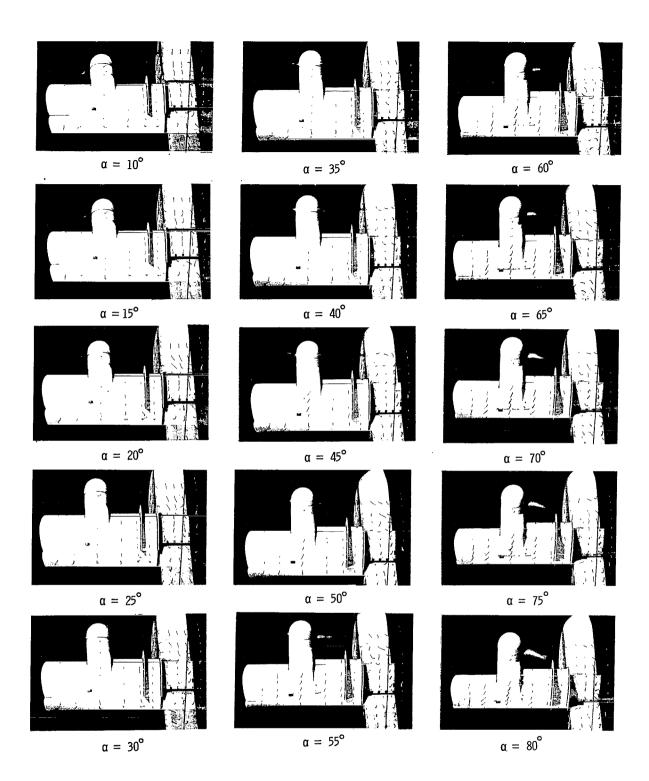
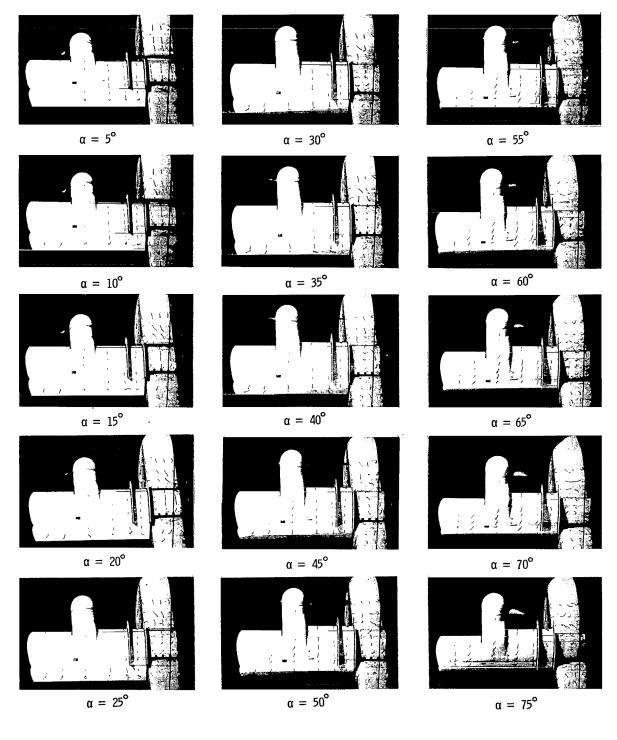


Figure 32.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, inboard slat on, fences on, and  $\delta_f = 40^\circ$ .

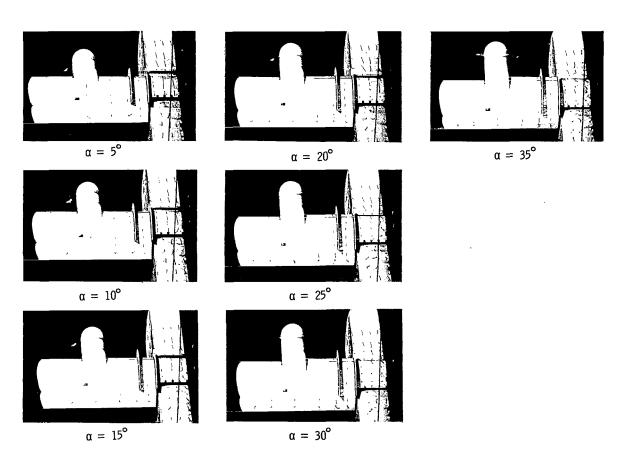


(b) Flow characteristics;  $c_{T,s} = 0.90$ . Figure 32.- Continued.



(c) Flow characteristics;  $C_{T,s} = 0.80$ . Figure 32.- Continued.

(d) Flow characteristics;  $c_{T,s} = 0.60$ . Figure 32.- Continued.



(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 32.- Concluded.

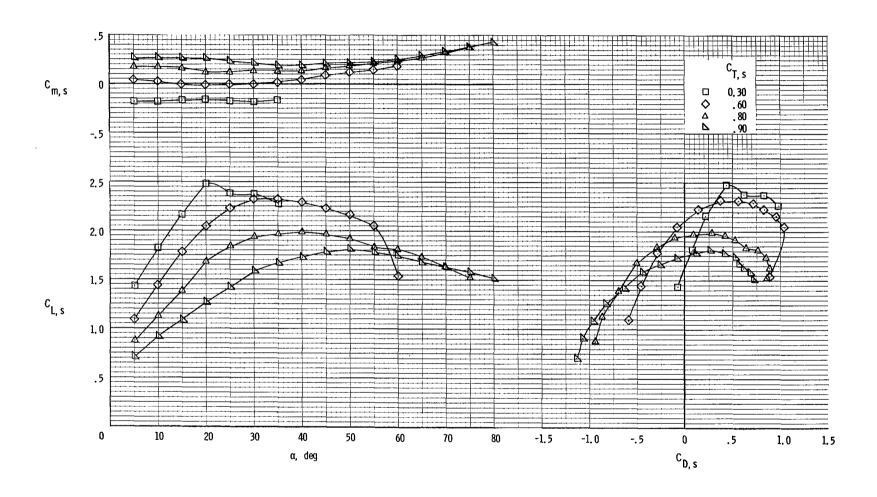
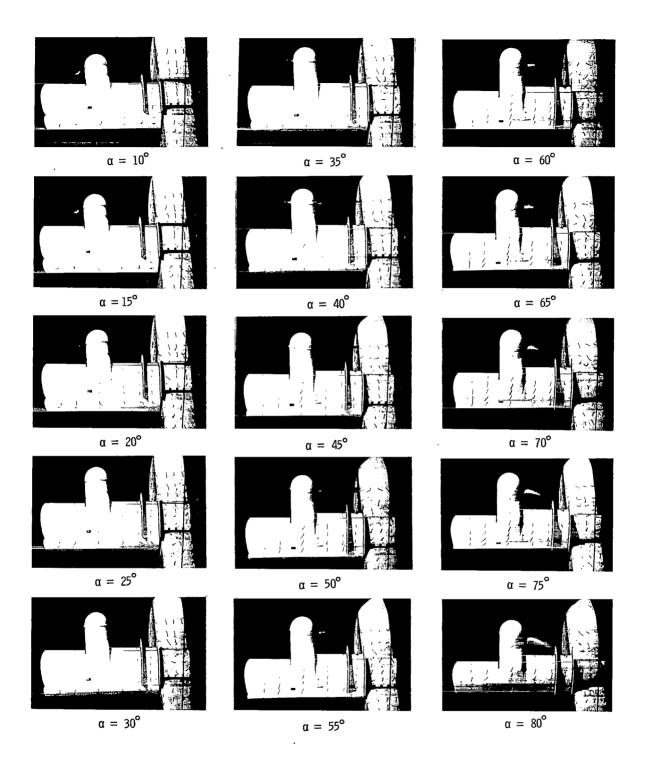
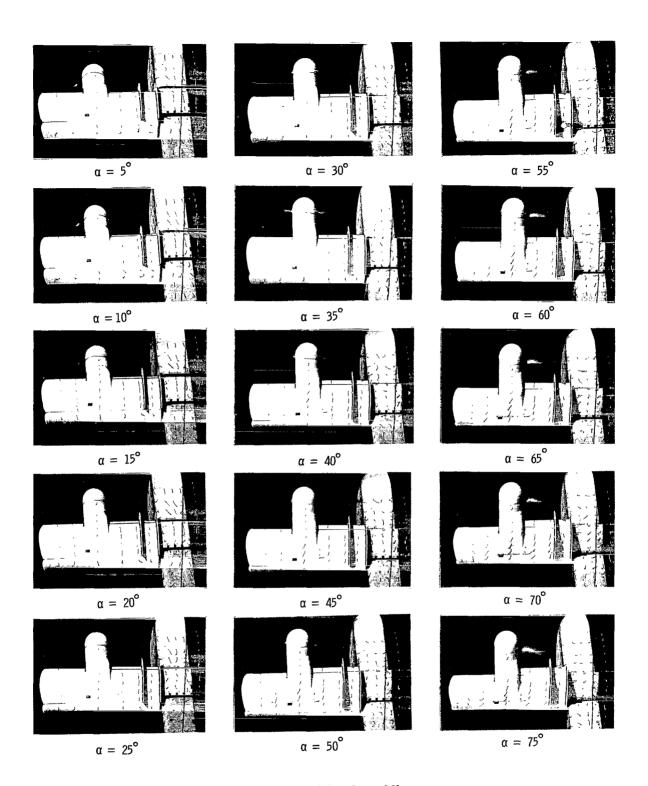


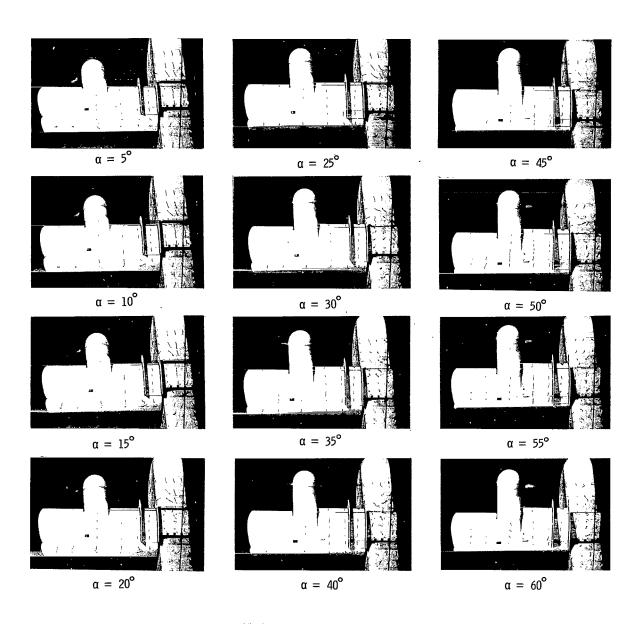
Figure 33.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, inboard slat on, fences on, and  $\delta_f = 60^{\circ}$ .



(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 33.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 33.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 33.- Continued.

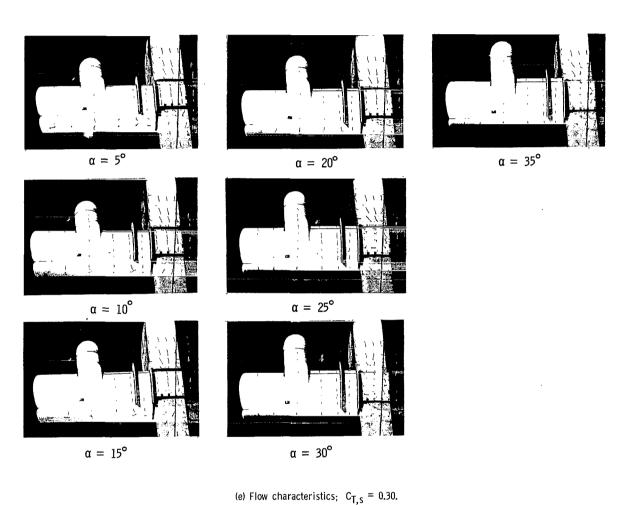


Figure 33.- Concluded.

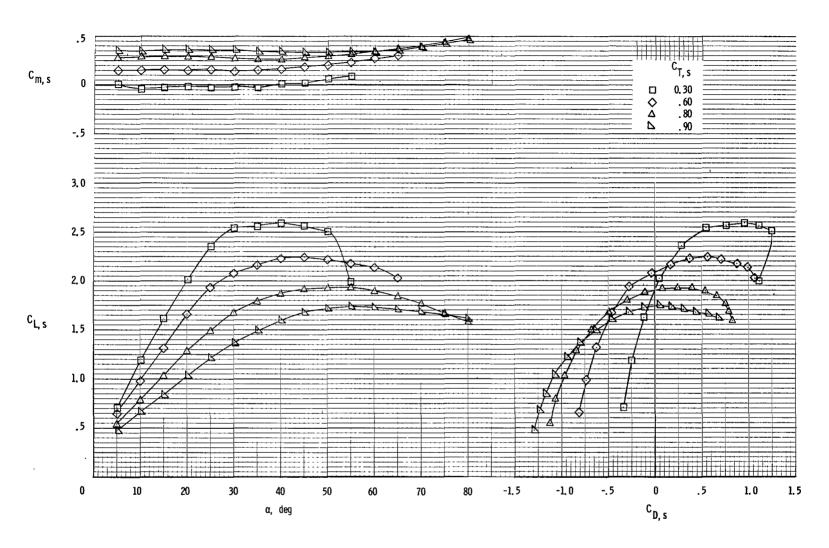
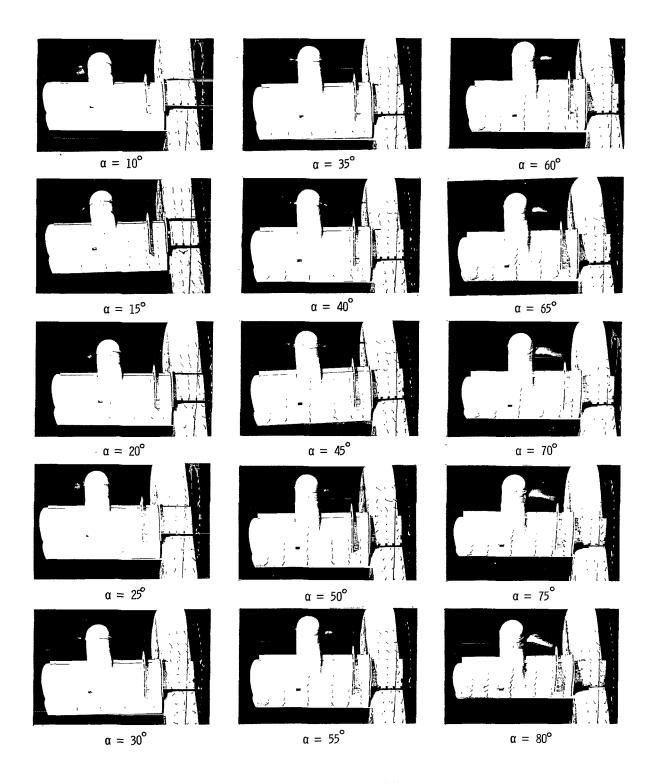
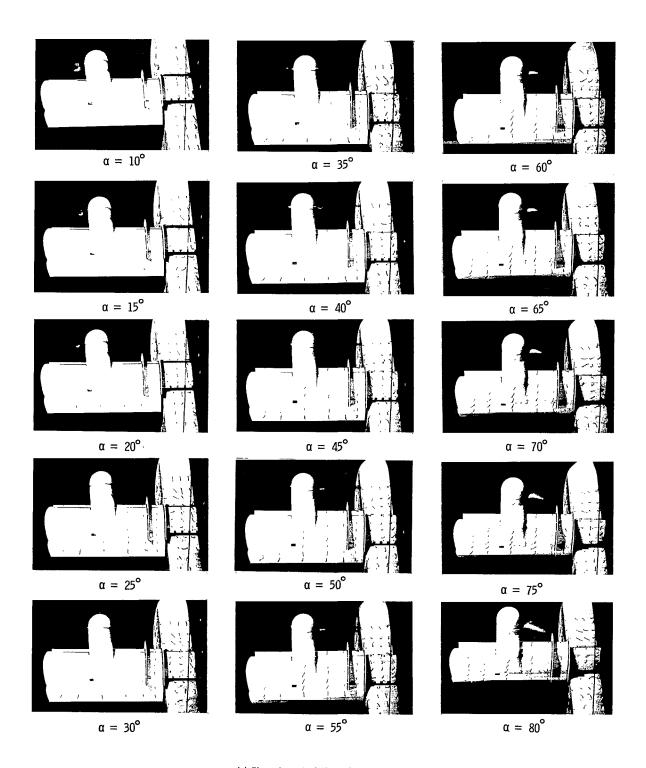


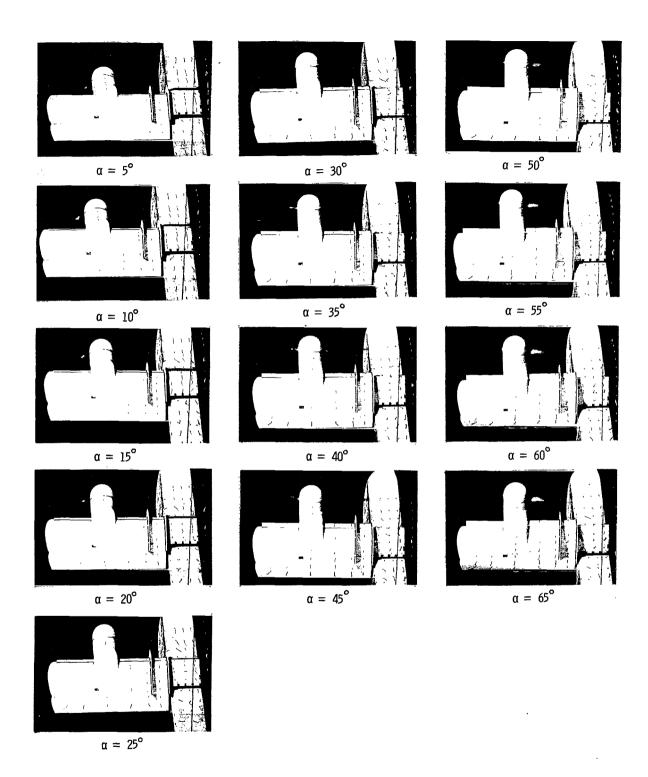
Figure 34.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, full-span slat on, fences on, and  $\delta_f = 20^\circ$ .



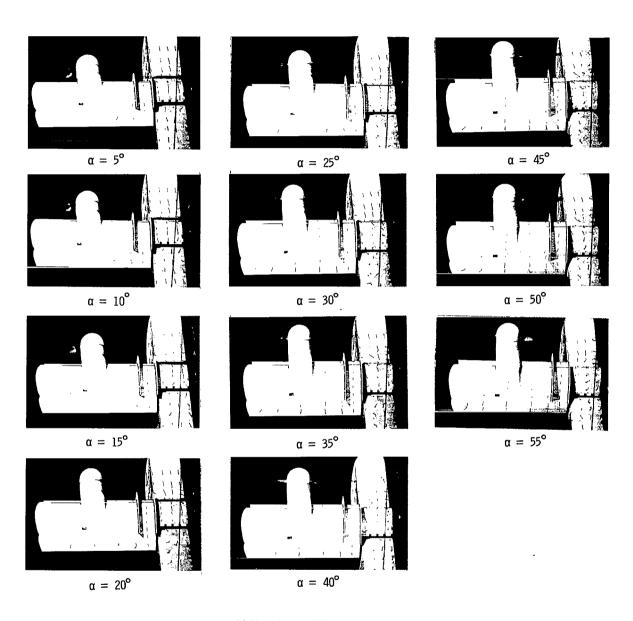
(b) Flow characteristics;  $C_{T,S} = 0.90$ . Figure 34.- Continued.



(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 34.- Continued.



(d) Flow characteristics;  $C_{T,S} = 0.60$ . Figure 34.- Continued.



(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 34.- Concluded.

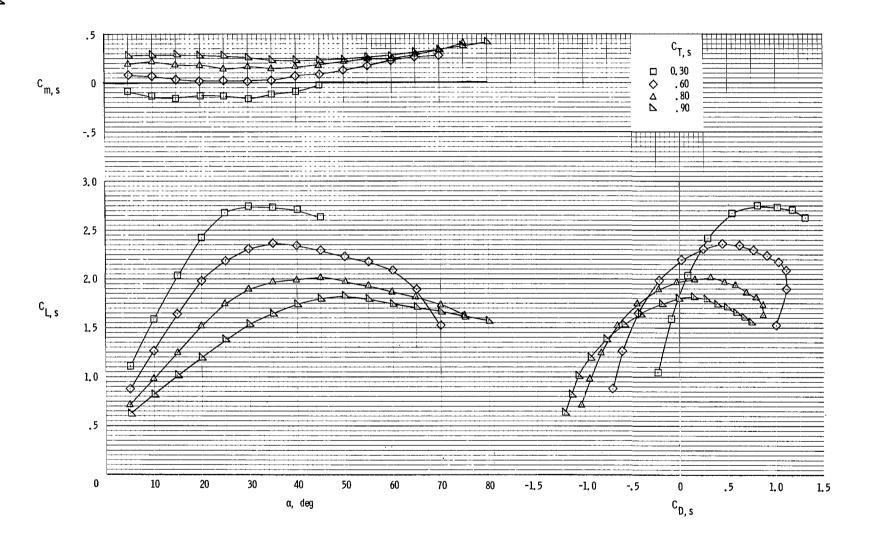
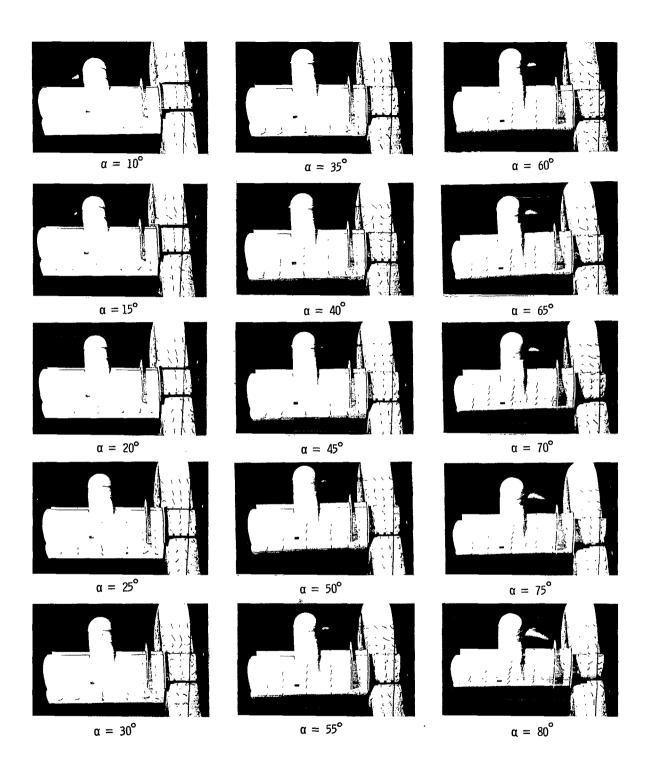
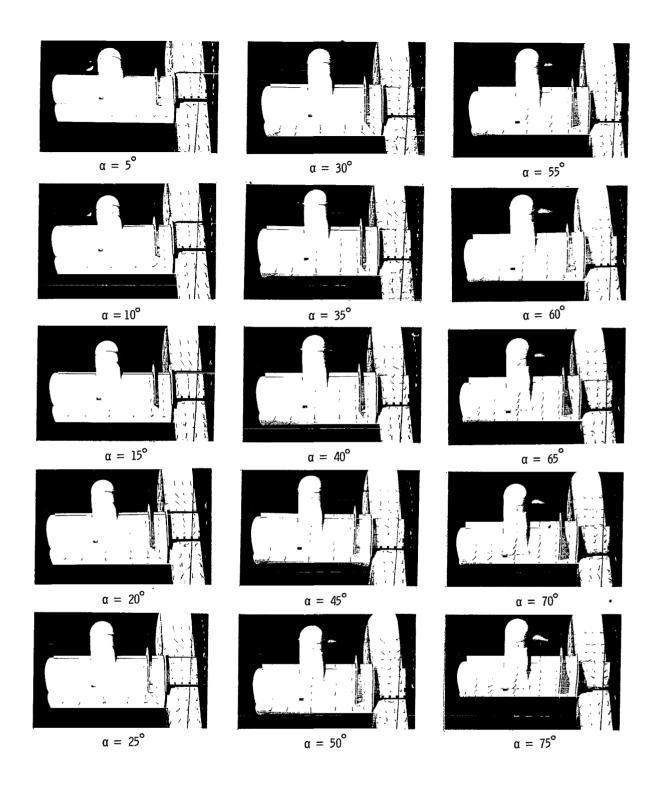


Figure 35.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, full-span slat on, fences on, and  $\delta_f = 40^\circ$ .

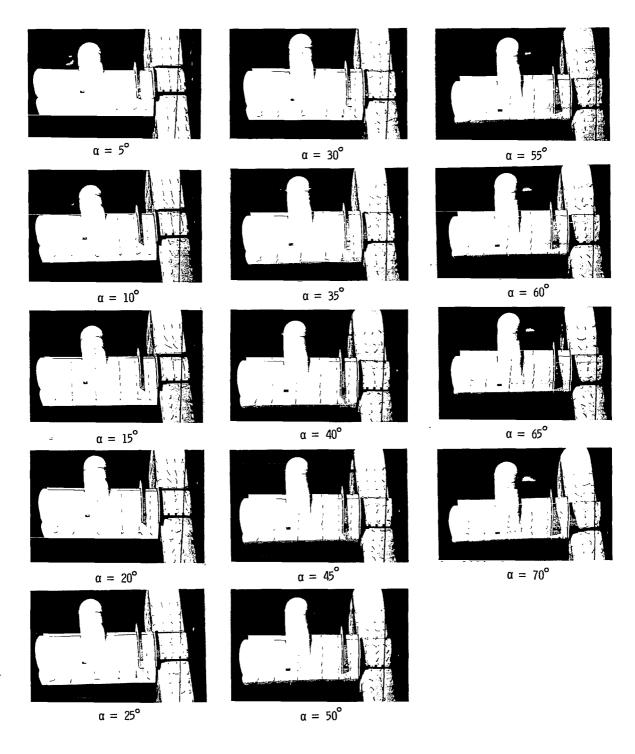


(b) Flow characteristics;  $C_{T,s} = 0.90$ . Figure 35.- Continued.

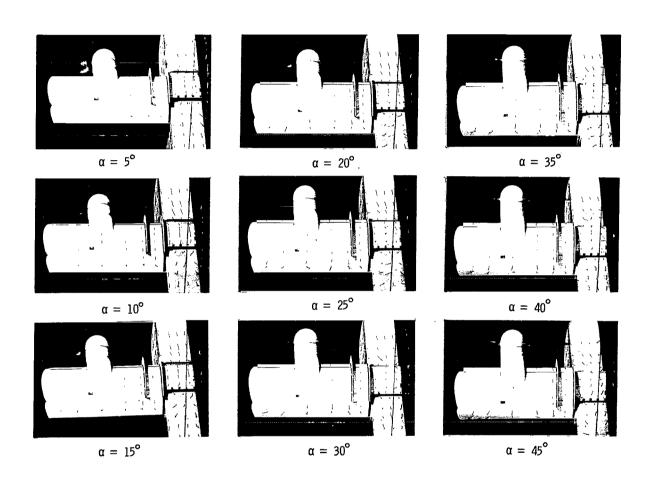
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(c) Flow characteristics;  $C_{T,S} = 0.80$ . Figure 35.- Continued.



(d) Flow characteristics;  $c_{T,s} = 0.60$ . Figure 35.- Continued.



(e) Flow characteristics;  $c_{T,s} = 0.30$ . Figure 35.- Concluded.

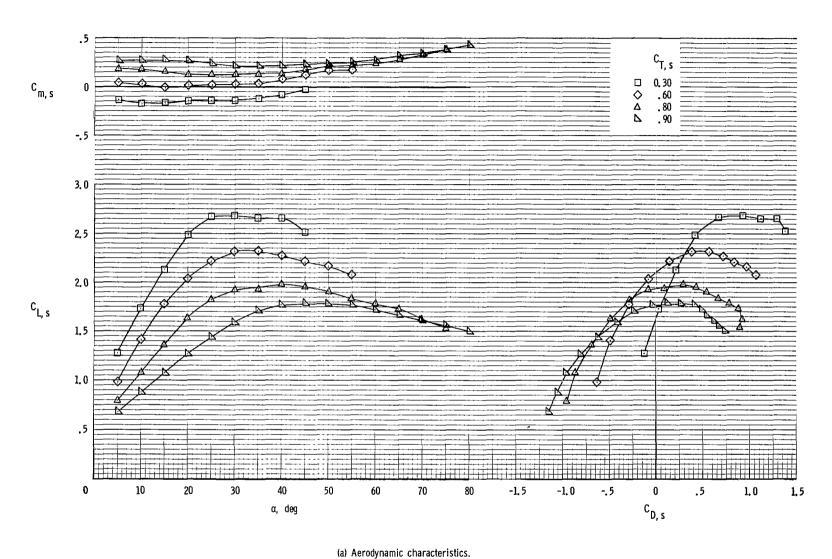
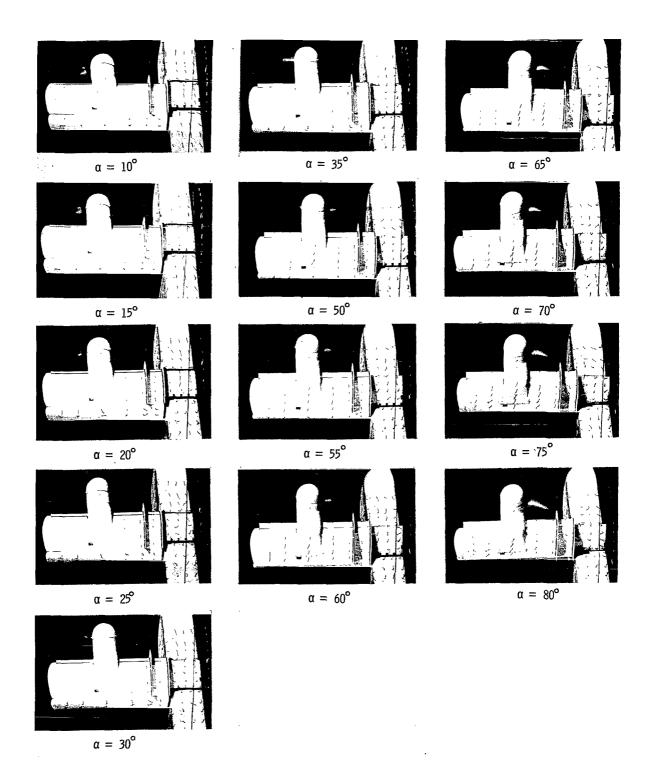
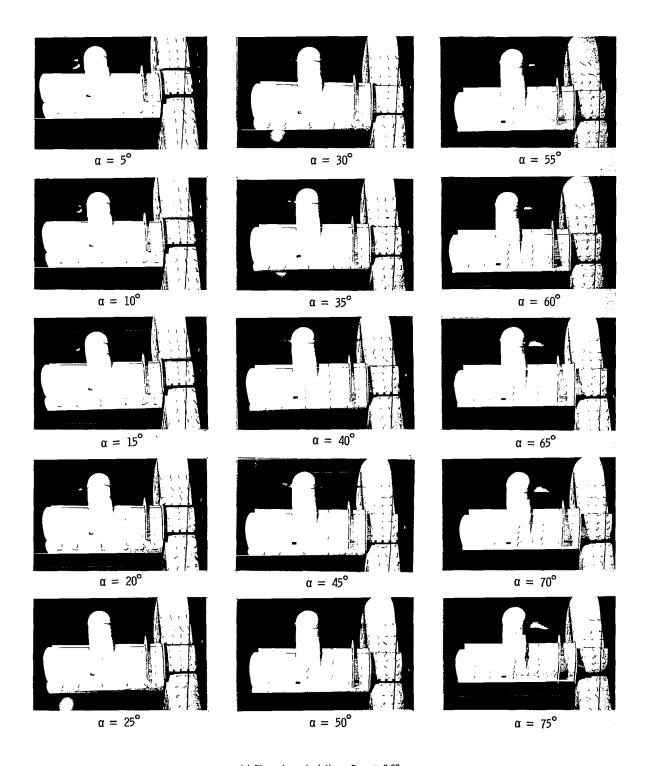


Figure 36.- Aerodynamic and flow characteristics of the wing with the propeller rotating up at the tip, full-span slat on, fences on, and  $\delta_f = 60^\circ$ .

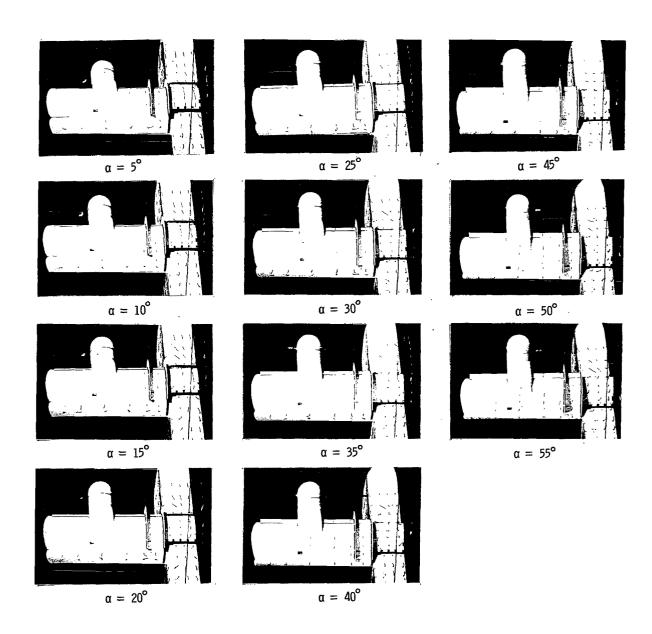


(b) Flow characteristics;  $c_{T,s} = 0.90$ . Figure 36.- Continued.

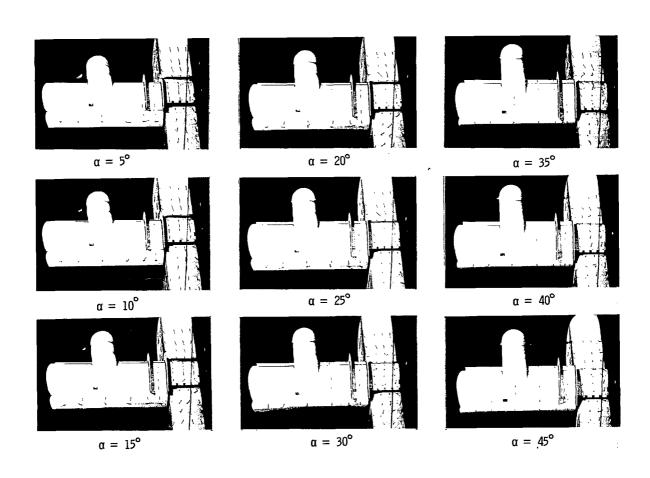


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(c) Flow characteristics;  $c_{T,s} = 0.80$ . Figure 36.- Continued.



(d) Flow characteristics;  $C_{T,s} = 0.60$ . Figure 36.- Continued.



(e) Flow characteristics;  $C_{T,S} = 0.30$ . Figure 36.- Concluded.

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